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The purpose of the Fuseology Section is to promote a better understanding of both fuses and common application details. The fuses to be considered are current sensitive devices which are designed as the intentional weak link in the electrical circuit. The function of the fuse is to provide protection of discrete components, or of complete circuits, by reliably melting under current overload conditions. This fuseology section will cover some important facts about fuses, selection considerations, and standards.

FUSE FACTS

The following fuse parameters or application concepts should be well understood in order to properly select a fuse for a given application.

AMBIENT TEMPERATURE: Refers to the temperature of the air immediately surrounding the fuse and is not to be confused with "room temperature." The fuse ambient temperature is appreciably higher in many cases, because it is enclosed (as in a panel mount fuseholder) or mounted near other heat producing components, such as resistors, transformers, etc.

BREAKING CAPACITY: See Interrupting Rating.

CURRENT RATING: The nominal amperage value marked on the fuse. It is established by the manufacturer as a value of current which the fuse can be loaded to, based on a controlled set of test conditions (See RERATING).

Catalog Fuse part numbers include series identification and amperage ratings. Refer to the FUSE SELECTION GUIDE section for guidance on making the proper choice.

RERATING: For 25°C ambient temperatures, it is recommended that fuses be operated at no more than 75% of the nominal current rating established using the controlled test conditions. These test conditions are part of UL/CSA/ANCE (Mexico) 248-14 "Fuses for Supplementary Overcurrent Protection," whose primary objective is to specify common test standards necessary for the continued control of manufactured items intended for protection against fire, etc. Some common variations of these standards include: fully enclosed fuseholders, high contact resistances, air movement, transient spikes, and changes in connecting cable size (diameter and length). Fuses are essentially temperature-sensitive devices. Even small variations from the controlled test conditions can greatly affect the predicted life of a fuse when it is loaded to its nominal value, usually expressed as 100% of rating.

The circuit design engineer should clearly understand that the purpose of these controlled test conditions is to enable fuse manufacturers to maintain unified performance standards for their products, and he must account for the variable conditions of his application. To compensate for these variables, the circuit design engineer who is designing for trouble-free, long-life fuse protection in his equipment generally loads his fuse not more than 75% of the nominal rating listed by the manufacturer, keeping in mind that overload and short circuit protection must be adequately provided for.

The fuses under discussion are temperature-sensitive devices whose ratings have been established in a 25°C ambient. The fuse temperature generated by the current passing through the fuse increases or decreases with ambient temperature change.

The ambient temperature chart in the FUSE SELECTION GUIDE section illustrates the effect that ambient temperature has on the nominal current rating of a fuse. Most traditional Slo-Blo® Fuse designs use lower melting temperature materials and are, therefore, more sensitive to ambient temperature changes.

DIMENSIONS: Unless otherwise specified, dimensions are in inches. The fuses in this catalog range in size from the approx. 0603 chip size (.063"L x .031"W x .018"H) up to the 5 AG, also commonly known as a "MIDGET" fuse (13/32" dia. x 1 1/2" length). As new products were developed throughout the years, fuse sizes evolved to fill the various electrical circuit protection needs. The first fuses were simple, open-wire devices, followed in the 1890's by Edison's enclosure of thin wire in a lamp base to make the first plug fuse. By 1904, Underwriters Laboratories had established size and rating specifications to meet safety standards. The renewable type fuses and automotive fuses appeared in 1914, and in 1927 Littelfuse started making very low amperage fuses for the budding electronics industry.

The fuse sizes in the chart below began with the early "Automobile Glass" fuses, thus the term "AG". The numbers were applied chronologically as different manufacturers started making a new size: "3AG," for example, was the third size placed on the market. Other non-glass fuse sizes and constructions were determined by functional requirements, but they still retained the length or diameter dimensions of the glass fuses. Their designation was modified to AB in place of AG, indicating that the outer tube was constructed from Bakelite, fibre, ceramic, or a similar material other than glass. The largest size fuse shown in the chart is the 5AG, or "MIDGET," a name adopted from its use by the electrical industry and the National Electrical Code range which normally recognizes fuses of 9/16" x 2" as the smallest standard fuse in use.

FUSE SIZES

SIZE	DIAMETER (Inches)		LENGTH (Inches)	
	1AG	1/4	.250	5/8
2AG	—	.177	—	.588
3AG	1/4	.250	1 1/4	1.25
4AG	9/32	.281	1 1/4	1.25
5AG	13/32	.406	1 1/2	1.50
7AG	1/4	.250	7/8	.875
8AG	1/4	.250	1	1

TOLERANCES: The dimensions shown in this catalog are nominal. Unless otherwise specified, tolerances are applied as follows:

- ± .010" for dimensions to 2 decimal places.
- ± .005" for dimensions to 3 decimal places.

The factory should be contacted concerning metric system and fractional tolerances. Tolerances do not apply to lead lengths.

FUSE CHARACTERISTICS: The characteristic of a fuse design refers to how rapidly the fuse responds to various current overloads. Fuse characteristics can be classified into three general categories: very fast-acting, fast-acting, or Slo-Blo® Fuse. The distinguishing feature of Slo-Blo® fuses is that these fuses have additional thermal inertia designed to tolerate normal initial or start-up overload pulses.

FUSE CONSTRUCTION: Internal construction may vary depending on ampere rating. Fuse photos in this catalog

FUSE FACTS

show typical construction of a particular ampere rating within the fuse series.

FUSEHOLDERS: In many applications, fuses are installed in fuseholders. These fuses and their associated fuseholders are not intended for operation as a “switch” for turning power “on” and “off”.

INTERRUPTING RATING: Also known as breaking capacity or short circuit rating, the interrupting rating is the maximum approved current which the fuse can safely interrupt at rated voltage. During a fault or short circuit condition, a fuse may receive an instantaneous overload current many times greater than its normal operating current. Safe operation requires that the fuse remain intact (no explosion or body rupture) and clear the circuit.

Interrupting ratings may vary with fuse design and range from 35 amperes AC for some 250V metric size (5 x 20mm) fuses up to 200,000 amperes AC for the 600V KLK series. Information on other fuse series can be obtained from the factory.

Fuses listed in accordance with UL/CSA/ANCE 248 are required to have an interrupting rating of 10,000 amperes, with some exceptions (See STANDARDS section) which, in many applications, provides a safety factor far in excess of the short circuit currents available.

NUISANCE OPENING: Nuisance opening is most often caused by an incomplete analysis of the circuit under consideration. Of all the “Selection Factors” listed in the FUSE SELECTION GUIDE, special attention must be given to items 1, 3, and 6, namely, normal operating current, ambient temperature, and pulses. For example, one prevalent cause of nuisance opening in conventional power supplies is the failure to adequately consider the fuse’s nominal melting I^2t rating. The fuse cannot be selected solely on the basis of normal operating current and ambient temperature. In this application, the fuse’s nominal melting I^2t rating must also meet the inrush current requirements created by the input capacitor of the power supply’s smoothing filter. The procedure for converting various waveforms into I^2t circuit demand is given in the FUSE SELECTION GUIDE. For trouble-free, long-life fuse protection, it is good design practice to select a fuse such that the I^2t of the waveform is no more than 20% of the nominal melting I^2t rating of the fuse. Refer to the section on PULSES in the FUSE SELECTION GUIDE.

RESISTANCE: The resistance of a fuse is usually an insignificant part of the total circuit resistance. Since the resistance of fractional amperage fuses can be several ohms, this fact should be considered when using them in low-voltage circuits. Actual values can be obtained from the factory. Most fuses are manufactured from materials which have positive temperature coefficients, and, therefore, it is common to refer to cold resistance and hot resistance (voltage drop at rated current), with actual operation being somewhere in between. Cold resistance is the resistance obtained using a measuring current of no more than 10% of the fuse’s nominal rated current. Values shown in this publication for cold resistance are nominal and representative. The factory should be consulted if this parameter is critical to the design analysis. Hot resistance is the resistance calculated from the stabilized voltage drop across the fuse, with current equal to the nominal rated current flowing through it.

Resistance data on all of our fuses is available on request. Fuses can be supplied to specified controlled resistance tolerances at additional cost.

SOLDERING RECOMMENDATIONS: Since most fuse constructions incorporate soldered connections, caution should be used when installing those fuses intended to be soldered in place. The application of excessive heat can reflow the solder within the fuse and change its rating. Fuses are heat-sensitive components similar to semi-conductors, and the use of heat sinks during soldering is often recommended.

TEST SAMPLING PLAN: Because compliance with certain specifications requires destructive testing, these tests are selected on a statistical basis for each lot manufactured.

TIME-CURRENT CURVE: The graphical presentation of the fusing characteristic, time-current curves are generally average curves which are presented as a design aid but are not generally considered part of the fuse specification. Time-current curves are extremely useful in defining a fuse, since fuses with the same current rating can be represented by considerably different time-current curves. The fuse specification typically will include a life requirement at 100% of rating and maximum opening times at overload points (usually 135% and 200% of rating). A time-current curve represents average data for the design; however, there may be some differences in the values for any one given production lot. Samples should be tested to verify performance, once the fuse has been selected.

UNDERWRITERS LABORATORIES: Reference to “Listed by Underwriters Laboratories” signifies that the fuses meet the requirements of UL/CSA/ANCE 248 “Fuses for Supplementary Overcurrent Protection”. Some 32 volt fuses (automotive) in this catalog are listed under UL Standard 275. Reference to “Recognized under the Component Program of Underwriters Laboratories” signifies that the item is recognized under the component program of Underwriters Laboratories and application approval is required.

VOLTAGE RATING: The voltage rating, as marked on a fuse, indicates that the fuse can be relied upon to safely interrupt its rated short circuit current in a circuit where the voltage is equal to, or less than, its rated voltage. This system of voltage rating is covered by N.E.C. regulations and is a requirement of Underwriters Laboratories as a protection against fire risk. The standard voltage ratings used by fuse manufacturers for most small-dimension and midjet fuses are 32, 63, 125, 250 and 600.

In electronic equipment with relatively low output power supplies, with circuit impedance limiting short circuit currents to values of less than ten times the current rating of the fuse, it is common practice to specify fuses with 125 or 250 volt ratings for secondary circuit protection of 500 volts or higher.

As mentioned previously (See RERATING), fuses are sensitive to changes in current, not voltage, maintaining their “status quo” at any voltage from zero to the maximum rating of the fuse. It is not until the fuse element melts and arcing occurs that the circuit voltage and available power become an issue. The safe interruption of the circuit, as it relates to circuit voltage and available power, is discussed in the section on INTERRUPTING RATING.

FUSE FACTS

To summarize, a fuse may be used at any voltage that is less than its voltage rating without detriment to its fusing characteristics. Please contact the factory for applications at voltages greater than the voltage rating.

DERIVATION OF NOMINAL MELTING I²t: Laboratory tests are conducted on each fuse design to determine the amount of energy required to melt the fusing element. This energy is described as nominal melting I²t and is expressed as "Ampere Squared Seconds" (A² Sec.). A pulse of current is applied to the fuse, and a time measurement is taken for melting to occur. If melting does not occur within a short duration of about 8 milliseconds (0.008 seconds) or less, the level of pulse current is increased. This test procedure

is repeated until melting of the fuse element is confined to within about 8 milliseconds. The purpose of this procedure is to assure that the heat created has insufficient time to thermally conduct away from the fuse element. That is, all of the heat energy (I²t) is used, to cause melting. Once the measurements of current (I) and time (t) are determined, it is a simple matter to calculate melting I²t. When the melting phase reaches completion, an electrical arc occurs immediately prior to the "opening" of the fuse element. Clearing I²t = Melting I²t + arcing I²t. The nominal I²t values given in this publication pertain to the melting phase portion of the "clearing" or "opening".

FUSE SELECTION GUIDE

The application guidelines and product data in this guide are intended to provide technical information that will help with application design. Since these are only a few of the contributing parameters, application testing is strongly recommended and should be used to verify performance in the circuit/application.

Many of the factors involved with fuse selection are listed below:

Selection Factors

1. Normal operating current
2. Application voltage (AC or DC)
3. Ambient temperature
4. Overload current and length of time in which the fuse must open.
5. Maximum available fault current
6. Pulses, Surge Currents, Inrush Currents, Start-up Currents, and Circuit Transients
7. Physical size limitations, such as length, diameter, or height
8. Agency Approvals required, such as UL, CSA, VDE, or Military
9. Considerations: mounting type/form factor, ease of removal, axial leads, visual indication, etc.
10. Fuseholder features: clips, mounting block, panel mount, p.c. board mount, R.F.I. shielded, etc.

NORMAL OPERATING CURRENT: The current rating of a fuse is typically derated 25% for operation at 25°C to avoid nuisance blowing. For example, a fuse with a current rating of 10A is not usually recommended for operation at more than 7.5A in a 25°C ambient. For additional details, see RERATING in the previous section and AMBIENT TEMPERATURE below.

VOLTAGE: The voltage rating of the fuse must be equal to, or greater than, the available circuit voltage. For exceptions, see VOLTAGE RATING.

AMBIENT TEMPERATURE: The current carrying capacity tests of fuses are performed at 25°C and will be affected by changes in ambient temperature. The higher the ambient temperature, the hotter the fuse will operate, and the shorter its life will be. Conversely, operating at a lower temperature will prolong fuse life. A fuse also runs hotter as the normal operating current approaches or exceeds the rating of the selected fuse. Practical experience indicates fuses at **room temperature** should last indefinitely, if operated at no more than 75% of catalog fuse rating.

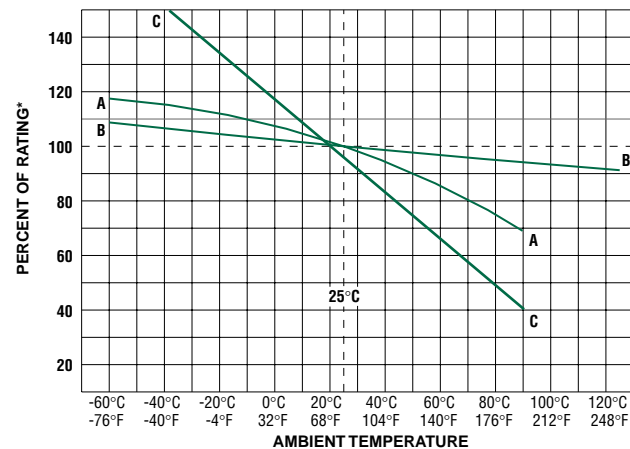
CHART SHOWING EFFECT OF AMBIENT TEMPERATURE ON CURRENT-CARRYING CAPACITY (TYPICAL)

KEY TO CHART:

Curve A: Thin-Film Fuses and 313 Series (.010 to .150A)

Curve B: Very Fast-Acting, Fast-Acting, and Spiral Wound Slo-Blo® Fuses

Curve C: Resettable PTC's



*Ambient temperature effects are in addition to the normal derating, see example.

Example: Given a normal operating current of 1.5 amperes in an application using a traditional Slo-Blo® fuse at room temperature, then:

$$\text{Catalog Fuse Rating} = \frac{\text{Normal Operating Current}}{0.75}$$

or

$$\frac{1.5 \text{ Amperes}}{0.75} = 2.0 \text{ Amp Fuse (at } 25^{\circ}\text{C)}$$

FUSE SELECTION GUIDE

Similarly, if that same fuse were operated at a very high ambient temperature of 70°C, additional derating would be necessary. Curve “A” (Traditional Slo-Blo® Fuse) of the ambient temperature chart shows the maximum operating “Percent of Rating” at 70°C to be 80%, in which case;

$$\text{Catalog Fuse Rating} = \frac{\text{Nominal Operating Current}}{0.75 \times \text{Percent of Rating}}$$

or

$$\frac{1.5 \text{ Amperes}}{0.75 \times 0.80} = 2.5 \text{ Amp Fuse (at 70°C)}$$

OVERLOAD CURRENT CONDITION: The current level for which protection is required. Fault conditions may be specified, either in terms of current or, in terms of both current and maximum time the fault can be tolerated before damage occurs. Time-current curves should be consulted to try to match the fuse characteristic to the circuit needs, while keeping in mind that the curves are based on average data.

MAXIMUM FAULT CURRENT: The Interrupting Rating of a fuse must meet or exceed the Maximum Fault Current of the circuit.

PULSES: The general term “pulses” is used in this context to describe the broad category of wave shapes referred to as “surge currents”, “start-up currents”, “inrush currents”, and “transients”. Electrical pulse conditions can vary considerably from one application to another. Different fuse constructions may not all react the same to a given pulse condition. Electrical pulses produce thermal cycling and possible mechanical fatigue that could affect the life of the fuse. Initial or start-up pulses are normal for some applications and require the characteristic of a Slo-Blo® fuse. Slo-Blo® fuses incorporate a thermal delay design to enable them to survive normal start-up pulses and still provide protection against prolonged overloads. The start-up pulse should be defined and then compared to the time-current curve and I²t rating for the fuse. Application testing is recommended to establish the ability of the fuse design to withstand the pulse conditions.

Nominal melting I²t is a measure of the energy required to melt the fusing element and is expressed as “Ampere Squared Seconds” (A² Sec.). This nominal melting I²t, and the energy it represents (within a time duration of 8 milliseconds [0.008 second] or less and 1 millisecond [0.001 second] or less for thin film fuses), is a value that is constant for each different fusing element. Because every fuse type and rating, as well as its corresponding part number, has a different fusing element, it is necessary to determine the I²t for each. This I²t value is a parameter of the fuse itself and is controlled by the element material and the configuration of the fuse element. In addition to selecting fuses on the basis of “Normal Operating Currents”, “Derating”, and “Ambient Temperature” as discussed earlier, it is also necessary to apply the I²t design approach. This nominal melting I²t is not only a constant value for each fuse element design, but it is also independent of temperature and voltage. Most often, the nominal melting I²t method of fuse selection is applied to those applications in which the fuse must sustain large current pulses of a short duration. These high-energy currents are common in many applications and are described by a variety of terms, such as “surge current”, “start-up current”, “inrush current”, and other similar circuit “transients” that can be classified in the general

category of “pulses.” Laboratory tests are conducted on each fuse design to determine its nominal melting I²t rating. The values for I²t given in this publication are nominal and representative. The factory should be consulted if this parameter is critical to the design analysis. The following example should assist in providing a better understanding of the application of I²t.

EXAMPLE: Select a 125V, very fast-acting PICO® fuse that is capable of withstanding 100,000 pulses of current (I) of the pulse waveform shown in Figure 1. The normal operating current is 0.75 ampere at an ambient temperature of 25°C.

Step 1 — Refer to Chart I (page #6) and select the appropriate pulse waveform, which is waveform (E) in this example. Place the applicable value for peak pulse current (i_p) and time (t) into the corresponding formula for wave-shape (E), and calculate the result, as shown:

$$I^2t = \frac{1}{5} (i_p)^2 t$$

$$= \frac{1}{5} \times 8^2 \times .004 = 0.0512 \text{ A}^2 \text{ Sec.}$$

This value is referred to as the “Pulse I²t”.

Step 2 — Determine the required value of Nominal Melting I²t by referring to Chart II (page 6). A figure of 22% is shown in Chart II for 100,000 occurrences of the Pulse I²t calculated in Step 1. This Pulse I²t is converted to its required value of Nominal Melting I²t as follows:

$$\text{Nom. Melt } I^2t = \text{Pulse } I^2t / .22$$

$$= 0.0512 / .22 = 0.2327 \text{ A}^2 \text{ Sec.}$$

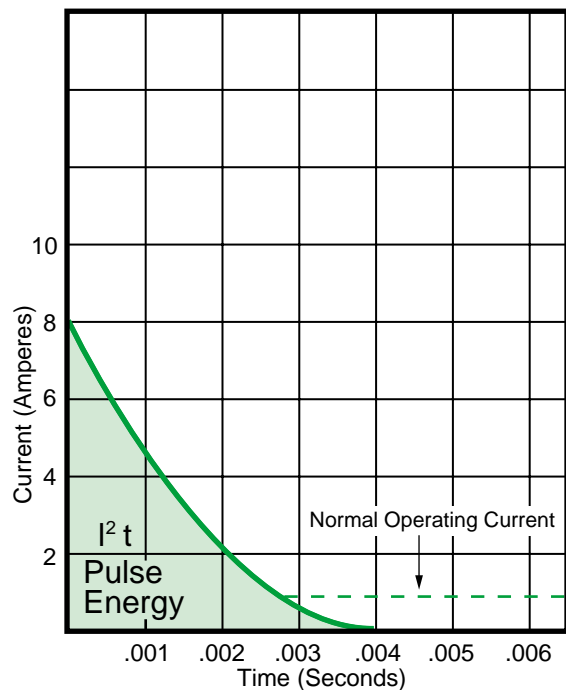
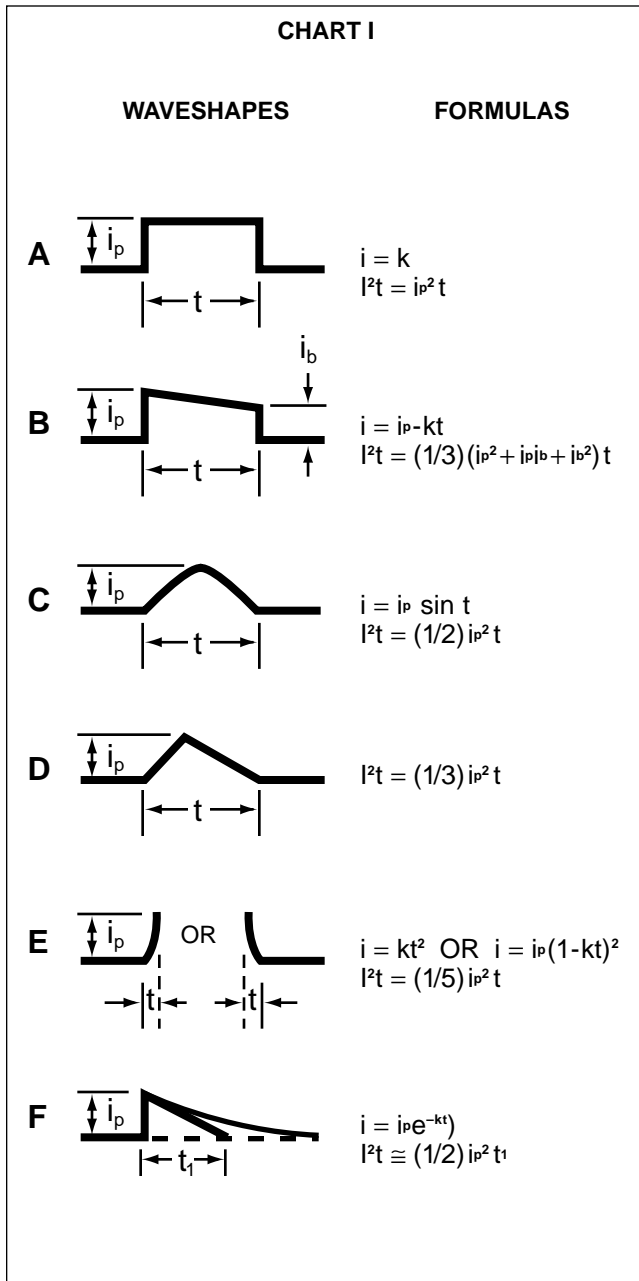


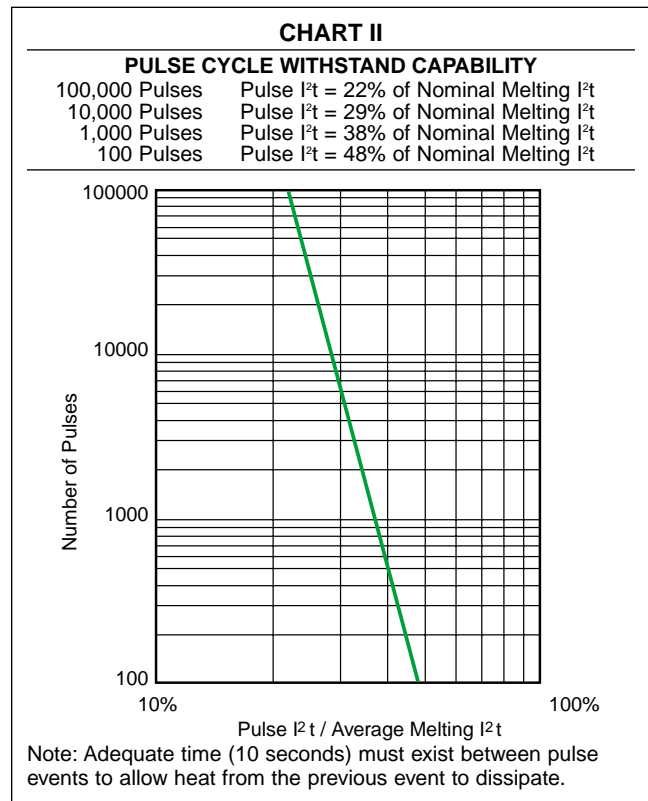
Figure 1

FUSE SELECTION GUIDE



Step 3 — Examine the I^2t rating data for the PICO® II, 125V, very fast-acting fuse. The part number 251001, 1 ampere design is rated at 0.256 A² Sec., which is the minimum fuse rating that will accommodate the 0.2327 A² Sec. value calculated in Step 2. This 1 ampere fuse will also accommodate the specified 0.75 ampere normal operating current, when a 25% derating factor is applied to the 1 ampere rating, as previously described.

TESTING: The above factors should be considered in selecting a fuse for a given application. The next step is to verify the selection by requesting samples for testing in the actual circuit. Before evaluating the samples, make sure the fuse is properly mounted with good electrical connections, using adequately sized wires or traces. The testing should include life tests under normal conditions and overload tests under fault conditions, to ensure that the fuse will operate properly in the circuit.



FUSEHOLDER SELECTION GUIDE

DERATING: For 25°C ambient temperatures, it is recommended that fuseholders be operated at no more than 60% of the nominal current rating established using the controlled test conditions specified by Underwriters Laboratories. The primary objective of these UL test conditions is to specify common test standards necessary for the continued control of manufactured items intended for protection against fire, etc. A copper dummy fuse is inserted in the fuseholder by Underwriters Laboratories, and then the current is increased until a certain temperature rise occurs. The majority of the heat is produced by the contact resistance of the fuseholder clips. This value of

current is considered to be the rated current of the fuseholder, expressed as 100% of rating. Some of the more common, everyday applications may differ from these UL test conditions as follows: fully enclosed fuseholders, high contact resistance, air movement, transient spikes, and changes in connecting cable size (diameter and length). Even small variations from the controlled test conditions can greatly affect the ratings of the fuseholder. For this reason, it is recommended that fuseholders be derated by 40% (operated at no more than 60% of the nominal current rating established using the Underwriter Laboratories test conditions, as stated above).

Littelfuse is at your service to help solve your electrical protection problems. When contacting Littelfuse sales engineers, please have all the requirements of your applications available. Requests for quotes or assistance in designing or selecting special types of circuit protection components for your particular applications are also welcome.

In the absence of special requirements, Littelfuse reserves the right to make appropriate changes in design, process, and manufacturing location without prior notice.

STANDARDS

Fuse ratings and other performance criteria are evaluated under laboratory conditions **and acceptance criteria**, as defined in one or more of the various fuse standards. It is important to understand these standards so that the fuse can be properly applied to circuit protection applications.

UL/CSA/ANCE (Mexico) 248-14 FUSES FOR SUPPLEMENTARY OVERCURRENT PROTECTION (600 Volts, Maximum) (Previously UL 198G and CSA C22.2, No. 59)

UL LISTED

A UL Listed fuse meets all the requirements of the UL/CSA 248-14 Standard. Following are some of the requirements.

UL ampere rating tests are conducted at 100%, 135%, and 200% of rated current. The fuse must carry 110% of its ampere rating and must stabilize at a temperature that does not exceed a 75°C rise at 100%.

The fuse must open at 135% of rated current within one hour. It also must open at 200% of rated current within 2 minutes for 0-30 ampere ratings and 4 minutes for 35-60 ampere ratings.

The interrupting rating of a UL Listed fuse is 10,000 amperes AC minimum at 125 volts. Fuses rated at 250 volts may be listed as interrupting 10,000 amperes at 125 volts and, at least, the minimum values shown below at 250 volts.

Ampere Rating of Fuse	Interrupting Rating In Amperes	Voltage Rating
0 to 1	35	250 VAC
1.1 to 3.5	100	250 VAC
3.6 to 10	200	250 VAC
10.1 to 15	750	250 VAC
15.1 to 30	1500	250 VAC

Recognized Under the Component Program of Underwriters Laboratories

The Recognized Components Program of UL is different from UL Listing. UL will test a fuse to a specification requested by the manufacturer. The test points can be different from the UL Listed requirements if the fuse has been designed for a specific application. Application approval is required by UL for fuses recognized under the Component Program.


UL 275 AUTOMOTIVE GLASS TUBE FUSES (32 Volts)

UL Listed

UL ampere ratings tests are conducted at 110%, 135%, and 200%. Interrupting rating tests are not required.

CSA Certification

CSA Certification in Canada is equivalent to UL Listing in the United States.

 The Component Acceptance Program of CSA is equivalent to the Recognition Program at UL. This CSA Program allows the manufacturer to declare a specification. CSA then verifies the test results.

MITI APPROVAL



MITI® approval in Japan is similar to UL Recognition in the United States.

MITI® has its own design standard and characteristics.

INTERNATIONAL ELECTROTECHNICAL COMMISSION (IEC)

Publication 60127, Sheet 1, 2, 3, 5, 6 (250 Volts)

The IEC organization is different from UL and CSA, since IEC only writes specifications and does not certify. UL and CSA write the specifications, are responsible for testing, and give certification.

Certification to IEC specifications are given by such organizations as SEMKO (Swedish Institute of Testing and Approvals of Electrical Equipment)  and BSI (British Standards Institute) , as well as UL and CSA.

IEC Publication 60127 defines three breaking capacity levels (interrupting rating). Low breaking capacity fuses must pass a test of 35 amperes or ten times rated current, whichever is greater, while enhanced breaking capacity fuses must pass a test of 150 amperes and finally high breaking capacity fuses must pass a test of 1500 amperes.

- Sheet 1 – Type F Quick Acting, High Breaking Capacity
- Sheet 2 – Type F Quick Acting, Low Breaking Capacity
- Sheet 3 – Type T Time Lag, Low Breaking Capacity
- Sheet 5 – Type T Time Lag, High Breaking Capacity
- Sheet 6 – Type T Time Lag, Enhanced Breaking Capacity

The letters 'F' and 'T' represent the time-current characteristic of the fast-acting and time delay fuses. One of these letters will be marked on the end cap of the fuse.

UL/CSA/ANCE (Mexico) 248-14 vs. IEC 60127 FUSE OPENING TIMES (UL/CSA/ANCE (Mexico) 248-14 Was Previously UL 198G and CSA 22.2, No. 59) vs. MITI®

Percent of Rating	UL & CSA STD 248-14	IEC TYPE F Sheet 1 (*)	IEC Type F Sheet 2 (*)	IEC Type T Sheet 3 & 4 (*)	IEC Type T Sheet 5 (*)	MITI®
110	4 Hr. Min.	—	—	—	—	
130	—	—	—	—	—	1Hr. Min.
135	60 Minutes Max.	—	—	—	—	
150	—	60 Minutes Min.	60 Minutes Min.	60 Minutes Min.	60 Minutes Min.	
160	—	—	—	—	—	1 Hr. Max.
200	2 Minutes Max.	—	—	—	—	2 Minutes Max.
210	—	30 Minutes Max.	30 Minutes Max.	2 Minutes Max.	30 Minutes Max.	

(*) Note: The IEC Specification is only written up to 6.3A, any components above these ratings are not recognized by the IEC (although the fuses may have those opening characteristics).

IEC also has requirements at 275%, 400% and 1000%; however, the chart is used to show that fuses with the same ampere rating made to different specifications are not interchangeable. According to the IEC 60127 Standard, a one ampere-rated fuse can be operated at one ampere. A one ampere-rated fuse made to UL/CSA/ANCE 248-14 should not be operated at more than .75 ampere (25% derated — See RERATING section of FUSEOLOGY).

MITI® covers only one characteristic i.e. there are no 'delay' definitions on other performance variants.

STANDARDS AND PACKAGING INFORMATION

Publication IEC 60127-4 (Universal Modular Fuse-Links [UMF])

This part of IEC 60127 covers both PCB through-hole and surface mount fuses. This standard covers fuses rated 32, 63, 125, and 250 volts. This standard will be accepted by UL/CSA making it the first global fuse standard. This specification uses different fusing gates than IEC 60127-2; the gates used here are 125%, 200%, and 1000%.

The fuses must not open in less than one hour at 125% of rated current and open within two minutes at 200% of rated current. The 1000% overload is used to determine the fuse characteristic. The time for each rating is listed below.

- Type FF: Less than 0.001 sec.
- Type F: From 0.001 - 0.01 sec.
- Type T: From 0.01 - 0.1 sec.
- Type TT: From 0.1 - 1.00 sec.

These characteristics correlate to the terminology used in IEC 60127-1.

Breaking capacity (interrupting rating) varies based on volt age rating. Parts rated at 32 & 63 volts must pass a test of 35 amperes or ten times rated current, whichever is greater. Parts rated at 125 volts must pass a test of 50 amperes or ten times rated current, whichever is greater. Parts rated at 250 volts are further defined as either low, intermediate or high breaking. The low breaking capacity fuses must pass a test of 100 amperes or ten times rated current, while intermediate breaking capacity fuses must pass a test of 500 amperes and, finally, high breaking capacity fuses must pass a test of 1500 amperes.

Packaging Suffixes

- A/X = 1 unit per bag
- V = 5 units per box
- T = 10 units per box
- H = 100 units per box
- U = 500 units per box
- M = 1000 units per box
- P = 2000 units per box
- W = 3000 units per box
- N = 5000 units per box
- R = Taped & reeled fuses
- M1 = Taped & reeled. Spacing = 4 mm.
1000 pieces per reel
- MT1 = Taped & reeled. Spacing = 2.062 inches (52.4 mm)
1000 pieces per reel
- MT2 = Taped & reeled. Spacing = 2.50 inches (63.5 mm)
1000 pieces per reel
- MT3 = Taped & reeled. Spacing = 2.874 inches (73 mm)
1000 pieces per reel
- NT1 = Taped & reeled. Spacing = 2.062 inches (52.4 mm)
5000 pieces per reel
- NT2 = Taped & reeled. Spacing = 2.50 inches (63.5 mm)
5000 pieces per reel
- NT3 = Taped & reeled. Spacing = 2.874 inches (73 mm)
5000 pieces per reel

Tx = Taped & reeled. Spacing to be determined.

MILITARY/FEDERAL STANDARDS

See Table of Contents for Military Product Section.

Fuses and holders approved to the following Military specifications are on the Qualified Products List (QPL) for that specification.

MIL-PRF-15160 and MIL-PRF-23419

These specifications govern the construction and performance of fuses suitable primarily for military electronic applications.

MIL-PRF-19207

This specification governs the construction and performance of fuseholders suitable for military applications.

DESC Drawing #87108

This drawing governs the construction and performance of .177" x .570" (2AG size) cartridge fuses and axial lead versions suitable for military applications. DESC #87108 designation is included in the fuse end cap marking.

FEDERAL SPECIFICATION W-F-1814

This specification governs the construction and performance of fuses with high interrupting ratings that are approved for federal applications. Fuses approved to these specifications are on the Federal Qualified Products List.

Write to the following agencies for additional information on standards, approvals, or copies of the specifications.

Underwriters Laboratories Inc. (UL)

333 Pfingsten Road
Northbrook, IL 60062
Att: Publications Stock

Canadian Standards Association (CSA)

178 Rexdale Boulevard
Rexdale, Ontario, Canada M9W 1R3
Att: Standard Sales

International Electrotechnical Commission (IEC)

3, Rue de Varembe
1211 Geneva 20
Switzerland
Att: Sales Department

Naval Publications and Military Standards Form Center (for Military and Federal Standards)

5801 Tabor Avenue
Philadelphia, PA 19120
Att: Commanding Officer

Defense Supply Center Columbus (DSSC)

3990 East Broad Street
Columbus, OH 43216-5000

Ministry of International Trade and Industry (MITI)

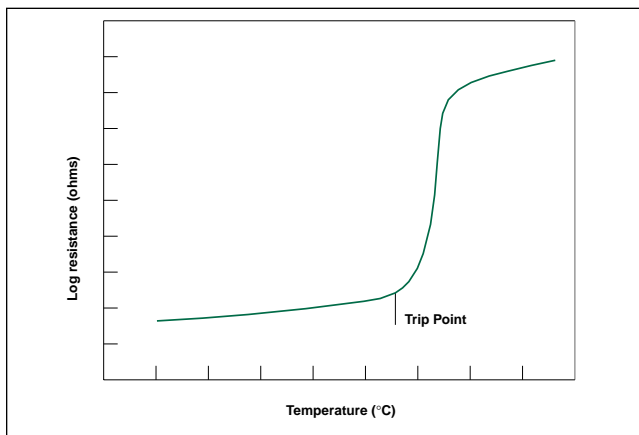
Kasumigaseki
Chi-Youda-Ku
Tokyo 100, Japan

PTC FACTS

Overcurrent circuit protection can be accomplished with the use of either a traditional fuse or the more recently developed resettable PTC. Both devices function by reacting to the heat generated by the excessive current flow in the circuit. The fuse melts open, interrupting the current flow, and the PTC changes from a low resistance to a high resistance to limit current flow. Understanding the differences in performance between the two types of devices will make the best circuit protection choice easier.

The most obvious difference is that the PTC is *resettable*. The general procedure for resetting after an overload has occurred is to remove power and allow the device to cool down. There are several other operating characteristics that differentiate the two types of products. The terminology used for PTCs is often similar but not the same as for fuses. Two parameters that fall into this category are leakage current and interrupting rating.

LEAKAGE CURRENT: The PTC is said to have “tripped” when it has transitioned from the low resistance state to the high resistance state due to an overload.



Protection is accomplished by limiting the current flow to some *leakage* level. Leakage current can range from less than a hundred milliamps at rated voltage up to a few hundred milliamps at lower voltages. The fuse on the other hand completely interrupts the current flow and this open circuit results in “0” leakage current when subjected to an overload.

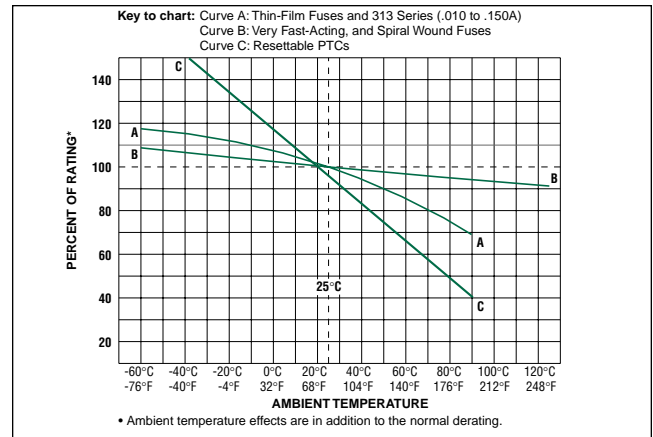
INTERRUPTING RATING: The PTC is rated for a maximum short circuit current at rated voltage. This fault current level is the maximum current that the device can withstand but the PTC will not actually interrupt the current flow (see LEAKAGE CURRENT above). A typical PTC short circuit rating is 40A. Fuses do in fact interrupt the current flow in response to the overload and the range of interrupting ratings goes from hundreds of amperes up to 10,000 amperes at rated voltage.

The circuit parameters may dictate the component choice based on typical device rating differences.

VOLTAGE RATING: General use PTCs are not rated above 60V while fuses are rated up to 600V.

CURRENT RATING: The operating current rating for PTCs can be up to 11A while the maximum level for fuses can exceed 20A.

TEMPERATURE RATING: The useful upper limit for a PTC is generally 85°C while the maximum operating temperature for fuses is 125°C. The following temperature derating curves that compare PTCs to fuses illustrate that more derating is required for a PTC at a given temperature.



Additional operating characteristics can be reviewed by the circuit designer in making the decision to choose a PTC or a fuse for overcurrent protection.

AGENCY APPROVALS: PTCs are Recognized under the Component Program of Underwriters Laboratories to UL Thermistor Standard 1434. The devices have also been certified under the CSA Component Acceptance Program. Approvals for fuses include Recognition under the Component Program of Underwriters Laboratories and the CSA Component Acceptance Program. In addition, many fuses are available with full “Listing” in accordance with the new Supplementary Fuse Standard UL/CSA/ANCE (Mexico) 248-14.

RESISTANCE: Reviewing product specifications indicates that similarly rated PTCs have about twice (sometimes more) the resistance of fuses.

TIME-CURRENT CHARACTERISTIC: Comparing the time-current curves of PTCs to time-current curves of fuses show that the speed of response for a PTC is similar to the time delay of a Slo-Blo® fuse.

SUMMARY: Many of the issues discussed become a matter of preference, but there is an important area of application where the use of resettable PTCs is becoming a requirement. Much of the design work for personal computers and peripheral devices is strongly influenced by *Microsoft and Intel System Design Guide* which states that “Using a fuse that must be replaced each time an overcurrent condition occurs is unacceptable.” And the *Plug and Play SCSI* (Small Computer Systems Interface) Specification for this large market includes a statement that “...must provide a self-resetting device to limit the maximum amount of current sourced”.

The PTC / fuse discussion provides some insight as to when PTCs may be the appropriate choice for providing overcurrent circuit protection. A selection guide worksheet appears on the following page as an aid in choosing the best circuit protection component.

SELECTION GUIDE WORKSHEET

1. Define the circuit operating parameters.

Complete the following form:

Normal operating current in amperes: _____

Normal operating voltage in volts: _____

Maximum interrupt current: (see page 3) _____

Ambient Temperature/Rerating: (see page 4) _____

Typical overload current: _____

Required opening time at specified overload: _____

Transient pulses expected: (see page 5) _____

Resettable or one-time: _____

Agency Approvals: _____

Mounting type/form factor: _____

Typical resistance (in circuit): _____

2. Select the proper circuit protection component.

LITTELFUSE CIRCUIT PROTECTION COMPARISON TABLE:

	Surface Mount PTC (Pg. 22-25)	30V PTC Leaded (Pg. 26-27)	60V PTC Leaded (Pg. 28-29)	'0603' SMF (Pg. 34-35)	'1206' SMF (Pg. 33, 36)
Operating Current Range	0.300 - 2.6A	0.900 - 9A	0.100 - 3.75A	0.250 - 5A	0.125 - 7A
Maximum Voltage (*)	60V	30V	60V	32V	125V
Maximum Interrupting Rating (**)	40A	40A	40A	50A	50A
Temperature Range	-40°C to 85°C	-40°C to 85°C	-40°C to 85°C	-55°C to 125°C	-55°C to 125°C
Thermal Rerating	Medium	Medium	Medium	Low	Low
Opening time at 200% I_N (***)	Slow	Slow	Slow	Fast	Fast to Medium
Transient Withstand	Low	Low	Low	Low	Low
Resistance	Medium	Low to Medium	Medium	Low	Low
Agency Approvals	UL, CSA, TUV	UL, CSA, TUV	UL, CSA, TUV	UL, CSA	UL, CSA
Operational Uses	Multiple	Multiple	Multiple	One Time	One Time
Mounting/Form Factor	Surface Mount	Leaded	Leaded	Surface Mount	Surface Mount

(*) Maximum operating voltage in the series, parts may be used at voltages equal to or less than this value.

(**) Maximum interrupting rating at specified voltage which may be less than maximum operating voltage.

(***) Opening time is in relation to other forms of protection. A fast device will typically operate within three seconds at 200% of rated current.

SELECTION GUIDE WORKSHEET

3. Determine the opening time at fault.

Consult the Time-Current (T-C) Curve to determine if the selected part will operate within the constraints of your application. If the device opens too soon, the application may experience nuisance operation. If the device does not open soon enough, the overcurrent may damage downstream components.

To determine the opening time for the chosen device, locate the overload current on the X-axis of the appropriate T-C Curve and follow its line up to its intersection with the curve. At this point read the time listed on the Y-axis. This is the average opening time for that device. If your overload current falls to the right of the curve the device will open. If the overload current is to the left of the curve the device will not operate.

4. Verify ambient operating parameters.

Ensure that the application voltage is less than or equal to the device's rated voltage and that the operating temperature limits are within those specified by the device.

5. Verify the device's dimensions.

Using the information from the Designer's Guide page, compare the maximum dimensions of the device to the space available in the application.

LITTELFUSE CIRCUIT PROTECTION COMPARISON TABLE:

	Nano [®] SMF Fuse (Pg. 40-41)	PICO [®] II Fuse (Pg. 48-51)	2AGs (Pg. 55-57)	5x20mm (Pg. 62-70)	3AGs/3ABs (Pg. 58-61,71)	Midgets (Pg 76-84)
Operating Current Range	0.062 - 15A	0.062 - 15A	0.100 - 10A	0.032 - 15A	0.010 - 35A	0.100 - 30A
Maximum Voltage (*)	125V	250V	250V	250V	250V	600V
Maximum Interrupting Rating (**)	50A	50A	10,000A	10,000A	10,000A	200,000A
Temperature Range	-55°C to 125°C	-55°C to 125°C	-55°C to 125°C	-55°C to 125°C	-55°C to 125°C	-55°C to 125°C
Thermal Rerating	Low	Low	Low	Low	Low	Low
Opening time at 200% I_N (***)	Fast to Medium	Fast to Medium	Fast to Medium	Fast to Slow	Fast to Slow	Fast to Slow
Transient Withstand	Low to Medium	Low to Medium	Low to High	Low to High	Low to High	Low to High
Resistance	Low	Low	Low	Low	Low	Low
Agency Approvals	UL, CSA, MITI	UL, CSA, MITI	UL, CSA, MITI	CSA, BSI, VDE, MITI, SEMKO, UL	UL, CSA, MITI	UL, CSA
Operational Uses	One Time	One Time	One Time	One Time	One Time	One Time
Mounting/Form Factor	Surface Mount	Leaded	Leaded or Cartridge	Leaded or Cartridge	Leaded or Cartridge	Cartridge

(*) Maximum operating voltage in the series, parts may be used at voltages equal to or less than this value.

(**) Maximum interrupting rating at specified voltage which may be less than maximum operating voltage.

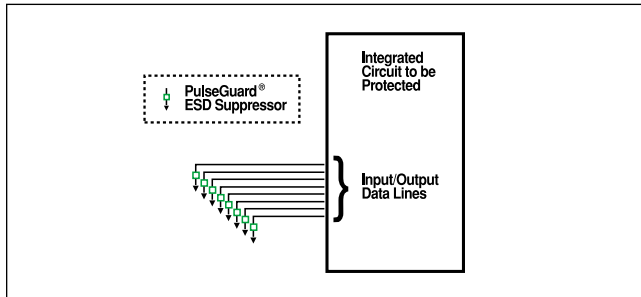
(***) Opening time is in relation to other forms of protection. A fast device will typically operate within three seconds at 200% of rated current.

PulseGuard® Suppressors

ESD Suppressor FACTS

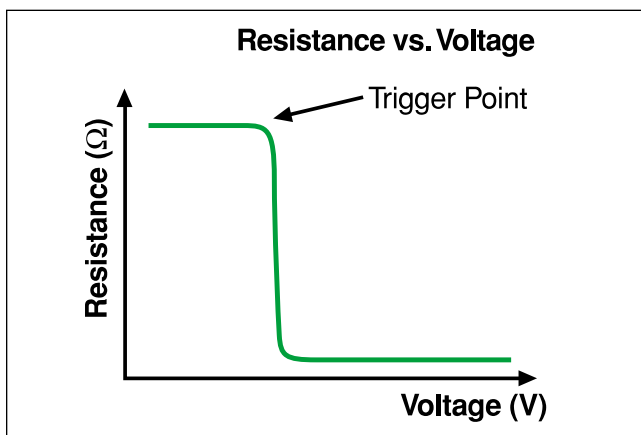
Electronic devices that rely on integrated circuitry are becoming more sensitive to the threats of electrostatic discharge (ESD) transient overvoltage events. Using the input/output communication ports as entryways, ESD pulses are able to pass from the outside of the electronic equipment to the I/O pins of the integrated circuit (IC) chips inside. The ESD transients are generated by people and transferred to the equipment during normal operation and maintenance.

IC's are typically manufactured to withstand ESD events up to 2,000 volts; however, ESD events often occur at levels exceeding 15,000 volts. Because of this protection discrepancy, reliability of the electronic equipment is compromised. The solution to this problem is to supplement the on-chip protection against ESD events by installing ESD suppressing components in parallel with the input/output communications lines as shown below.



Protection is provided by the PulseGuard suppressor as it transitions from a high resistance state to a low resistance state. In the "off" state, the high resistance causes the part to be electrically transparent to the circuit. After being triggered, the ESD protector shifts to the "on" state, becomes conductive, and shunts the ESD pulse from the signal line to ground. The amount of voltage that the system experiences due to ESD is thus minimized. After the ESD energy is dissipated, the PulseGuard suppressor "resets" itself to the high resistance "off" state.

A factor that complicates the protection of data communication lines is that signal transmission rates are increasing continuously. The information age has mandated the need for more communication links between electronic systems,

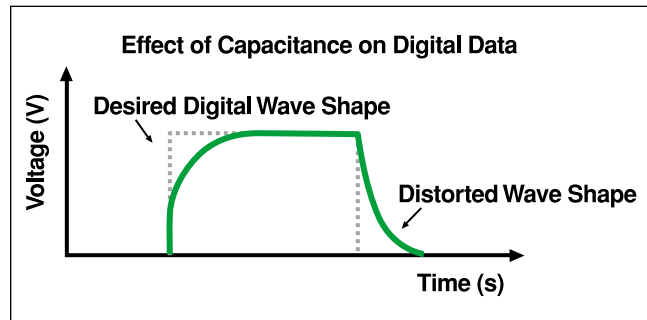


causing an associated explosion in the magnitude of data that must be handled. Data transmission rates, by necessity, have increased and will continue to increase.

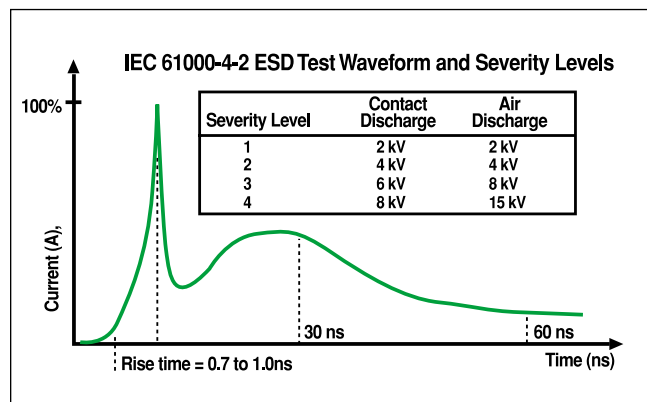
As the transmission rate of data increases, the inherent capacitance of the ESD suppressor becomes an issue. Capacitance will cause degradation to the signals that are passing along the data line. PulseGuard suppressors have less than 1 pF of capacitance and will not affect the signals. Typical effects on the data waveshape can be seen below.

For those applications where the speed of the data streams is approximately 100MHz or less, Littelfuse also offers electroceramic and silicon products for ESD protection. The MultiLayer Varistor (MLV) devices should be used to protect data lines where the speed of the signal is approximately 100MHz or less. The SP series contains the SP720, SP721, SP723, and SP724 devices. Both of these product families also provide protection against Electrical Fast Transients (EFT's) and have limited surge (8x20 μs) capabilities.

As an example, the SP724 would be the ideal solution for USB1.1 data lines, which transmit data up to speeds of 12 Mbps. The new USB2.0 serial bus will be able to transmit data at speeds up to 480 Mbps. For that application, the PulseGuard product would be the ideal solution.



Aside from reliability, the IEC 61000-4-2 test specification is an important design consideration. Created by the International Electrotechnical Commission (IEC), this specification provides the definition of the ESD waveform, severity levels, and the methodologies that are used to test the ability of electronic equipment to survive multiple ESD events. The following chart includes the waveshape and voltage level information relating to this specification.



PulseGuard® Suppressors

ESD Suppressor FACTS

Currently, electronic equipment manufacturers are required to certify that their equipment can survive testing to the IEC standard if they are selling that equipment into the European Union. Non-compliance is a prosecutable offense. Compliance is voluntary in the United States. Use of PulseGuard ESD suppressors will help our customers to meet this important specification.

LEAKAGE CURRENT: Until the PulseGuard suppressor transitions to the “on” state, it is electrically transparent to the circuit. Leakage current passing through the device is less than .1 μA .

INTERRUPTING RATING: ESD suppressors are not rated as current-breaking devices; however, PulseGuard suppressors are able to withstand the 45A that are present during worst case ESD discharges.

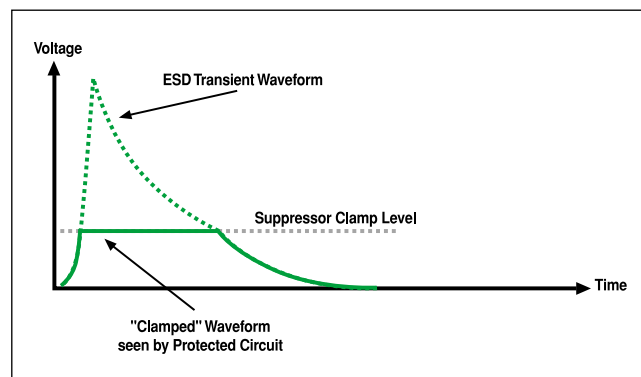
VOLTAGE RATING: PulseGuard suppressors are rated for use in operating environments up to 24 VDC.

TEMPERATURE RATING: The operating temperature range is -65°C to $+125^{\circ}\text{C}$. These devices do not operate as a result of thermal action; therefore, there is no derating necessary.

AGENCY APPROVALS: At this time, there are no applicable standards for ESD suppressor components. Nonetheless, PulseGuard suppressors have been subjected to all levels of severity of the IEC 61000-4-2 test specification using both the Contact Discharge and Air Discharge injection methods. In all cases, clamping of the ESD transient is provided.

RESISTANCE: While in the “off” state, the suppressors remain electrically transparent to the circuit. The measured resistance of the suppressors is 10 $\text{M}\Omega$, or greater.

TIME-VOLTAGE CHARACTERISTIC: Because the magnitude of the voltage and the time duration vary with the individual ESD event, a general form of this curve is shown below.



SUMMARY: The decision to use the surface mount suppressor or the connector array suppressor is left to the individual application. The ideal location is at the connector site, so that the ESD pulse is shunted to ground before the pulse enters the body of the electronic equipment. However, protection against the ESD threat will also be realized if the surface mount PulseGuard suppressors are installed as close as possible to the source of ESD. That is, on the PC board behind the connector so that the suppressor is the first device encountered by the ESD pulse after it passes through the connector.