Devices thru Material Innovation

NEC/TOKIN

Vol. 01

Permanent Magnets

PERMANENT MAGNETS

When using our products, the following Precautions should be taken.

1. Safety Precautions

(1) Large magnets exert an extremely powerful suction force (and sometimes a repelling force) on other magnets or metal scraps and other magnetically attracted substances. This force is capable of causing you to suddenly lose your balance or suffer serious injury if your hand or other parts of your body become trapped in the magnetic field while carrying or installing the magnets. Please take sufficient care when handling these magnets and always use appropriate tools.

(2) The sharp edges of magnets can cause injury to your fingers and hands especially. Please handle the magnets with care.

(3) When attaching magnets using a hollow-core coil, please be aware that the magnet may suddenly spring away from the coil. For safety's sake, place the magnet in the center area of the coil and secure it.

(4) Keep magnets out of the reach of children so as to avoid accidental swallowing. Should this occur, see a physician immediately.

(5) People whose skin is allergic to metals should avoid working with magnets, as this may cause an adverse reaction (rough, red skin).

(6) It is extremely dangerous to handle magnets near people who are wearing pa cemakers or other electronic medical devices. Take special care when using magnets around medical equipment, as it may impair normal operations.

(7) Magnets are generally susceptible to breakage. Please take care when handling any magnet, and be aware that magnet fragments can easily enter your eyes or cause other serious bodily injury.

2. Design Precautions

(1) Some anisotropic ferrite magnets, depending on the material, suffer reduced magnetism at low temperature.
Always check the performance of the magnet at the temperature at which it will be used.

(2) Ferrite magnets are often used for transmission; since the material cracks very easily, take measures to protect it from shock.

3. Handling Precautions

(1) If magnetized magnets are placed one on top of another, they can become diffi cult to pull apart or chip. Separate the magnets by using a spacer such as cardboard.

(2) If a magnetized magnet is allowed to be attracted to a metal plate or if two magnetized magnets are allowed to attract or repel each other, their magnetism may decrease, so use caution.

(3) If a magnetized magnet enters an AC or DC magnetic field, its magnetism may decrease.

(4) A magnetized magnet will attract debris such as iron filings, so unpack it from the case in a dust-free environment.

(5) A magnet can adhere to small magnetic bodies even if unmagnetized, so use caution in handling. In addition, when mounting a magnet in a precision motor, clean it after assembly before use.

(6) Each magnet has its own characteristic Curie temperature, depending on the material. If a magnet is heated to near the Curie temperature, it will lose its magnetism. If it is absolutely necessary to heat a magnet in an assembly process, please consult with us.

(7) If a magnet is held to, for example, a yoke by adhesion, select an appropriate adhesive and adhesion method so that mechanical distortion will not remain after adhesion. If the magnet is used while residual stress is still applied, the magnet may be cracked by even a slight shock.

(8) Magnets are not very resistant to shock and are easily cracked and chipped, so use caution. Cracking and chipping may cause deterioration of the magnet's characteristics, as well as loss of rigidity.

4. Others

(1) Please keep magnets away from magnetic tape, floppy disks, prepaid cards, CRTs, magnetic tickets, electronic watches and similar items. This can result in loss of recorded data or lead to malfunction due to magnetization.

(2) Please keep magnets away from electronic devices such as measuring boards and control panels, as this may cause them to malfunction or result in an accident.

(3) When cutting a magnet, please be aware that resulting magnetic dust can catch fire spontaneously due to the heat produced by friction during cutting. Kkeep magnets away from fire or flammable materials. As a precaution against fire, keep a dry chemical extinguisher, a supply of sand, and any other necessary equipment. Also, do NOT use an electric vacuum cleaner.

INTRODUCTION

NEC TOKIN, as a leading manufacturer of magnetic materials, has been engaged in R&D of permanent magnets. As a result NEC TOKIN has introduced a superior lineup of products such as "TMK" alnico magnet , Ferrinet® ferrite magnets and Lanthanet® rare-earth magnets. Today, application fields of these permanent magnets is extended to new industrial fields.

LANTHANET® is a super high-performance permanent magnet featuring high energy products. These magnets are best suited for electronic clocks, printers, motors, small-sized coreless motors vehicle applications, etc.

Ferrinet® is a ferrite magnet featuring high coercive force which is used in wide range of applications including speakers, communications equipment, motors, relays, etc. Especially wet anisotropic Ferrinet® is best suited of magnets for speakers and motors.

Plastic Bonded Magnets are manufactured by mixing ferrite magnets and can be manufactured in a variety of complex and irregular shapes and easily processed.

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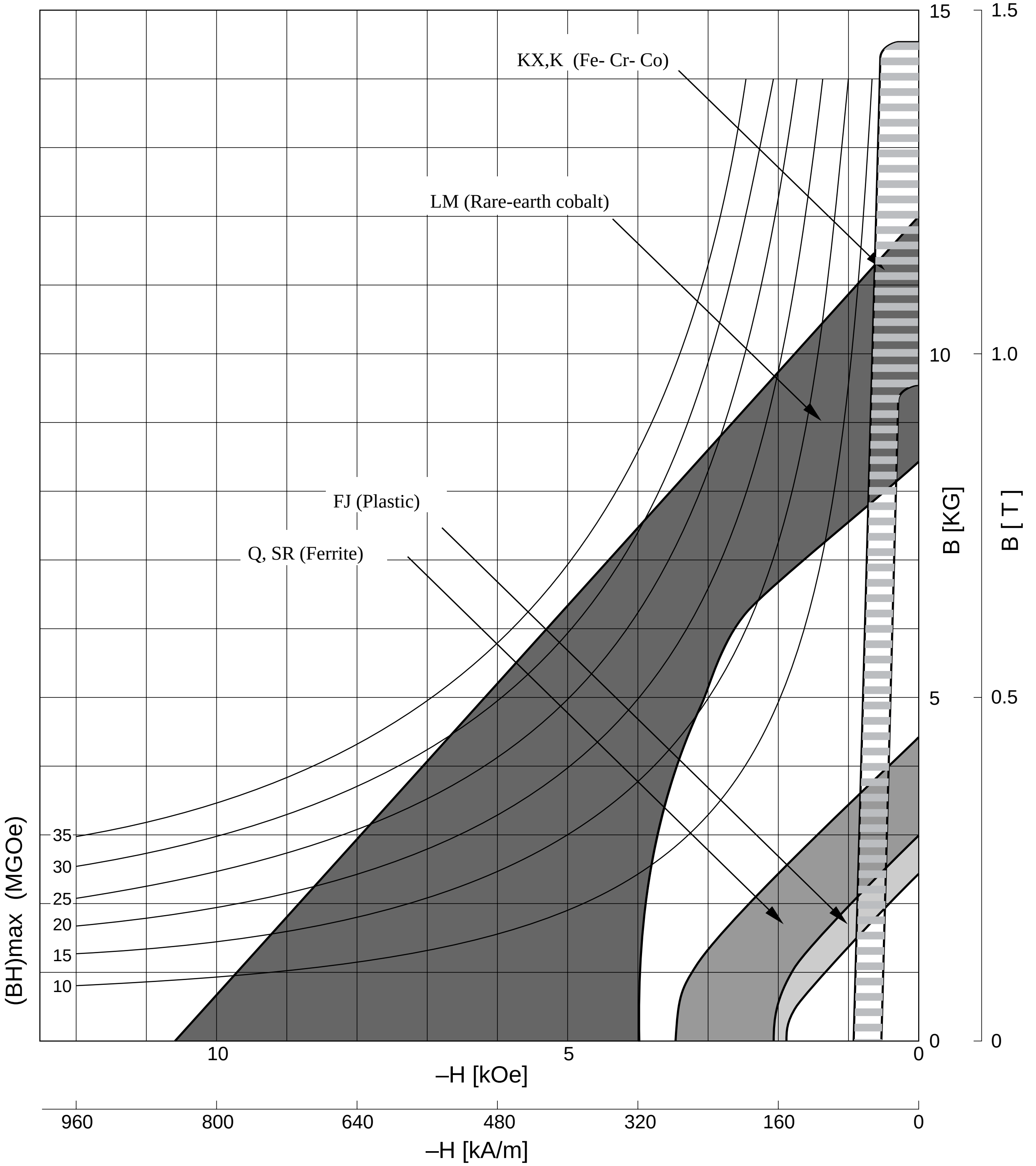

KX,K (Fe- Cr- Co)
LM (Rare-earth cobalt)
FJ (Plastic)
Q, SR (Ferrite)
(BH)max (MGOe)
35
30
25
20
15
10
15
10
5
0
B [KG]
1.5
1.0
0.5
0
B [T]
10
5
0
–H [kOe]
960
800
640
480
320
160
0
–H [kA/m]

Lanthanet® Rare-earth Magnets

Features

Table 1 presents features and applications for a variety of Lanthanet® magnets.
LM-19: Magnets with large coercive force and high energy products (Type 1-5).
LM-20FB—LM-32FH: Magnets with high Br and high energy product (Type 2-17).
Select the most suitable material that meets your needs.

Standard Material Characteristics and Applications

Table 1 Standard Material Characteristics

Material	Type	Residual flux density **Br Tesla (kG)**	Coercive force **H_{CB} kA/m (kOe)**	Maximum energy product **(BH)max kJ/m³ (MGOe)**	Intrinsk Coercive force **H_{CJ} kA/m (kOe)**	Density **D kg/m³**	Temperature coefficient **ΔBd/Bd %/ ˚C**	Electrical resistivity **ρ Ω – m**	Application
LM-19	Type 1-5	0.84 ~ 0.90 (8.4 ~ 9.0)	653 ~ 700 (8.2 ~ 8.8)	139 ~ 159 (17.5 ~ 20.0)	1194 ~ 2387 (15.0 ~ 30.0)	$8.3 \pm 0.15 \times 10^{-3}$	– 0.043	8×10^{-7}	Printers Motors CD actuators Instruments Traveling wave tube
LM-20FB	Type 2-17	0.96 ~ 1.04 (9.6 ~ 10.4)	517 ~ 716 (6.5 ~ 9.0)	151 ~ 183 (19.0 ~ 23.0)	597 ~ 1194 (7.5 ~ 15.0)	$8.3 \pm 0.15 \times 10^{-3}$	– 0.04	9×10^{-7}	Stepping motors Headphones Loudspeakers
LM-23FB	Type 2-17	1.01 ~ 1.08 (10.1 ~ 10.8)	517 ~ 756 (6.5 ~ 9.5)	175 ~ 207 (22.0 ~ 26.0)	597 ~ 1194 (7.5 ~ 15.0)	$8.3 \pm 0.15 \times 10^{-3}$			
LM-21B	Type 2-17	0.95 ~ 1.00 (9.5 ~ 10.0)	318 ~ 398 (4.0 ~ 5.0)	135 ~ 159 (17.0 ~ 20.0)	358 ~ 477 (4.5 ~ 6.0)	$8.3 \pm 0.15 \times 10^{-3}$	– 0.03	9×10^{-7}	Stepping motors
LM-25B	Type 2-17	1.00 ~ 1.07 (10.0 ~ 10.7)	318 ~ 398 (4.0 ~ 5.0)	151 ~ 183 (19.0 ~ 23.0)	358 ~ 477 (4.5 ~ 6.0)	$8.3 \pm 0.15 \times 10^{-3}$			Headphones Loudspeakers
LM-24F	Type 2-17	0.98 ~ 1.06 (9.8 ~ 10.6)	477 ~ 637 (6.0 ~ 8.0)	175 ~ 207 (22.0 ~ 26.0)	557 ~ 875 (7.0 ~ 11.0)	$8.2 \pm 0.15 \times 10^{-3}$	– 0.03	9×10^{-7}	Flat motors VCM Printers Relays
LM-24FH	Type 2-17	0.98 ~ 1.06 (9.8 ~ 10.6)	597 ~ 756 (7.5 ~ 9.5)	175 ~ 207 (22.0 ~ 26.0)	716 ~ 1432 (9.0 ~ 18.0)	$8.2 \pm 0.15 \times 10^{-3}$			
LM-26FH	Type 2-17	1.02 ~ 1.08 (10.2 ~ 10.8)	637 ~ 756 (8.0 ~ 9.5)	191 ~ 223 (24.0 ~ 28.0)	716 ~ 1432 (9.0 ~ 18.0)	$8.2 \pm 0.15 \times 10^{-3}$	– 0.03	9×10^{-7}	Printers VCM Servo motors
LM-30F	Type 2-17	1.07 ~ 1.15 (10.7 ~ 11.5)	477 ~ 637 (6.0 ~ 8.0)	199 ~ 247 (25.0 ~ 31.0)	557 ~ 875 (7.0 ~ 11.0)	$8.2 \pm 0.15 \times 10^{-3}$	– 0.03	9×10^{-7}	Relays Coreless motors CD actuators VCM Printers Flat motors
LM-30FH	Type 2-17	1.07 ~ 1.15 (10.7 ~ 11.5)	597 ~ 756 (7.5 ~ 9.5)	199 ~ 247 (25.0 ~ 31.0)	637 ~ 1432 (8.0 ~ 18.0)	$8.2 \pm 0.15 \times 10^{-3}$			
LM-26SH	Type 2-17	1.02 ~ 1.07 (10.2 ~ 10.7)	676 ~ 812 (8.5 ~ 10.2)	175 ~ 215 (22.0 ~ 27.0)	1592 ~ 2149 (20.0 ~ 27.0)	$8.2 \pm 0.15 \times 10^{-3}$	– 0.03	9×10^{-7}	Vehicle-use sensors Ignition coils Surface mounting devices
LM-30SH	Type 2-17	1.05 ~ 1.12 (10.5 ~ 11.2)	676 ~ 836 (8.5 ~ 10.5)	199 ~ 247 (25.0 ~ 31.0)	1592 ~ 2149 (20.0 ~ 27.0)	$8.2 \pm 0.15 \times 10^{-3}$			
LM-32F	Type 2-17	1.15 ~ 1.20 (11.5 ~ 12.0)	480 ~ 637 (6.0 ~ 8.0)	224 ~ 256 (28.0 ~ 32.0)	520 ~ 875 (6.5 ~ 11.0)	$8.2 \pm 0.15 \times 10^{-3}$	– 0.03	9×10^{-7}	Sensors Switches Coreless motors Servo motors Actuators
LM-32FH	Type 2-17	1.15 ~ 1.20 (11.5 ~ 12.0)	560 ~ 756 (7.0 ~ 9.5)	224 ~ 256 (28.0 ~ 32.0)	680 ~ 1194 (8.5 ~ 15.0)	$8.2 \pm 0.15 \times 10^{-3}$			

Demagnetization Curves

Demagnetization Curves of LANTHANET® (1)

LM-19

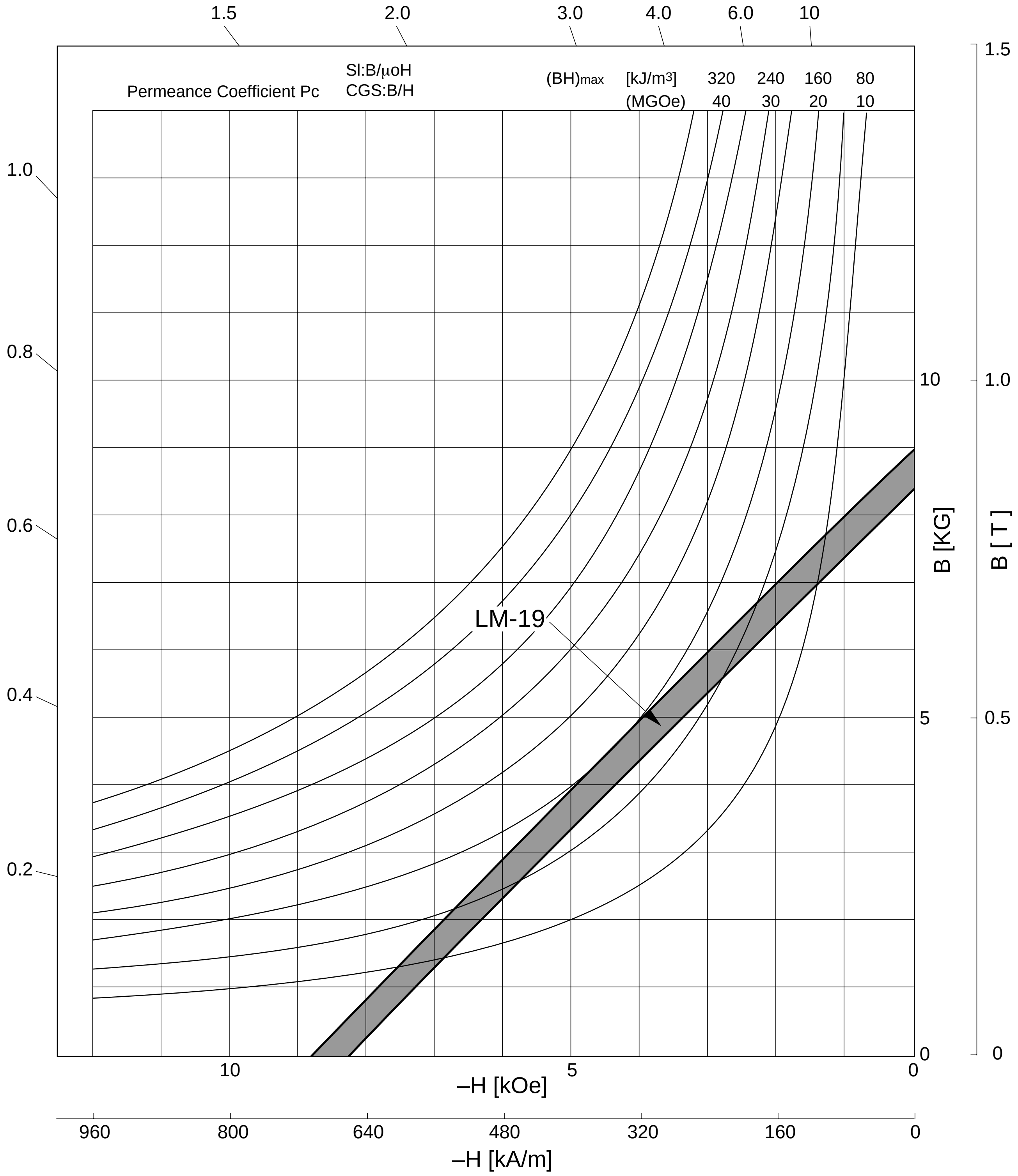


Fig. 1

Demagnetization Curves of LANTHANET® (2)

LM-20FB/LM-23FB

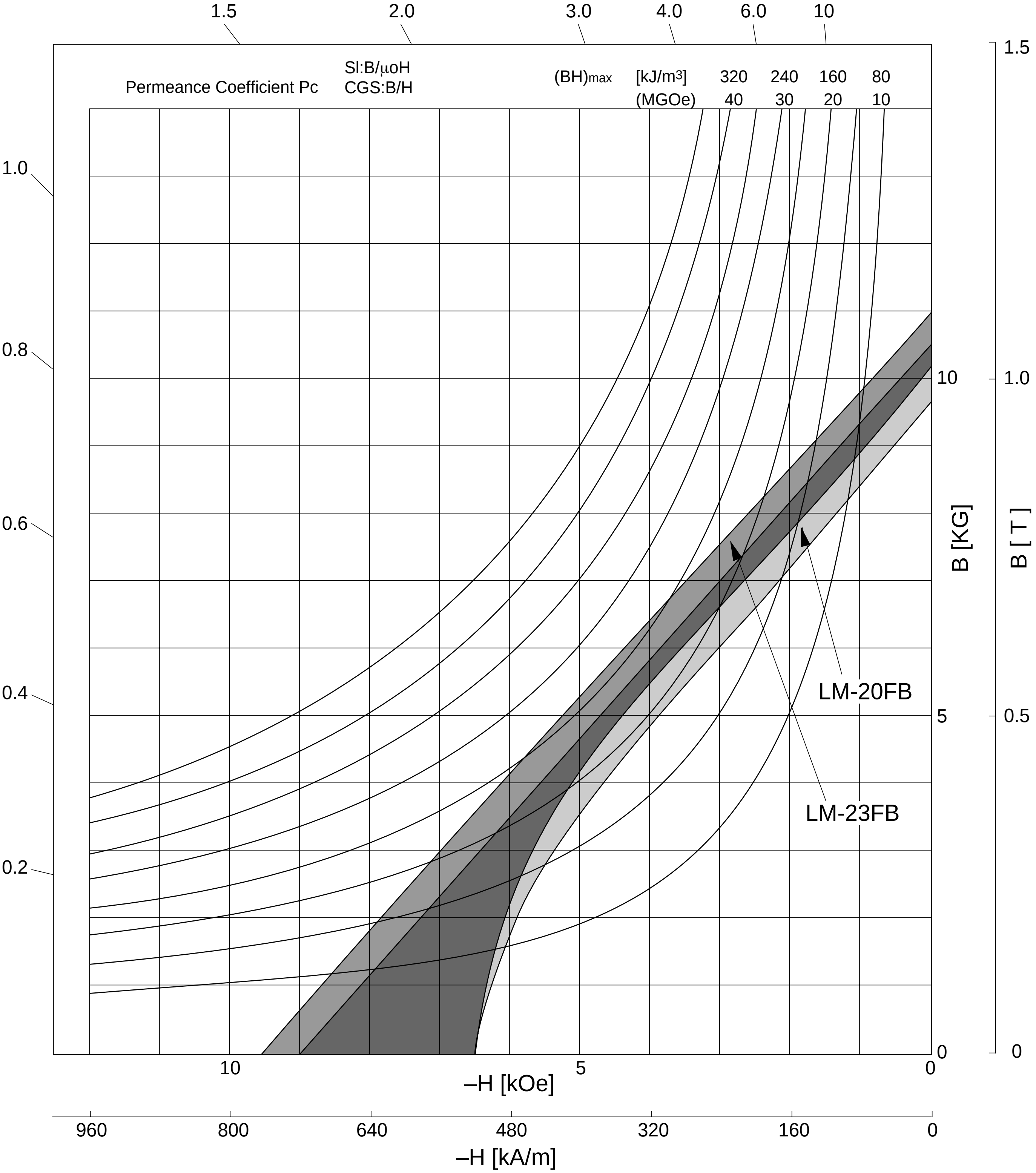


Fig. 2

- LM-20FB/LM-23FB are ideal for stepping motors, headphones and loudspeakers.

Demagnetization Curves of LANTHANET® (3)

LM-21B/LM-25B

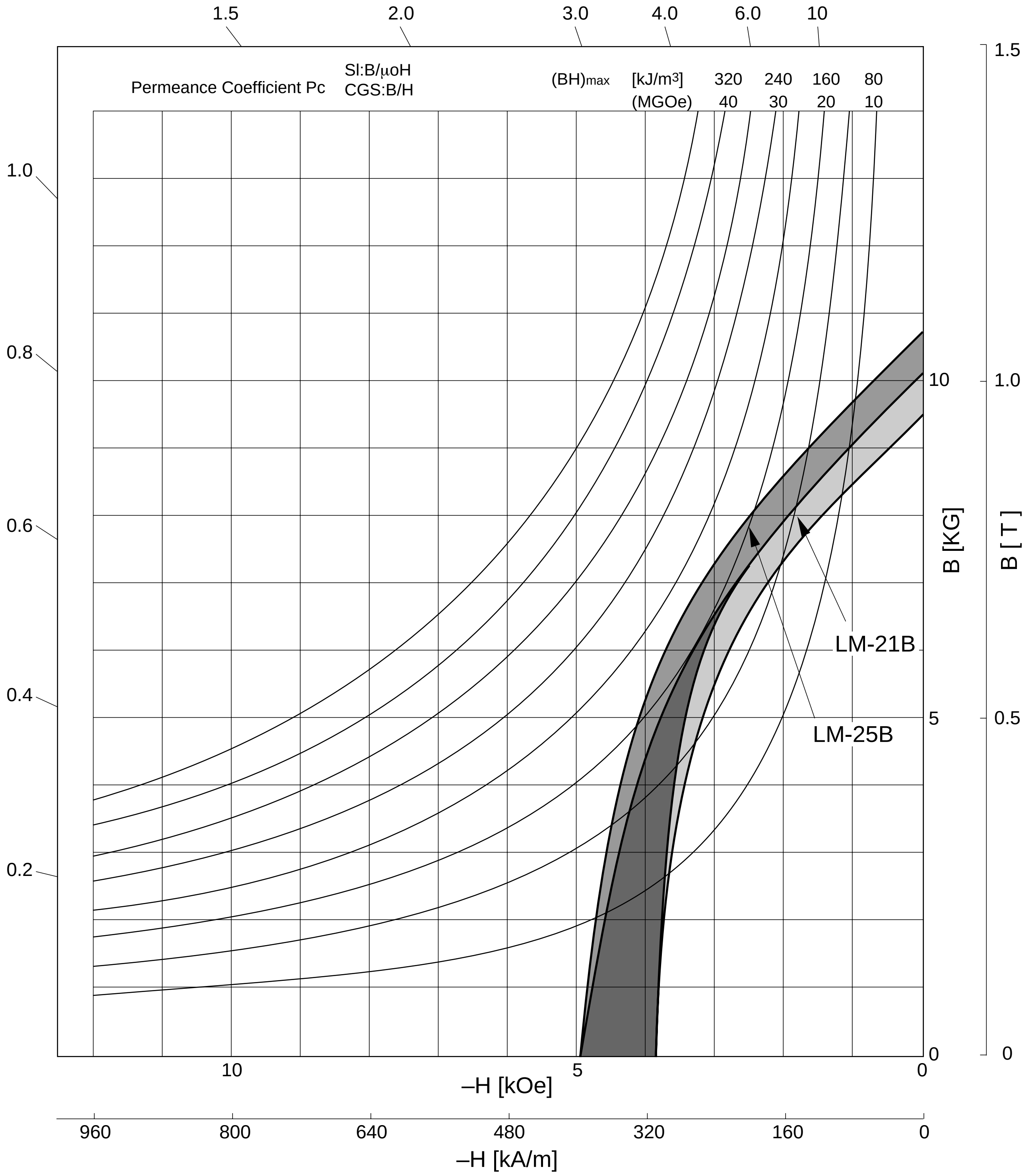


Fig. 3

- LM-21B/LM-25B are ideal for stepping motors, headphones and loudspeakers.
- Easy alternating-current demagnetization.

Demagnetization Curves of LANTHANET® (4)

LM-24F/LM-24FH

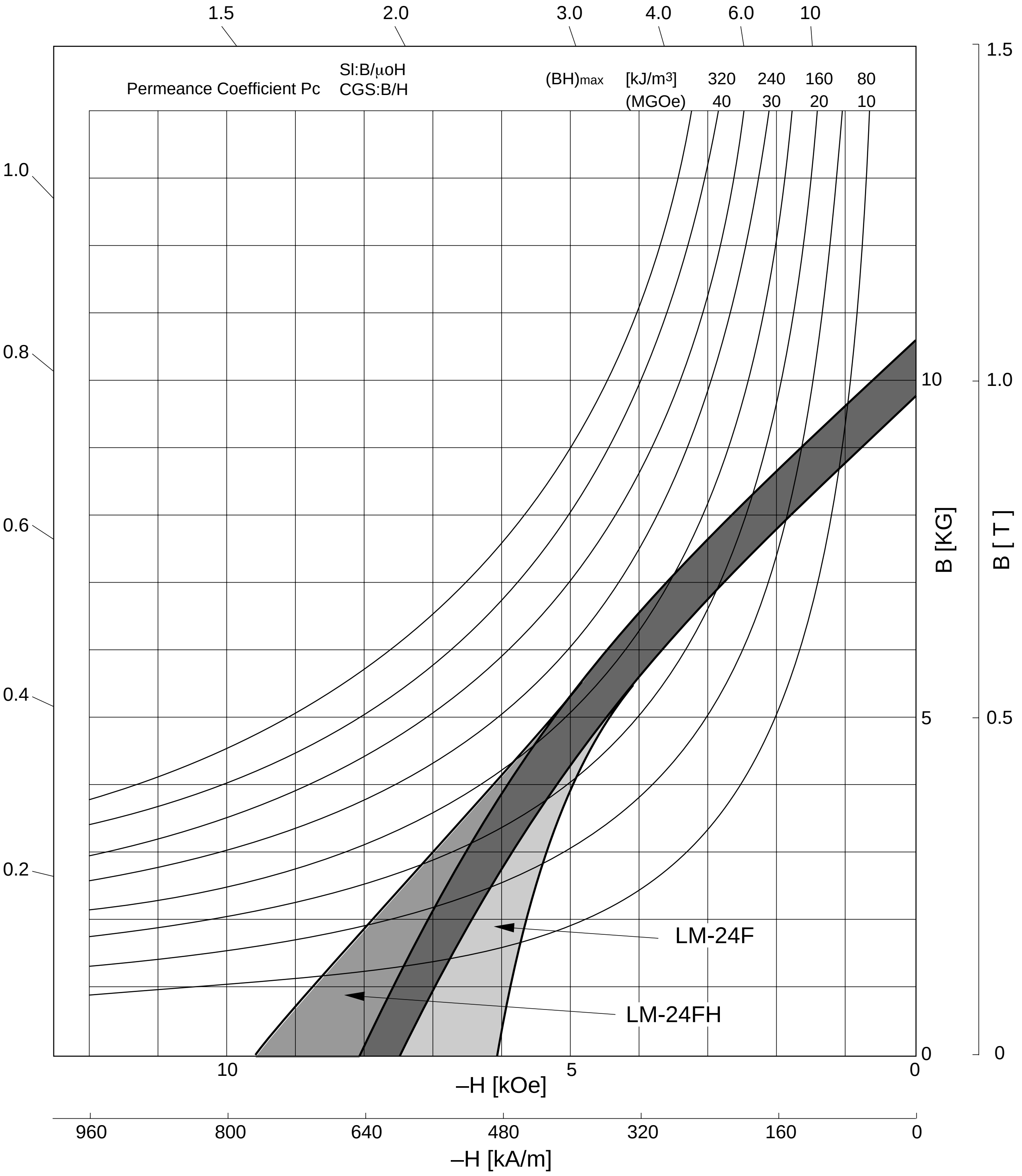


Fig. 4

- LM-24F is ideal for motors that use flat-ring type magnets.
- LM-24FH is ideal for printers.

Demagnetization Curves of LANTHANET® (5)

LM-26FH

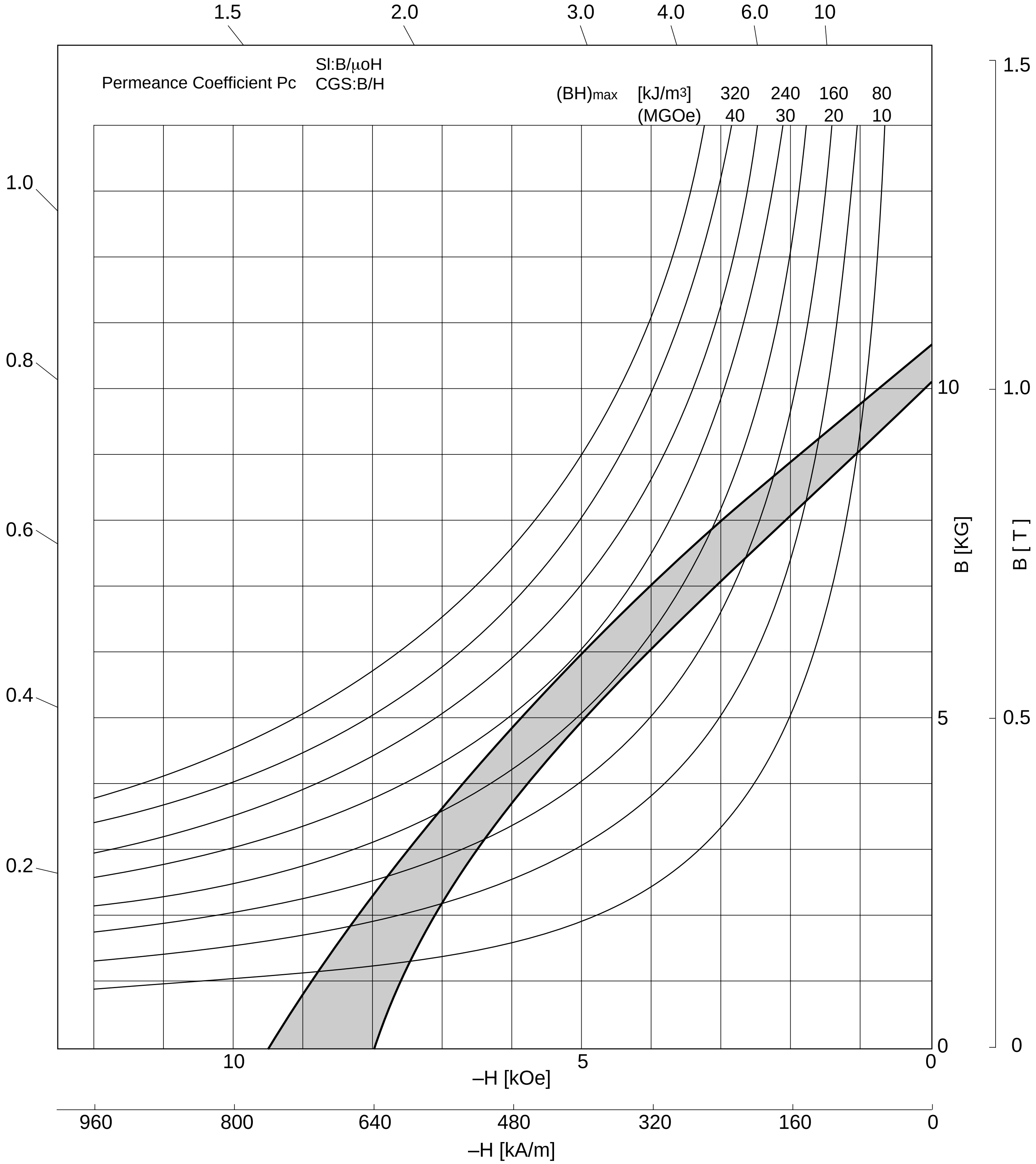


Fig. 5

- LM-26FH is ideal for printers, servo motors and VCM.

Demagnetization Curves of LANTHANET® (6)

LM-30F/LM-30FH

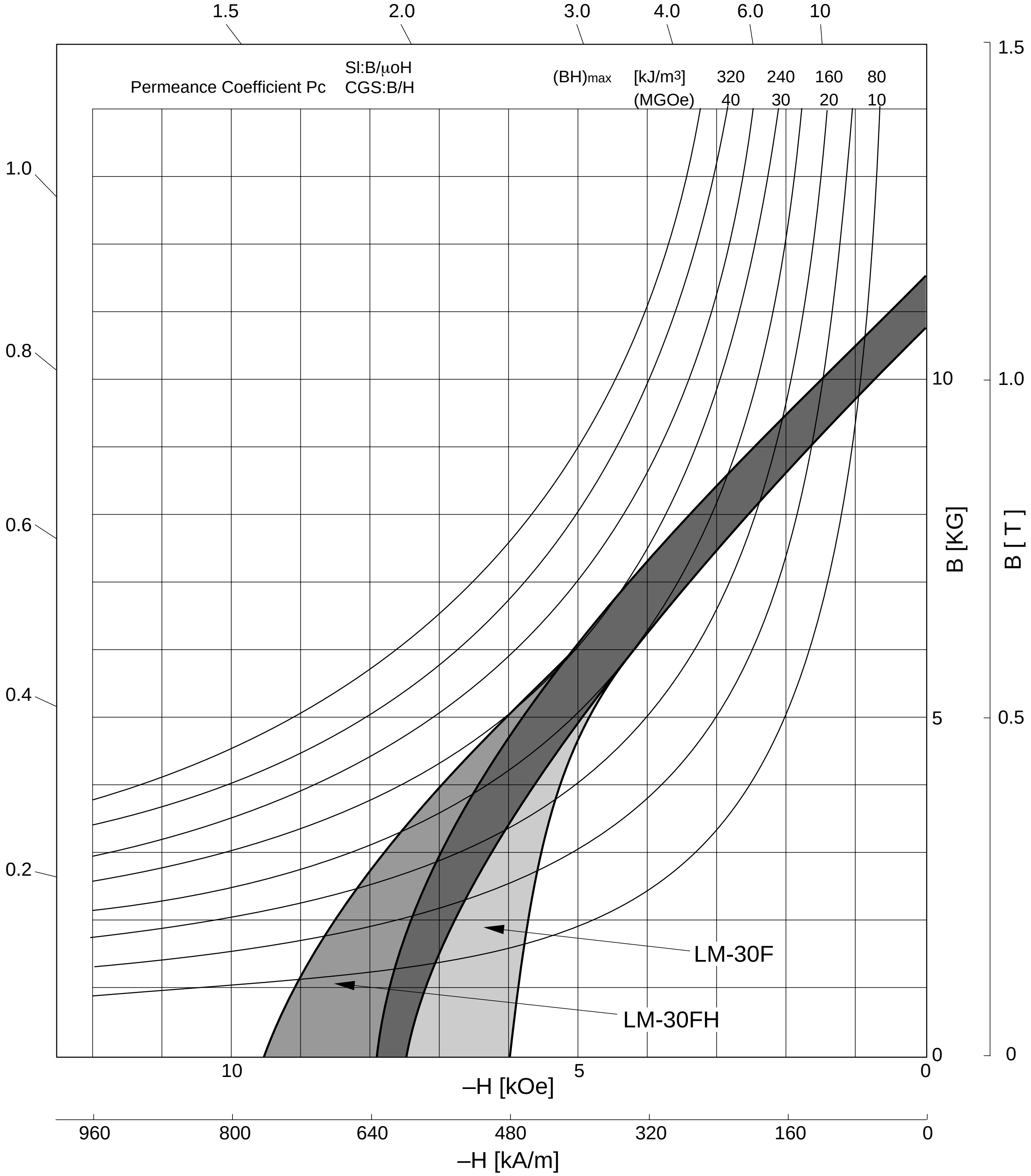


Fig. 6

- LM-30F is ideal for careless motors and relays.
- LM-30FH is ideal for flat motors and line printers.

Demagnetization Curves of LANTHANET® (7)

LM-32F/LM-32FH

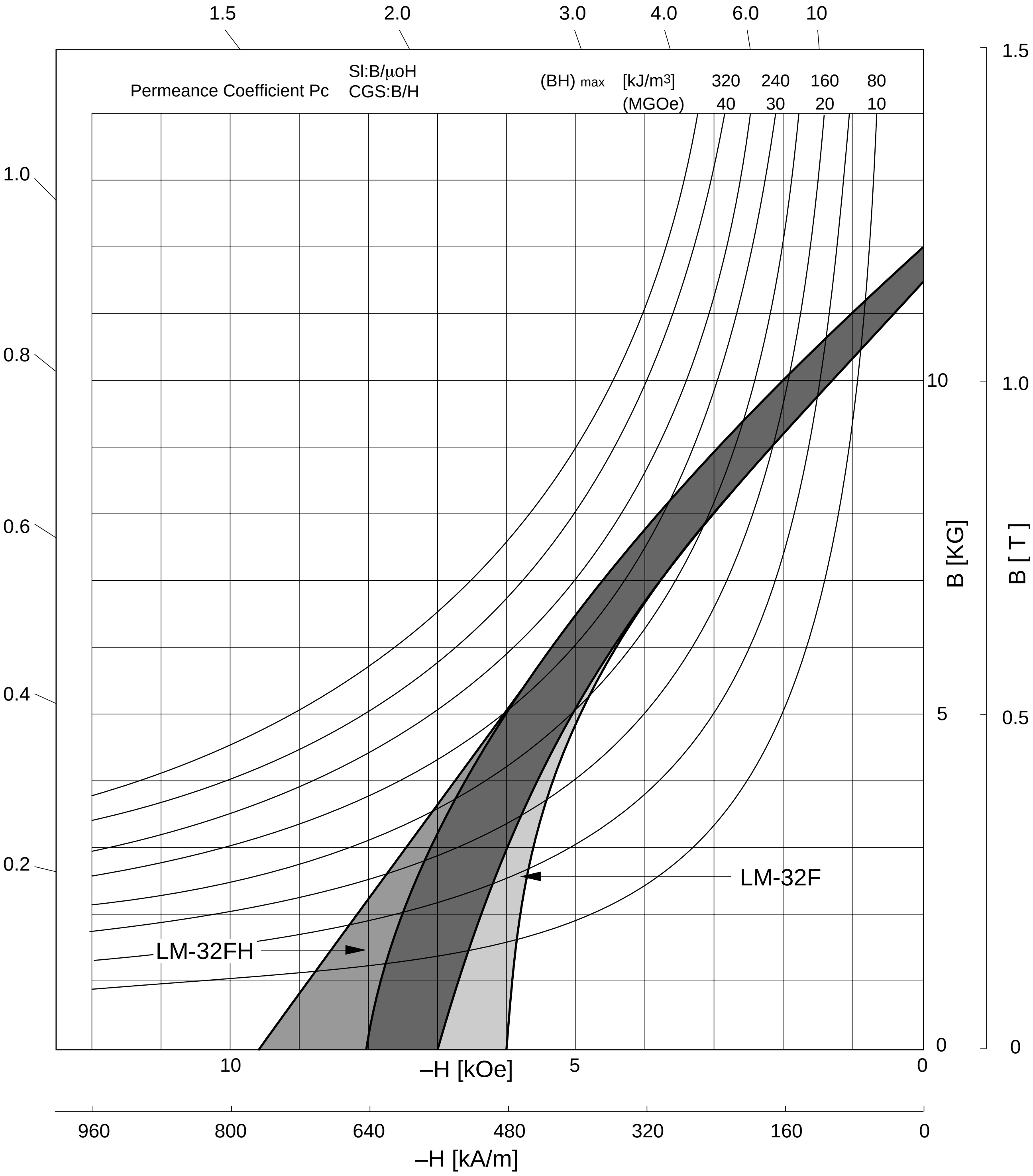


Fig. 7

- LM-32F is ideal for coreless motors and relays.
- LM-32FH is ideal for serbo-motors, HDDs, and latching magnets.

Demagnetization Curves of LANTHANET® (8)

LM-26SH/LM-30SH

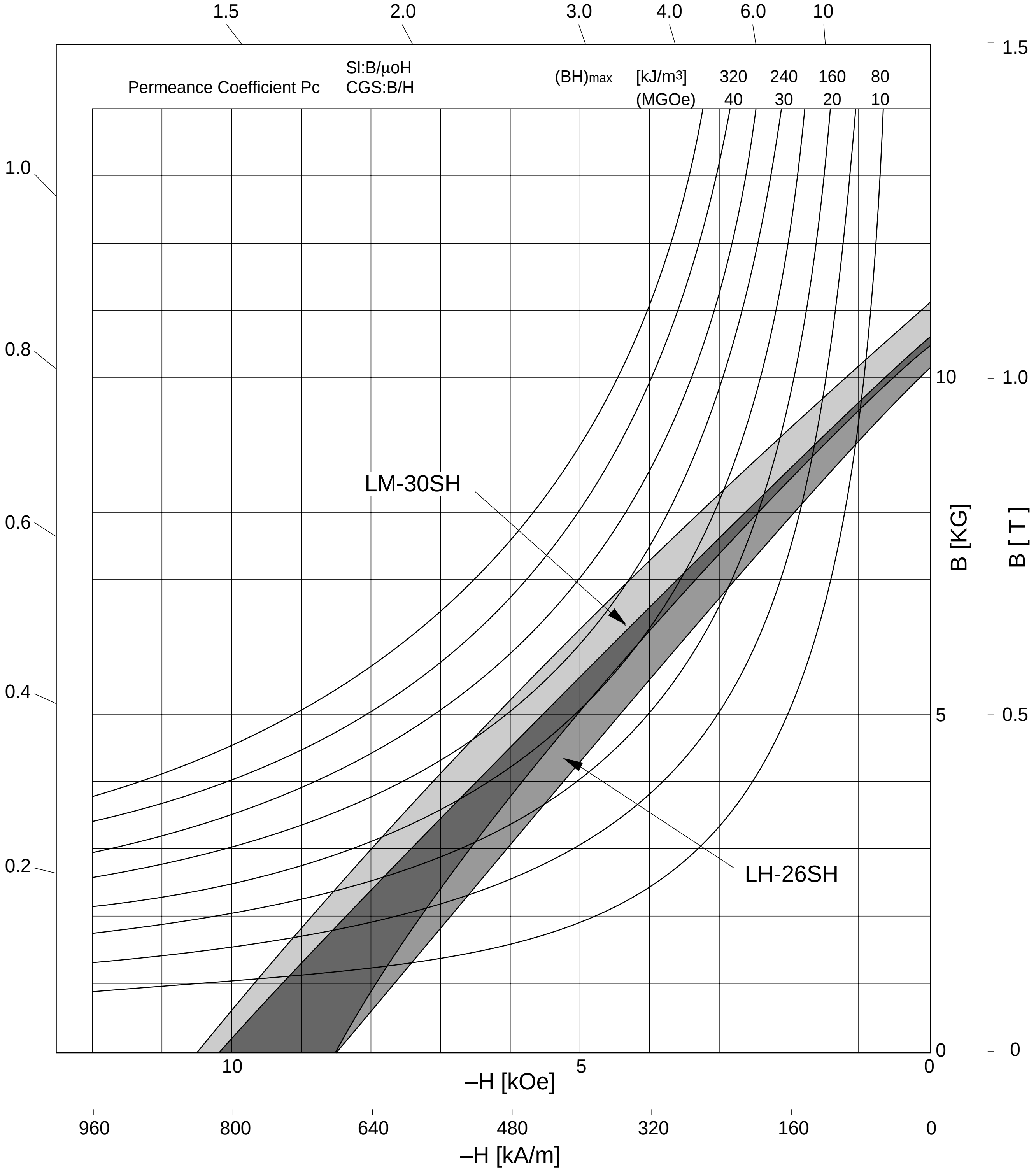


Fig. 8

- Vehicle applications: speed sensors, ABS sensors, ignition coils
- Surface mounting applications: relays, sounders

Demagnetization Curves of LANTHANET® (9)

LM-19

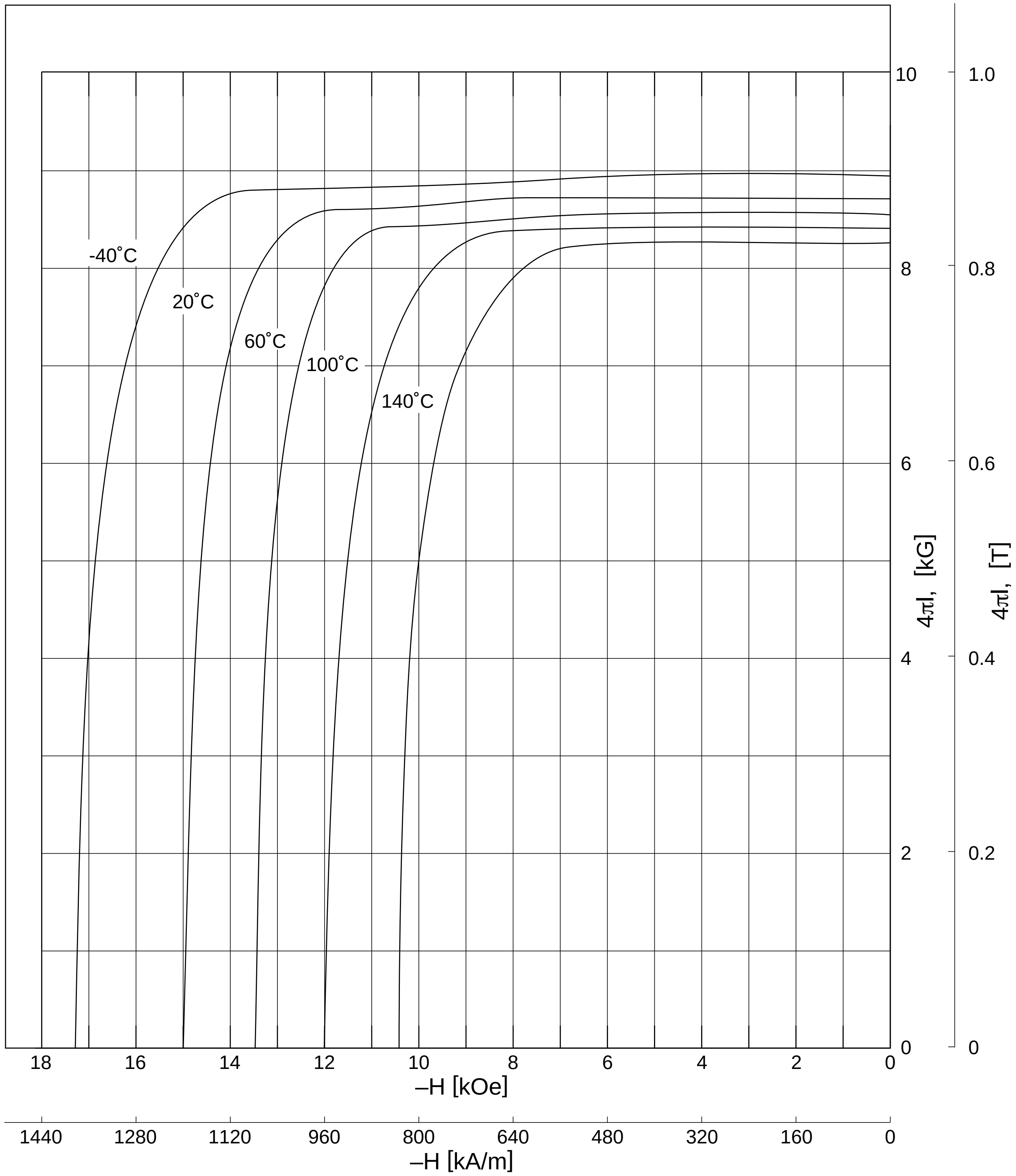


Fig. 9

Demagnetization Curves of LANTHANET® (10)

LM-19

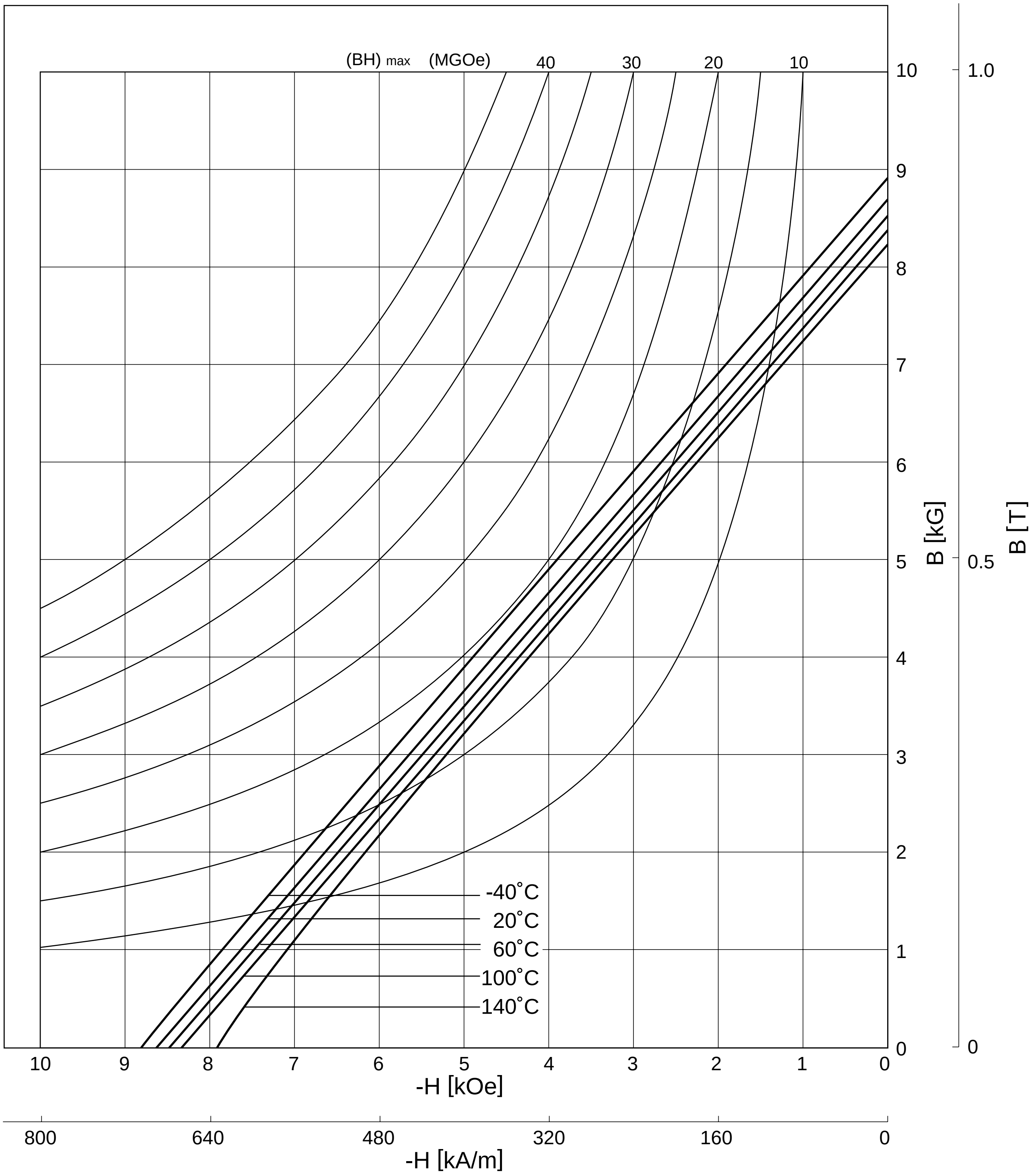


Fig. 10

Demagnetization Curves of LANTHANET® (11)

LM-30FH

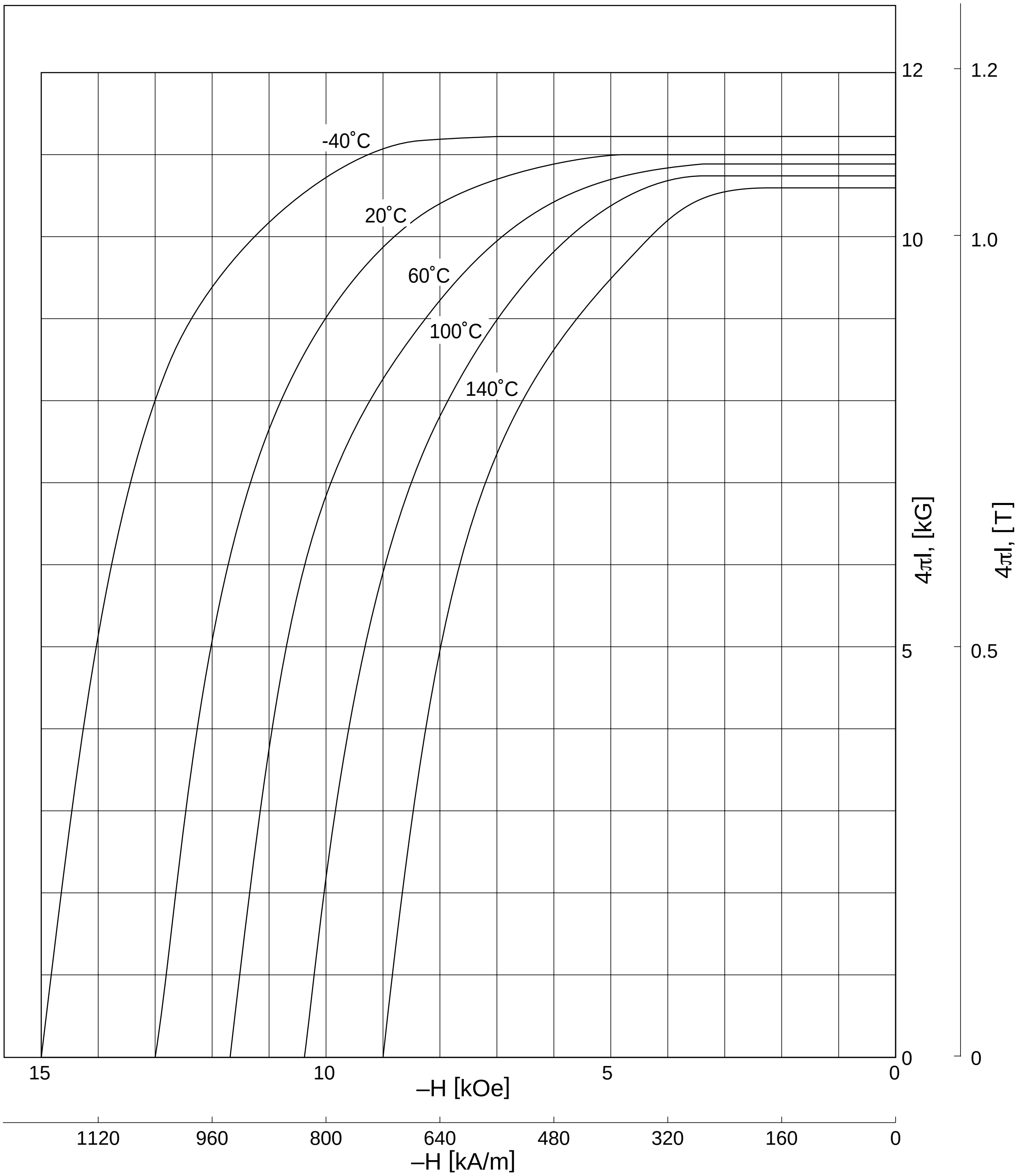


Fig. 11

Demagnetization Curves of LANTHANET® (12)

LM-30FH

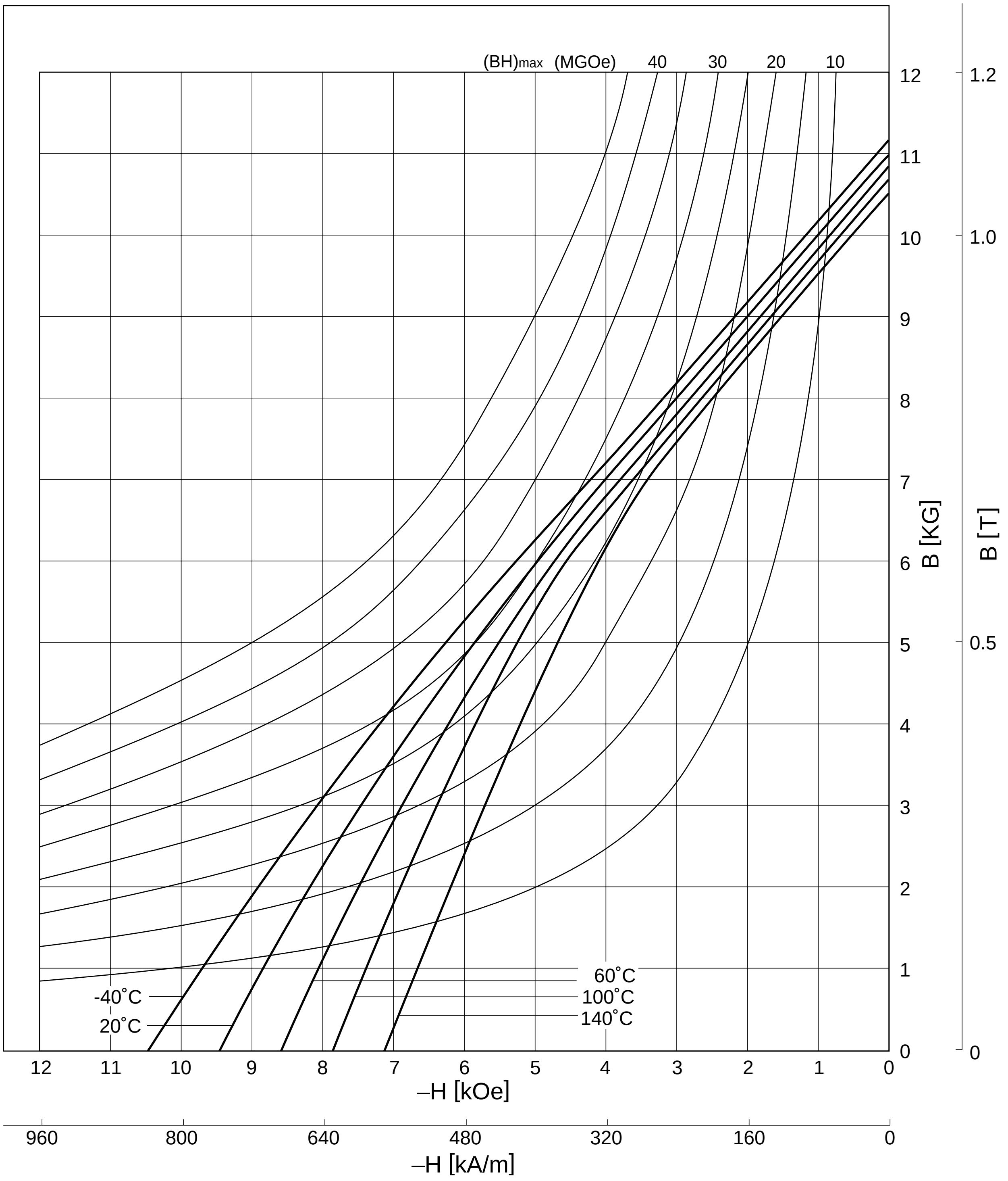


Fig. 12

Thermal Variations of Magnetic Characteristics

Irreversible Temperature Variations

The magnetic flux density generated by a permanent magnet decreases even without a change in the material if a permanent magnet is exposed to a high temperature and then returned to normal temperature. The variation ratio of the magnetic flux density gradually decreases commensurate to the time it is exposed to a high temperature and reaches saturation soon (30 minutes to 4 hours) after the variations stop. The variation ratio of the first magnetic flux density at this time is called the irreversible temperature variation ratio, and the variation width differs a great deal due to the holding temperature and magnet operating point position.

Figures 13-18 present approximate levels of irreversible temperature variations asainst the coercive force of LANTHANET®. It also shows that irreversible temperature variations are changed by the permanent magnet working point (P). In general, the larger the H_{CJ} and working point, the smaller the irreversible variations will be.

Irreversible Temperature Variations of LANTHANET® Fig. 13-18

LM19

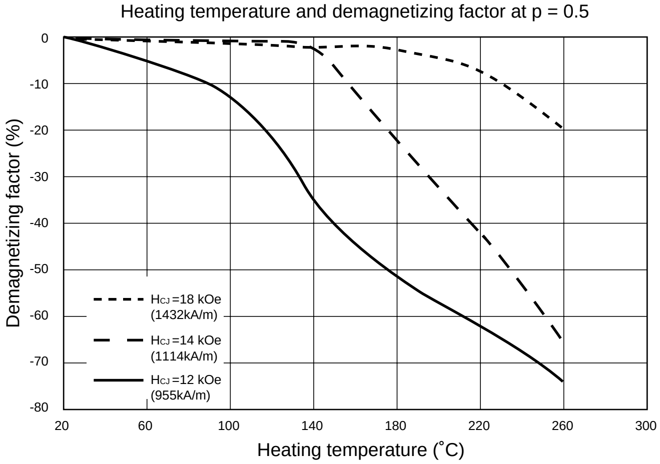


Fig. 13

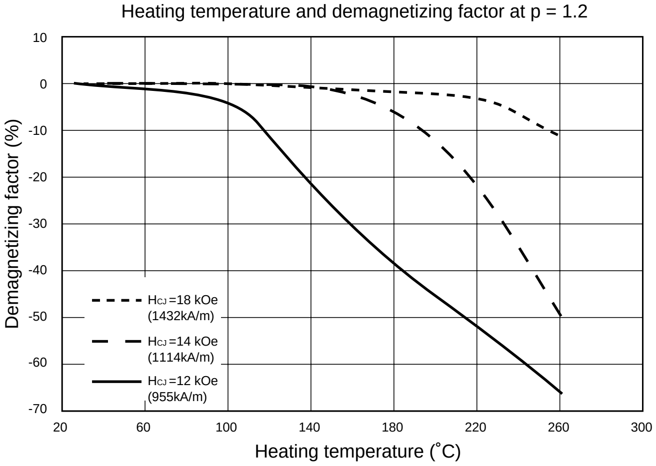


Fig. 14

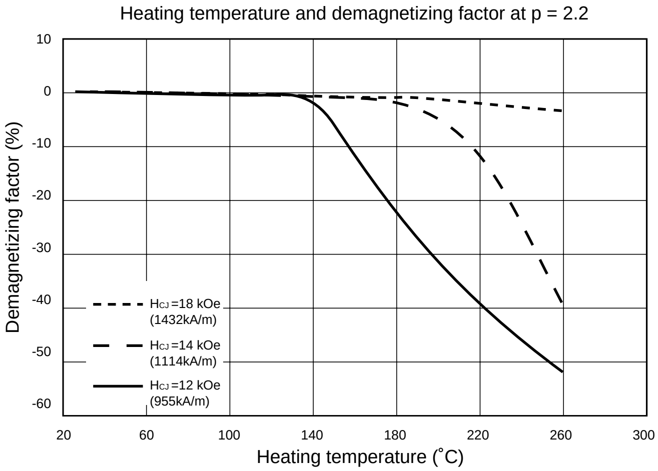


Fig. 15

LM24F, 24FH, 26FH, 26SH
LM30F, 30FH, 30SH

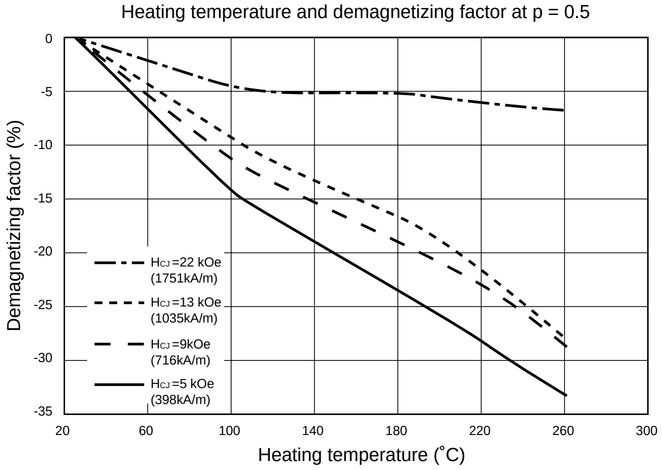


Fig. 16

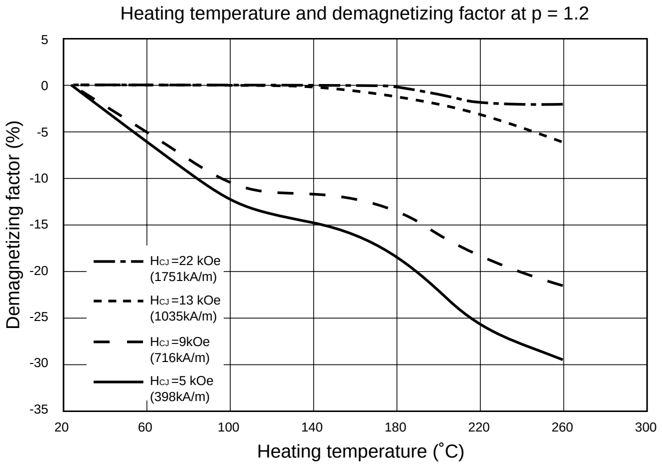


Fig. 17

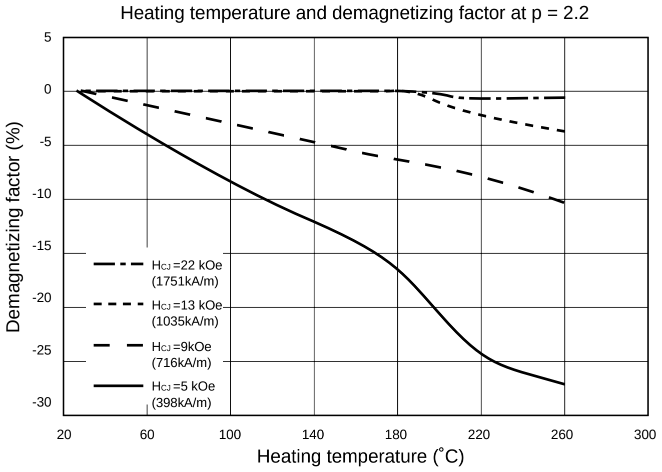


Fig. 18

Reversible Temperature Variations

Reversible variations of magnetic characteristics intrinsic to materials due to temperature variations are called reversible temperature variations. The variation factor of magnetic flux density per degree centigrade is called the reversible temperature coefficient. The reversible temperature variations are measured after completing irreversible temperature variations at each temperature.

The temperature coefficients in Table 1 show the reversible temperature variations. The LM-20BT, the magnetic material with the swallest temperature variations, is a specially made by NEC TOKIN.

Magnetizing Field

Compared with alnico and ferrite magnets, LANTHANET® requires a high magnetizing field, and the magnetic field requires careful attention. Table 2 shows the required magnetic fields for LANTHANET®.

NEC TOKIN also manufactures and sells various magnetizing equipment. Do not hesitate to consult NEC TOKIN about your magnetizing requirements and equipment.

Table 2 Required Magnetizing Field for LANTHANET®

Material	Magnetic field kA/m(kOe)
LM-19	1273 (16)
LM-21B,25B	1194 (15)
LM-20FB,23FB	1989 (25)
LM-24F,30F,32F	1592 (20)
LM-24FH,LM-26FH,30FH,32FH	1989 (25)
LM-26SH,30SH	3183 (40)

If the demagnetizing field to a permanent magnet product is large, a larger magnetic field may be required to compensate the field.

Precaution

The force of attraction of magnetized LANTHANET® is very large. Careless handling, such as joining or separating two pieces of LANTHANET®, or attaching it to a metal, may damage its edges.

Ordering Information

When placing an order with NEC TOKIN LANTHANET®, be sure to specify the following items.

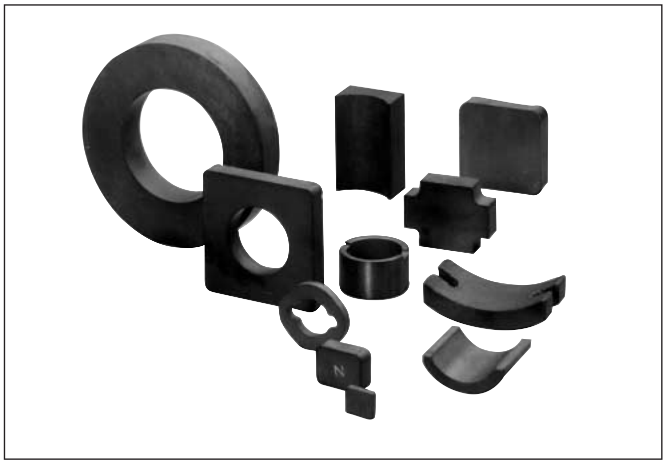
- Material and magnetic characteristics
- Dimensions and tolerances
- Whether or not magnetizing is necessary; direction of magnetization
- Whether or not grinding is necessary
- The purpose for which the material will be used
- The conditions under which the material will be used
- Any other relevant specifications

We welcome your queries regarding the shapes and dimensions of LANTHANET®. Please note however, the following limitations:

1) Upper limit of shape (monolithic construction)
Round shape : Less than ϕ65mm
Rectangular shape : Length - less than 75mm
Width – less than 30mm

2) Accuracy
Standard tolerance : ±1/10mm
Special tolerance : ±5/100mm
(Further accuracy depends on the shape of magnet)

Ferrinet® Ferrite Magnets



Standard Material Characteristics and Applications

Table 3 presents Magnetic and physical characteristics of various Ferrinet® Ferrite Magnets. There is no substantial difference between isotropic and anisotropic Ferrinet® Ferrite Magnets. However, Anisotropic Ferrinet® Ferrite Magnet is manufactured by rotating particle of micro powder by imposing external magnetic fields on them while molding the press and then forming crystalomagnetic axis in line according to the direction of the press. Therefore Anisotropic Ferrinet® is drastically improved in magnetic performance compared with Isotropic Ferrinet®. Its magnetic energy per unit weight is equal to that of cast magnets.

Wet Anisotropic Ferrinet® is manufactured by pressing mud powder within magnetic field. These magnets are classified into the following categories: Q6 (Barium type), SR-1H, SR-2H, SR-1, SR-3 and SR-4 (Strontium type). When you design magnetic circuit including magnets, if there is a large opening in the circuit, or the circuit receives great influence from external magnetic fields, or occurrence of irreversible demagnetization at considerably low temperature must be avoided, we suggest using SR-1H, SR-2H, SR-1, or SR-2 with great coercive force. When you need high magnetic flux density, we suggest you use SR-3 or SR-4 which has large energy product. Q10. SR-10, SR-20 and SR-30 are Dry Anisotropic Ferrinet® Ferrite Magnets which are manufactured by pressing dry magnetic powder in magnetic fields and ideal for mass production of small-sized products.

Table 4 presents application example of Ferrinet® Ferrite Magnets

Standard Material Characteristics

Table 3

Material	Classification		Residual flux density Br T (G)	Coercive force BHc kA/m (Oe)	Maximum energy product (BH)max kJ/m^3 (MGOe)	Density g/cm^3	Curie temperature (°C)	Thermal expansion coefficient 10^{-5}/°C
Q2	Isotropic	Ba type	0.20 ~ 0.24 (2000 ~ 2400)	127 ~ 160 (1600 ~ 2000)	7.1 ~ 10.4 (0.9 ~ 1.3)	4.9 ~ 5.0	460	0.9 ~ 1.5
Q6	Wet Anisotropic	Ba type	0.40 ~ 0.43 (4000 ~ 4300)	143.3 ~ 175 (1800 ~ 2200)	28.8 ~ 32.0 (3.6 ~ 4.0)	5.0 ~ 5.2	450	0.9 ~ 1.5
SR-1H	Wet Anisotropic	Sr type	0.34 ~ 0.37 (3400 ~ 3700)	254 ~ 279 (3200 ~ 3500)	22.4 ~ 27.2 (2.8 ~ 3.4)	4.75 ~ 4.95	460	0.9 ~ 1.5
SR-2H	Wet Anisotropic	Sr type	0.38 ~ 0.41 (3800 ~ 4100)	262 ~ 287 (3300 ~ 3600)	27.0 ~ 32.0 (3.4 ~ 4.0)	4.75 ~ 4.95	460	0.9 ~ 1.5
SR-1	Wet Anisotropic	Sr type	0.36 ~ 0.40 (3600 ~ 4000)	223 ~ 263 (2800 ~ 3300)	24.0 ~ 28.8 (3.0 ~ 3.6)	4.7 ~ 4.9	460	0.9 ~ 1.5
SR-2	Wet Anisotropic	Sr type	0.38 ~ 0.41 (3800 ~ 4100)	223 ~ 263 (2800~3300)	27.2 ~ 32.0 (3.4 ~ 4.0)	4.8 ~ 5.0	460	0.9 ~ 1.5
SR-3	Wet Anisotropic	Sr type	0.41 ~ 0.43 (4100 ~ 4300)	215 ~ 247 (2700 ~ 3100)	32.0 ~ 35.2 (4.0 ~ 4.4)	4.8 ~ 5.0	460	0.9 ~ 1.5
SR-4	Wet Anisotropic	Sr type	0.42 ~ 0.44 (4200 ~ 4400)	215 ~ 247 (2700 ~ 3100)	33.6 ~ 36.8 (4.2 ~ 4.6)	4.8 ~ 5.0	460	0.9 ~ 1.5
Q10	Dry Anisotropic	Ba type	0.36 ~ 0.40 (3600 ~ 4000)	143 ~ 175 (1800 ~ 2200)	26.3 ~ 29.5 (3.3 ~ 3.7)	4.8 ~ 5.0	460	0.9 ~ 1.5
SR-30	Dry Anisotropic	Sr type	0.34 ~ 0.38 (3400 ~ 3800)	222 ~ 255 (2800 ~ 3200)	20.6 ~ 24.5 (2.6 ~ 3.2)	4.8 ~ 5.0	460	0.9 ~ 1.5
SR-40	Dry Anisotropic	Sr type	0.36 ~ 0.39 (3600 ~ 3900)	218 ~ 251 (2750 ~ 3150)	23.0 ~ 27.9 (2.9 ~ 3.5)	4.9 ~ 5.1	460	0.9 ~ 1.5
SR-40S	Dry Anisotropic	Sr type	0.38 ~ 0.41 (3800 ~ 4100)	214 ~ 247 (2700 ~ 3100)	27.0 ~ 31.9 (3.4 ~ 4.0)	4.9 ~ 5.1	460	0.9 ~ 1.5
SR-40SS	Dry Anisotropic	Sr type	0.38 ~ 0.41 (3800 ~ 4100)	222 ~ 255 (2800 ~ 3200)	27.0 ~ 31.9 (3.4 ~ 4.0)	4.8 ~ 5.0	460	0.9 ~ 1.5
SR-40H	Dry Anisotropic	Sr type	0.36 ~ 0.39 (3600 ~ 3900)	254 ~ 287 (3200 ~ 3600)	24.6 ~ 29.5 (3.1 ~ 3.7)	4.8 ~ 5.0	460	0.9 ~ 1.5

Substance Characteristics

Items		Ranges
Specific heat	(J/Kg·K)	630~840
Thermal conductivity	(W/m·K)	~5.8
Transverse strength	(Kgf/cm^2)	5~9
Tensile strength	(Kgf/cm^2)	2~5
Thermal expansion coefficient	(10^{-6}/°C)	Anisotropic direction 14~15 Anisotropic square direction 9~10
Temperature coefficient	(⊿Br/Br/°C)	–0.18~–|0.20
	(⊿Hc/Hc/°C)	+0.20~+0.50
Vickers hardness		400~700
Electrical resistance	(Ω·cm)	$<10^4$
Recoil permeability	(μ rec)	1.05~1.20
Magnetizing power	(KOe)	10
required for magnetization	(A/m)	796

Application Example of Ferrinet® Ferrite Magnets

Table 4

Shape	Material	Applications
	Q2	Reverberation equipment Deflection remedy for televisions Pickup Generating lamps, measuring equipment
	Q2 Q10 SR-30 SR-40	Magnetic recording eraser Magnetic chuck Tools Microphones Electric guitars, telephones
	Q2 SR-30 SR-40	Magnetic doors Deflection remedy for televisions
	Q2 SR-30 SR-40	Motor for toys Precision motors Measuring equipment
	Q2 SR-1 SR-2 SR-30 SR-40	Teaching materials, toys Speed control Isolators Circulators
	Q2 SR-30 SR-40	Dynamic speakers Earphones, wipers Micromotors Polarized relays Traveling wave tubes
	Q6 SR-2H SR-3 SR-4 SR-30 SR-40	Speakers Motors
	Q2 Q6 SR-1 SR-2 SR-3 SR-30 SR-40	Reed switches Polarized relays

Demagnetization Curves

Demagnetization Curves of Isotropic and Wet Anisotropic Ferrinet® Ferrite Magnets

Fig. 19 and 20 presents demagnetization curves of various types of Ferrinet® Ferrite Magnets. It clearly shows the difference in performance of each Ferrinet®. Permeance coefficient (p=Bd/Hd) during operation should be lower than that of cast magnets. The value should ideally be between 1.5 and 3. The shape of magnet will be generally flattened.

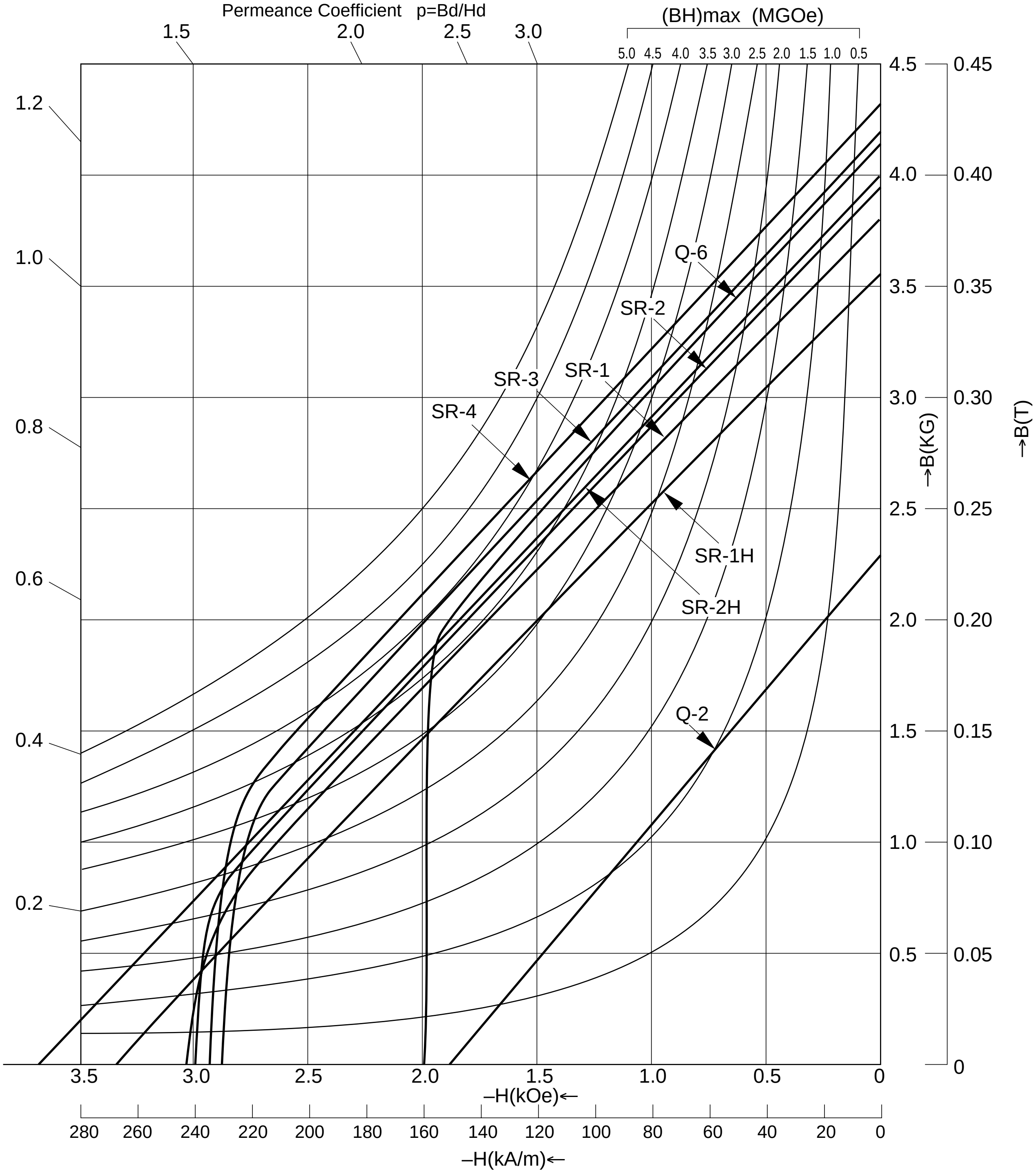


Fig. 19

Demagnetization Curves of Dry Anisotropic Ferrinet® Ferrite Magnets

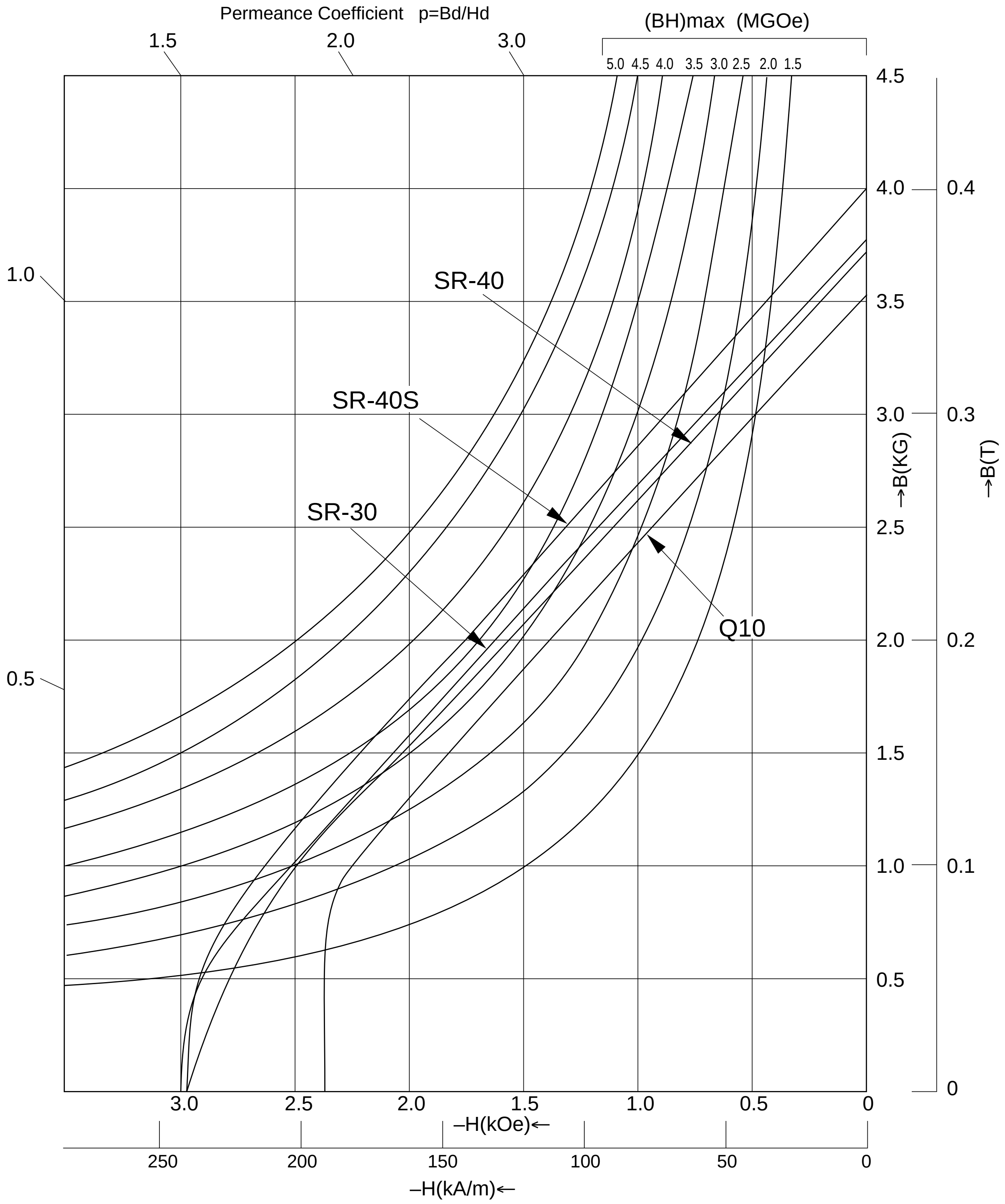


Fig. 20

Magnetic Stability

Magnetized materials tends to be demagnetized due to various external influences during operation. Therefore, it is necessary to perform various stabilizing processes when general magnets are used. However, Ferrinet® Ferrite Magnet has high magnetic stability, and its performance is hardly lowered by external disordered magnetic field and machinery shocks, thanks to its great coercive force.

Temperature Change
Table 21 and 22 presents temperature change in demagnetization curves of various Ferrinet® Ferrite Magnets.
Ferrite magnets has large temperature coefficient of remanence (apparent remanent magnetic flux density) and tends to receive irreversible demagnetization. Therefore, you must be careful of deciding operating point of magnets.

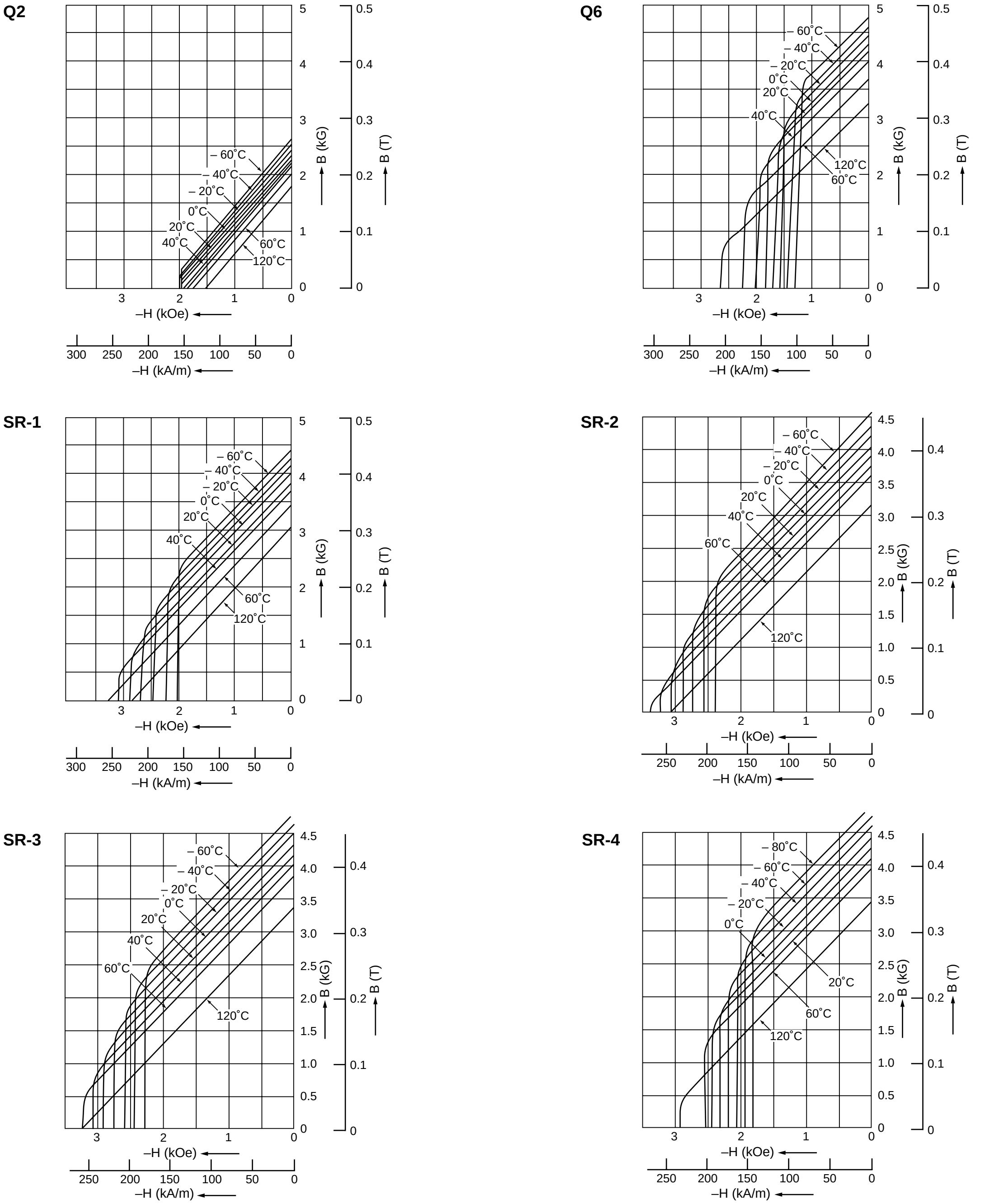


Fig. 21 Temperature Change in Demagnetization Curves of Various Ferrinet® Ferrite Magnets

Thermal Variations in Demagnetization Curves

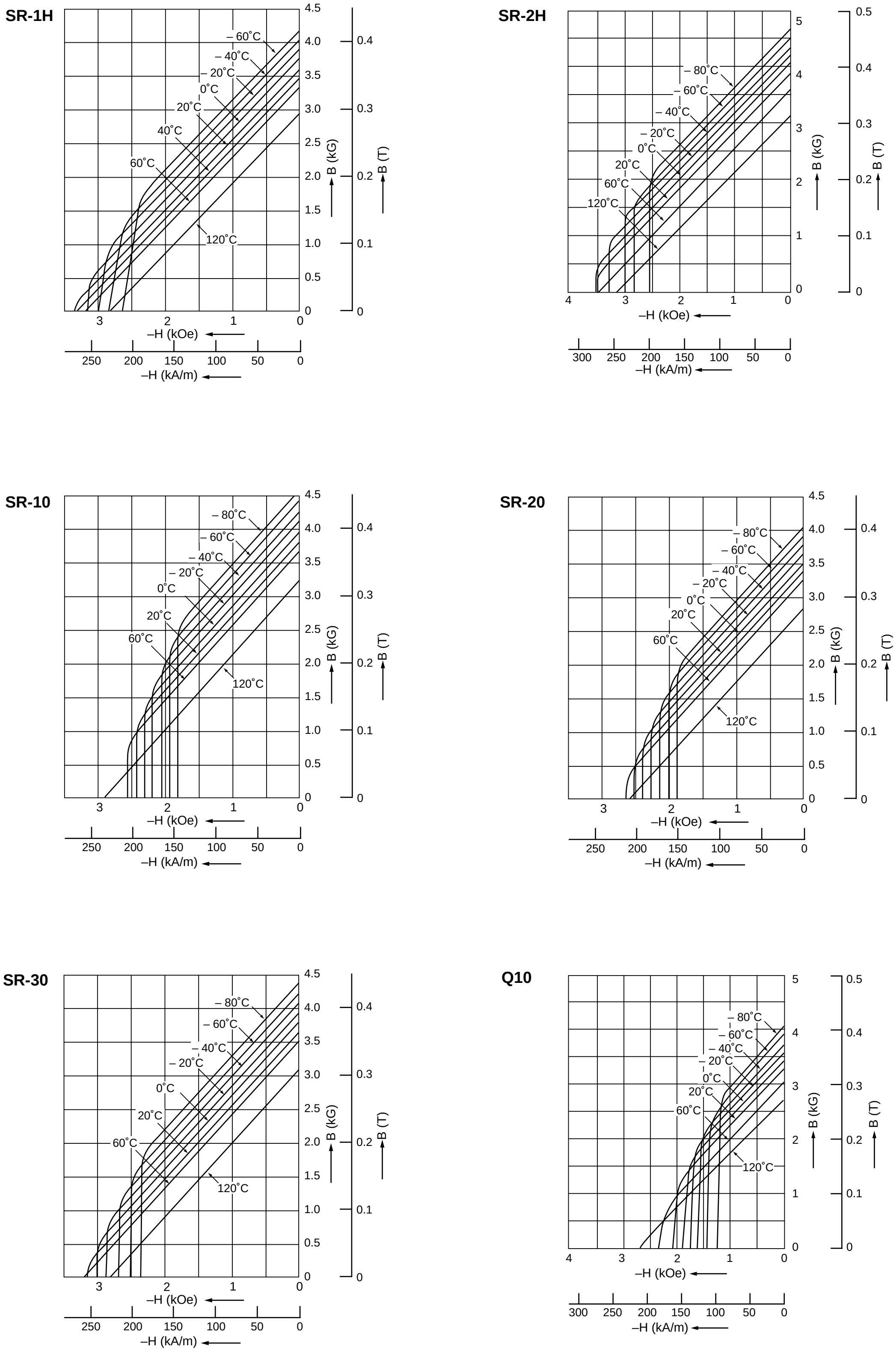


Fig. 22 Termal Variations of Demagnetization Curves of Various Ferrinet® Ferrite Magnets

1) Operating Point

Fig 23 presents an example of traveling (moving??) state of operating point due to temperature variations. A-B shows demagnetization curve of Q6 material at 20˚C. And A'-B' shows the curve of Q6 at -40˚C. And 2 operating state are shown in operating line X-0 and Y-0. In X-0 operating state, operating point of magnet irreversibly changes along X-0 line holding constant temperature coefficient (0.19%/˚C). However, in Y-0 operating state, where operating line is more slanted, the operating point will move from B to B' and that remanence value will be equivalent to the value of irreversible attenuation B''-B'. This difference will not be changed even when temperature returns to normal level. After exposed to irreversible demagnetization at low temperature, the operating point moves to B''' on Y-0 line.

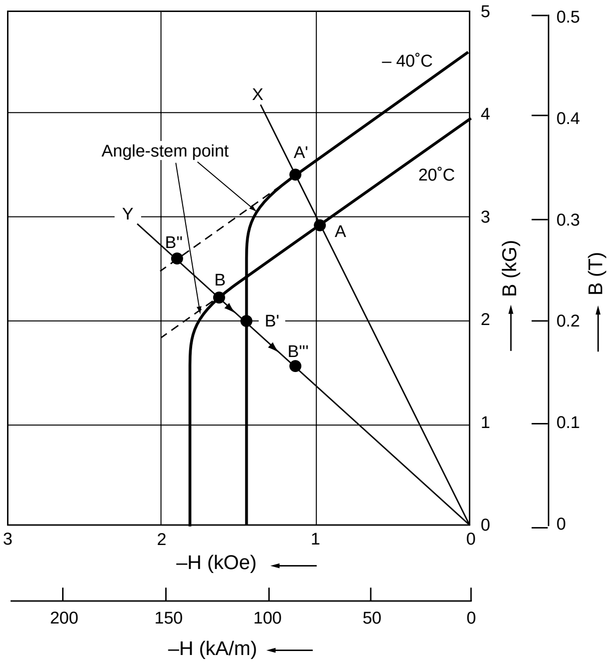


Fig. 23 Temperature vs. Demagnetization Characteristics

2) Remanence Curve at Operating Point (X-0, Y-0)

Fig. 24 presents variations of remanence value on operating line X-0 and Y-0 shown in Fig. 23 on another scale. It shows the irreversible demagnetization starts at low temperature starts from point C. This low-temperature demagnetization is affected by material or operating points (permeance coefficient). Therefore, when avoiding low-temperature demagnetization, material with large Hc such as Q2 should be used. Or permeance coefficient should be set high so that the operating point can be positioned above angle-stem point of demagnetization curve at minimum usage limit of the material in Quadrant II.

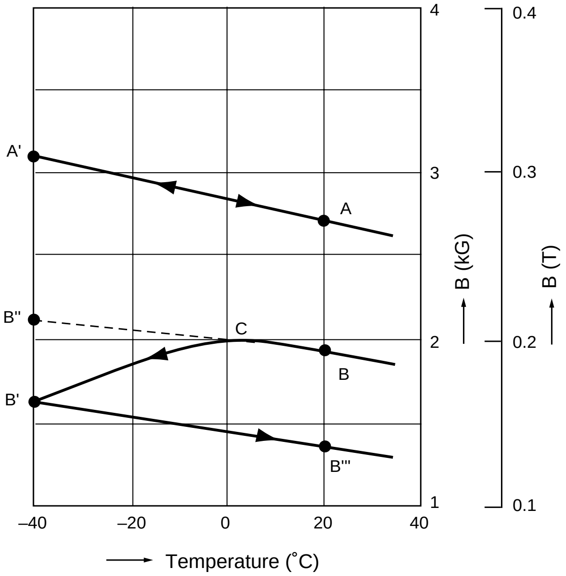


Fig. 24 Temperature vs. Remanence Characteristics

3) High-temperature Heating Characteristics

Fig. 25 presents remanence characteristics due to heating. Heating up to high-temperature causes few demagnetization although remanence will be irreversibly changed up to 400˚C (lower than Curie temperature).

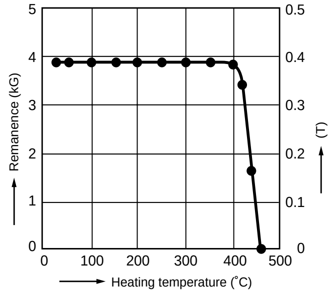


Fig. 25 High-temperature Heating vs. Remanence Characteristics

4) Remanence vs. Time

Fig. 26 presents change in remanence vs. time. It is hardly changed due to the time consumed.

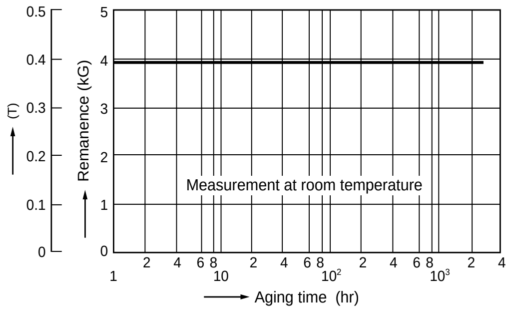


Fig. 26 Remanence vs. Time

Magnetization and Degaussing

Magnetization

As seen from hysteresis loop shown on Fig. 27, Ferrinet® requires much larger magnetizing field than metal magnets. And to reach saturation, magnetic field of more than 15,000 Oe must be added. But practically, approximately 10,000 Oe is enough.

a) As shown in Fig. 27, the hysteresis loop of isotropic Ferrinet®, regardless of directions, will be almost identical. And magnetic strength will not be changed whether Ferrinet® is installed before or after it is demagnetized. So it is very simple to handle.

b) As shown in Fig. 27, the hysteresis loop of anisotropic Ferrinet® will be completely different whether the direction of Ferrinet® is parallel or perpendicular to the magnetic direction during molding process. In general, the larger the azimuth ratio [Br (//)/Br(⊥), the better anisotropy anisotropic Ferrinet® shows. The anisotropy is between 3.0 and 4.0.

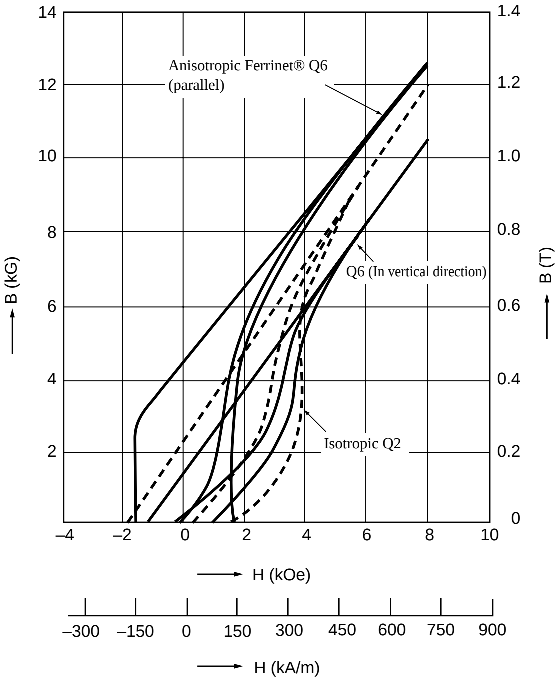


Fig. 27 Hysteresis Loop

Degaussing

Degaussing of every materials requires reverse magnetic field commensurate Hc, however, for any materials, reverse magnetic field is to high degaussing cannot be done completely. Therefore, to conduct large amount of degaussing safely, the best method is heat-degaussing (heat materials above Curie temperature).

Ordering Information

When placing an order with NEC TOKIN Ferrinet®, be sure to specify the following items.

- Material and magnetic characteristics
- Dimensions and tolerances
- Whether or not grinding is necessary
- Whether or not magnetizing is necessary; direction of magnetization
- Specify sealing and signs
- The purpose for which the material will be used
- Any other relevant specifications

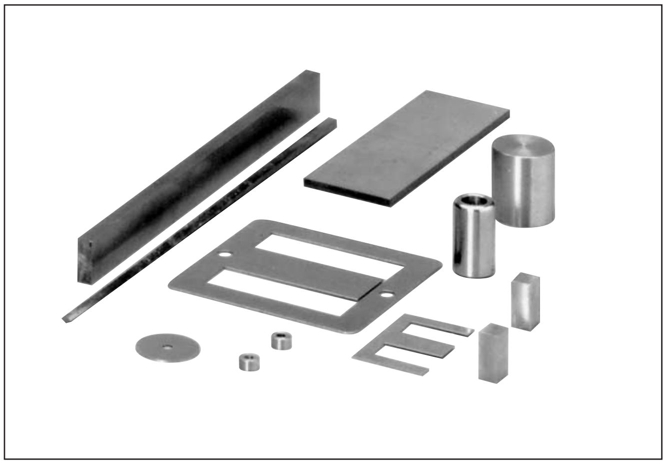
At NEC TOKIN, the type and dimensions of Ferrinet® are displayed as follows:

Initial : FM
Dimensions : Figures which stand for sizes are separated by X and placed in large-to-small order.

Example:

Square plate	Length
	Width
	Thickness
	Material
Round plate	Outer diameter
	Inside diameter
	Thickness
	Material

Fe-Cr-Co Magnets



Outline

Iron-Chromium-Cobalt Magnets were developed by Professor Kaneko of Tohoku University and have been manufactured by NEC TOKIN. Their most prominent features are that they have equivalent performance to that of casting alnico magnets and economical magnets that have low content of Co and can be easily machine processed. In addition these magnets have the following features:

1) Plastic working is possible. Therefore, can be manufactured into thin plate or fine wire. Further, machining such as cutting, die parching, and drilling, which allows free designing of magnetic circuit and applications for new fields.

2) Since Iron-Chromium-Cobalt Magnets are manufactured in the process of rolling and drawing, they have no gross porosity or cracks and cannot be cracked or broken due to shocks.

3) They can be soldered. Their magnetic characteristics does no change due to temperature rise during operation. However, when heated with temperature over 500˚C (eg. silver blazing), their magnetic characteristics will be degraded.

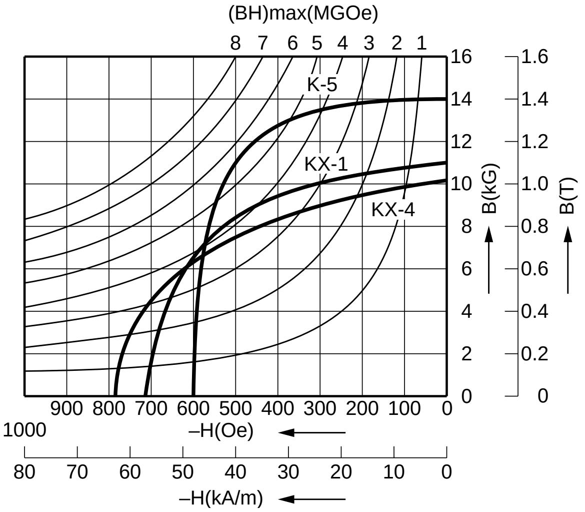


Fig. 29 Demagnetization Curve of Iron-Chromium-Cobalt Magnets

Standard Material Characteristics

Table 6 Magnetic Characteristics of Iron-Chromium-Cobalt Magnets

Material	Residual flux density	Coercive force	Maximum energy product	Optimum operating point			Remarks
	Br **T** **(kG)**	**Hc** **kA/m** **(Oe)**	**(BH)max** **kJ/m^3** **(MGOe)**	**Bd** **T** **(kG)**	**Hd** **kA/m** **(Oe)**	Permeance coefficient **p**	
KX-1	1.1 ~ 1.2 (11.0 ~ 12.0)	51.7 ~ 59.7 (650 ~ 750)	27.9 ~ 35.8 (3.5 ~ 4.5)	0.85 (8.5)	39.8 (500)	17	Alnico 6
KX-4	0.95 ~ 1.05 (9.5 ~ 10.5)	55.7 ~ 63.7 (700 ~ 800)	25.5 ~ 33.4 (3.2 ~ 4.2)	0.70 (7.0)	43.8 (550)	14	
K-5	1.35 ~ 1.45 (13.5 ~ 14.5)	39.8 ~ 47.7 (500 ~ 600)	43.8 ~ 55.7 (5.5 ~ 7.0)	1.3 (13.0)	35.8 (450)	29	Alnico 5-7

Mechanical and Physical Characteristics

Mechanical and physical characteristics of Fe-Cr-Co Magnets shown in table 7 is measured as solution treatment and mag, final heat treatment. Thermal expansion coefficient is average of temperature range from 0 to 500˚C.

Table 7 Mechanical and Physical Properties of Iron-Chromium-Cobalt Magnets

	Mechanical properties			Physical properties			
	Hardness **Hv**	Tensil strength **N/mm^2**	Elongation **(%)**	Density **(kg/m^3)**	Electric resistance **(μΩ • m)**	Thermal expansion coefficient **(/˚C)**	Curie tempera-ture **(˚C)**
After solution treatment	200 ~ 230	637 ~ 735	10 ~ 15				
After mag, final heat treatment	450 ~ 500	441 ~ 490	0	7.8×10^{-3}	0.62	14×10^{-6}	670

Magnetic Stability

Generally speaking, when heating permanent magnet with high temperature, magnet materials appear irreversible demagnetization and also appear reversible demagnetization along with temperature change. Once you heat the material above operational temperature and the irreversible demagnetization is finished, you have only to pay attention to reversible change responding to temperature coefficient. Fe-Cr-Co Magnets do not generate irreversible demagnetization under temperature below 500˚C as shown in Fig. 30. However, when used under temperature above 500˚C, they show drastic decrease in flux value. (Keep magnets within each temperature range for an hour and measure flux value after temperature is lowered to room temperature). Therefore, magnets can be soldered but magnetism will be degradated when silver-soldered.

Table 8 presents rate of temperature change in Br of permanent magnetic materials under temperature range below 400˚C where degradation of irreversible characteristics is not generated. Fe-Cr-Co magnets show a bit larger rage of change compared with alnico magnets but much smaller compared with ferrite magnets. In most cases, these value can be ignored.

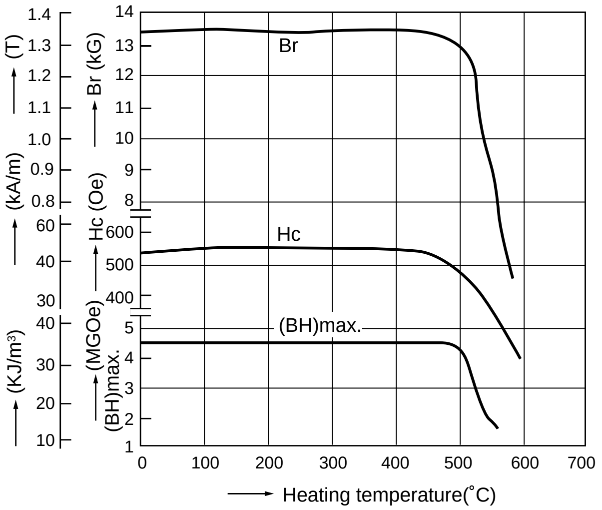


Fig. 30 Irreversible Temperature Change of Fe-Cr-Co Magnets

Table 8 Rate of Change in Br of Various Permanent Magnetic Materials (Irreversible Change)

Materials	Rate of Temperature Change in Br (%/˚C)
Alnico 5	– 0.021
Fe-Cr-Co Magnets	– 0.040
Rare-earth Magnets	– 0.043
Barium Ferrites	– 0.019

Change in Magnetic Resistance of Magnetic Circuit

The flux density at operating point will change in case magnetic resistance of magnetic circuit under operation changes. And since the rate of change is interrelated with permeablilty of recoil, recoil curve of Fe-Cr-Co Magnet KX-1 is shown in Fig. 31. From this, you can see Fe-Cr-Co Magnets is superior to alnico magnets regarding magnetic stability. (μrec. of alnico 5 is approx. 3.7 max.)

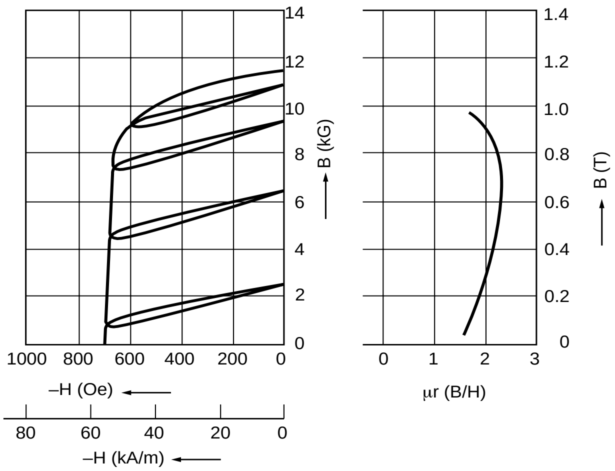


Fig. 31 Recoil Curve of Fe-Cr-Co Magnets KX-1

Magnetization and Demagnetization

Magnetization

Magnetized magnets may be demagnetized upon influence from diamagnetic fields or handling of products when transported. And, regarding their performance, it is advantageous to magnetize product after they are assembled. Therefore, we deliver general magnets without being magnetized. Approximately 3kOe of the magnetic field is necessary for the saturation magnetization. However, in reality, half that value is needed for actual magnetization.

Demagnetization

Generally, magnets generate a few percent of demagnetization due to contact demagnetization. Therefore, when designing magnetic circuit, it is possible to take optimum margin for demagnetizing and demagnetize that margin in order to ensure the performance of the circuit under operation.

Ordering Information

When placing an order with NEC TOKIN Iron-Chromium-Cobalt Magnets, be sure to specify the following items.

1) Shapes and dimensions
2) Necessary magnetic properties
3) Direction of magnetization
4) Whether or not magnetizing is necessary
5) Conditions under which the material will be used.
6) Any other relevant specifications (plating, coating, sealing)

Table 9 General Shapes and Dimensions

Shapes	Dimensions	Others
Plate	t0.3 ~ 4.0	Magnets of shapes stated left or molded by die-cutting, or grinding are available.
Rod	ø10 ~	
Line	ø0.5 ~ 10	

Magnetizing Electromagnets

M-G Series Magnetizer

Specifications

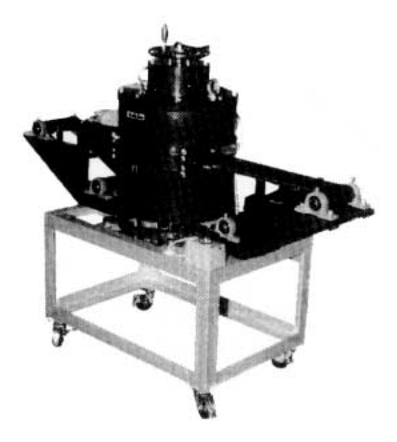
Table 10 Specifications of M-G Series Magnetizer

Model	Magnetic pole diameter **Dp(mm)**	Magnetic pole interval **Lg(mm)**	Magnetic field strength **T(kG)**	Cooling method	Weight (kg)	Power	
						Input	Output
M-10G	50	10	2.0(20)	Air	130	AC 200V 1ø	DC 8A 200V
	60	30	1.0(10)				
M-20G	70	10	2.0(20)	Air	250	AC 200V 1ø	DC 20A 200V
	90	30	1.0(10)				
	40	20	2.0(20)				
M-30G	60	30	2.0(20)	Air	520	AC 200V 1ø	DC 30A 200V
	100	50	1.0(10)				
	100	15	2.0(20)				
M-40G	100	42	2.0(20)	Air	1,300	AC 200V 3ø	DC 60A 200V
M-50G	125	50	2.0(20)	Air	3,000	AC 200V 3ø	DC 70A 330V

Accessory
1. I/O cable (5m each)
2. Foot switch

Note: As designed for magnetizing, duty is 20~30%.

M-G Series Avtomatic Demagnetizer



Outline

M-G Series automatic magnetizer enables continuous magnetization of magnets for small motors, micro relays, dot printers, etc. within the magnetic circuit. Combination of magnetizer and belt conveyor offers compatibility with various magnetic circuits and easy combination with robots. Built-in magnetizing power supply, control unit for belt conveyor and robot control circuit minimizes installation space. The system is composed of:
1)Magnetizer (M-G Series, water cooling type)
2)Belt conveyor unit
3)Demagnetizing power supply and conveyor unit
4)Optional installation unit
5)Pedestal
Please consult NEC TOKIN for details.
Note: As designed for magnetizing, duty is 20~30%.

Technical Terms

The following are terms describing magnetic volumes by SI units which are necessary for using permanent magnets.

Magnetic Properties

Magnetic Fields

There exists magnetic fields on earth. This exists not only in permanent magnets but also around electric conductors.

Magnetic field is represented by H. The unit (SI) is represented by A/m. For instance, earth magnetic field is approximately 24A/m. It is possible to create easily magnetic filed of 1.6MA/m by using electromagnets. However it needs some device to create stronger magnetic fields.

Magnetization

When placing magnetic materials in magnetic fields, that material will generate magnetic changes. This is called magnetization. Further, the rate of magnetization is called "intensity of magnetization". And its strength is represented by M. Its unit is T.

Saturation Magnitization

As increasing magnetic fields imposed upon magnetic material, that material will reach saturation. This degree of magnetization is called saturation magnitization. For instance, saturation magnitization of barium ferrite magnet is approximately 0.44T and that of Lanthanet® [LM-19] is approximately 0.86T.

Magnetizing

The operation to apply magnetic field enough for magnetic material to reach saturation is called magnetizing. And when remove magnetic field used for magnetizing from the material, it will keep the state of being magnetized. After going through this process, magnetic material will be permanent magnet.

Magnetic Flux Density (Magnetic Induction)

As stated above, magnetic material is magnetized by magnetizing. In this case, magnetic flux goes through the material. Magnetic flux per unit area is called magnetic flux density (magnetic induction) and it is represented by B. The unit is represented by gauss, equal to that of intensity of magnetization. This magnetic flux density is represented by $B = J + \mu_0 H$. Briefly speaking, this value is equivalent to magnetic field given to the material plus intensity of magnetization. The intensity of magnetization in the air is nearly zero regardless of the intensity of the magnetic field (In another words, 4pl of the air is nearly zero.). Therefore, after taking the magnets used for magnetizing out of the magnetic field, the intensity of magnetization around the magnet will be equal to the magnetic field on site. Practically, the most important matter is the value of this magnetic flux density.

Residual Magnetic Flux Density,

This section explains the change in the intensity of magnetic field and the magnetic flux density when exerting magnetic field to the magnetic material gradually or conducting the reverse process by decreasing magnetic field.

At first, as stated in the previous section, when gradually adding magnetic field to magnetic material, it will gradually gain magnetization and finally reaches saturation magnetization. This process is called primary magnetizing process. In the next stage, the magnetic flux density gained by decreasing magnetic fields and eliminating external magnetic field exerted upon the magnetic material is called residual magnetic flux density Br (residual magnetic induction). Further, by exerting magnetic field to the material without external magnetic field towards the reverse direction, the magnetizing and magnetic flux density will decrease. Then the magnetic flux will not go through the magnetic material. The intensity of magnetic field exerted upon the material on this stage in called coercive force H_{CB}. Further, when increasing magnetic field of reverse direction, the magnetic flux will flow toward reverse direction and then magnetization intensity will be eliminated. In another word, there are two kinds of coercive force. One is magnetic field H_{CB} gained by decreasing magnetic flux density B to zero. Another is magnetic field H_{CJ}, gained by decreasing the intensity of magnetization intensity J to zero.

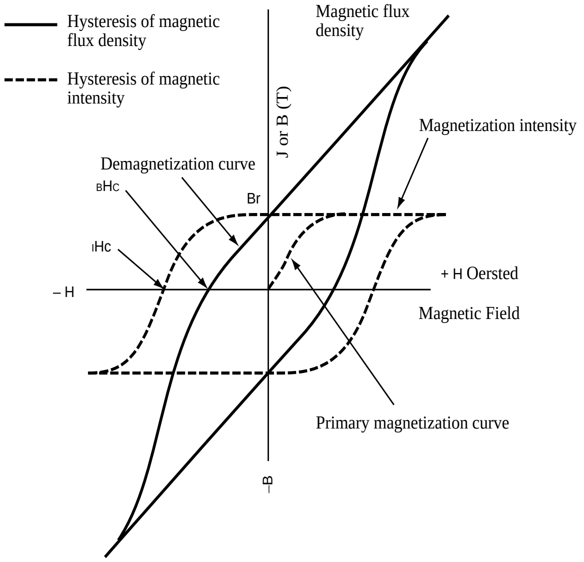


Fig. 32 Hysteresis Loop of Permanent Magnet

When increasing diamagnetic field beyond coercive force H_{CJ}, the magnetization intensity will turn around to the opposite direction and correspond to the direction of diamagnetic field, and finally the magnetization intensity will be saturated. The curve describing repetition of these processes is called Hysteresis Loop (Refer to Fig. 32).

Diamagnetic Field

Permanent magnet generates external magnetic field by its N and S pole. On the other hand, the magnetic field exists within the magnet generated by the same N and S pole. This is called diamagnetic field (demagnetization field). The size and direction is different from magnetic flux density inside the magnet. Diamagnetization field tends to decrease its own magnetic intensity. And as near as N and S pole exists (the length of magnet is short), demagnetization field gets larger.

Demagnetization Curve

As stated in the section of magnetic flux density, permanent magnet uses its magnetic flux generated through magnetization process. Therefore, as much magnetic flux density remains in the permanent magnet despite large diamagnetic field, it can be said that its feature is more prominent. As a result, the essential condition for superior permanent magnet is that it has large residual magnetic flux density and coercive force BHC. Demagnetization curve is used in order to find out how magnetic flux density changes according to the intensity of diamagnetic field. This curve is identical to the second quadrant of hysteresis loop which explains the relationship between magnetic flux density and magnetic field.
(Refer to Fig. 32)
The first step to evaluate the permanent magnet is to see its hysteresis Loop.

Operating Point

When diamagnetic field exerted upon the permanent magnet is equal to Hd, the magnet generates magnetic flux density (magnetic induction) which correspond to Bd on the demagnetization curve. In this way, the point represented by Hd and Bd is called the operating point of the permanent magnet. (Refer to Fig. 33). However, in practical use, this point changes according to the environmental conditions. For example, the operating point of magnet is positioned at P in Fig. 33 after being magnetized, it will move to area in which diamagnetic field decreases and magnetic flux density increases when attaching iron piece to the magnet.

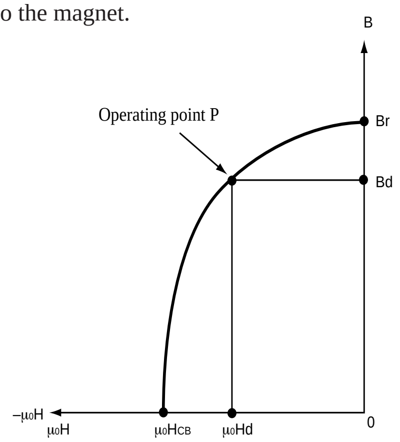


Fig. 33 Operating Point of Permanet Magnet Operating point P

Maximum Energy Product

As stated in the section of demagnetization curve, the criteria to judge the magnetic properties of permanent magnet is to see demagnetization curve. In another words, if some diamagnetic field Hd exists, it is only necessary to find out how much the magnetic flux density Bd is. So, best way to judge magnetic properties of permanent magnet is to use maximum product of Hd x Bd on operating point. Since Hd x Bd is proportional to energy per magnet volume which magnet enables to give off into outer space, that value is called maximum energy product. The unit of maximum energy product is J/m^3.
Optimum method to design permanent magnet is to make sure that the operating point is identical to the point of maximum energy product. The reason is that it is possible to minimize the volume of permanent magnet required to gain necessary energy.

Minor Loop

In the previous section, it is stated that operating point moves according to operational conditions of permanent magnet. This does not mean the operating point moves exactly on demagnetization curve. But it moves on hysteresis Loop which are formed with the primary operating point as the datum point as shown in Fig. 34. This small hysteresis Loop which starts from demagnetization curve is called minor loop. The operating point of permanent magnet should generally be on minor loop. However, in case the operating point does not move such as that of magnet for speaker, it is naturally on demagnetization curve.

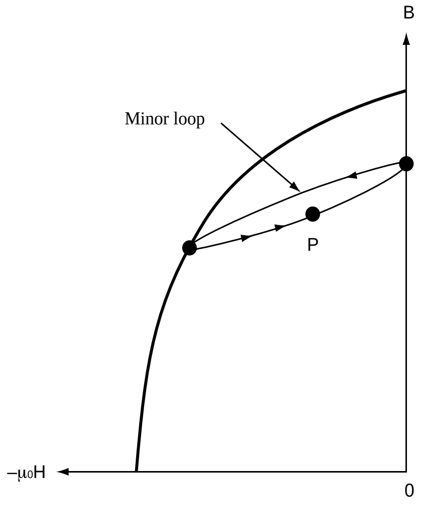
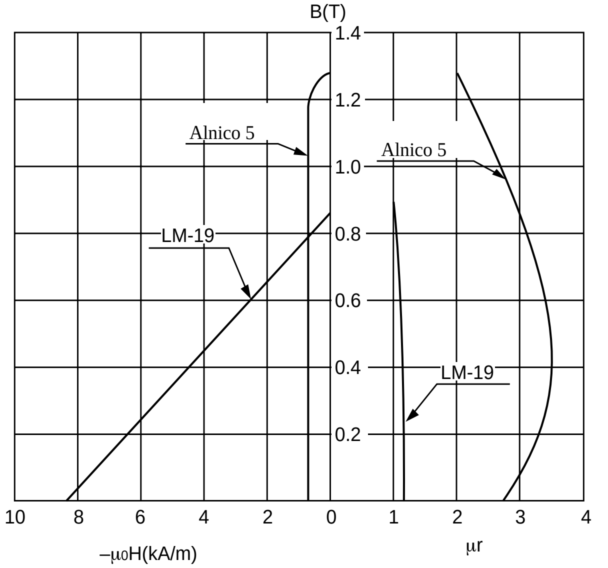


Fig. 34 Minor Loop and Operating Point

Reversible Permeability

Since the area of minor loop is small, generally round trip of the loop can be represented by one line. The angle of this line B/H is called reversible permeability and represented by μr. Reversible permeability varies depending upon its starting point on demagnetization curve. Fig. 35 shows comparison of permeability between Lanthnet® and Alnico magnet on the same scale. Usually, when representing reversible permeability by one figure, the value showing maximum energy product on operating point is used. The reason is that the magnetic material whose angle of demagnetization curve is close to 45˚ has reversible permeability which is close to 1. And since its coercive force is large, the operating point will return to the primary position even though strong diamagnetic field is exerted. Therefore, it is advantageous to use this value when generating magnetic field and using power of absorption as well as using repulsive power.



Demagnetization Curve **Reversible Permeability curve**

Fig. 35

Thermal Variations of Magnetic Properties

Irreversible Thermal change

Magnetic flux density of permanent magnet decreases when it is exposed to high temperature even though the quality of material does not change. This rate of change in magnetic flux density gradually gets smaller proportional to the length of the time during which the magnet is exposed to high temperature. And it reaches saturation in relatively short period of time and stop to change. The rate of change at this stage corresponding to primary value of magnetic flux density is called irreversible thermal variations. The irreversible thermal variations, whether small or large, is found in any permanent magnet. The degree of variation varies in a large scale depending upon retention temperature and position of operating point of magnet. Although barium ferrite is demagnetized when exposed to low temperature, Lanthanet® is not.

Heat treatment and AC Demagnetization

Since permanent magnet incurs irreversible thermal variation, its magnetic properties will be deteriorated when exposed to high temperature during operation. In order to avoid this, it is necessary to allow the magnetic flux density to be compatible with rate of irreversible thermal variations for maximum operating temperature when designing permanent magnet. And then expose the magnet to the maximum operating temperature for several hours after magnetized. This process to stabilize magnet is called thermal seasoning. For alnico magnet, stabilizing process is performed by exerting AC magnetic fields (AC demagnetization).

Reversible thermal change (Temperature Coefficient)

So far, magnetic properties at room temperature is stated. Conditions of magnetic properties when magnet is exposed to low or high temperature is extremely important upon practical operation. In order to find thermal change of magnetic properties, demagnetization curve at each temperature is required. By simplifying this process, changes in operating point Bd per 1˚C is called rate of irreversible thermal change(temperature coefficient). This rate should be measured after irreversible thermal variations at every temperature is completed.

In addition, regarding general magnets, rate of irreversible thermal variations will change according to the position of operating point of the magnet. However, when this rate is represented by one figure, the value should be based on the variations of Bd at the point of maximum energy product like reversible permeability.

Designing of Permanent Magnets

It is possible to design permanet magents in a highly accurate scale without using electronic calculator. The following is the basic concept of designing permanent magnets.

Basic Concept of Designing Permanent Magnets

When creating magnetic fields using permanent magnets, it is necessary to prevent loss of magnetomotive force by using combination of permanent magnet and a yoke. The problem regarding design of magnetic circuit is how to decide minimum required dimensions of permanent magnets. There are two equations to solve above problem.

a) Magnetomotive force of permanent magnets is equal to loss of magnetomotive force in void.

$$Hd \bullet Lm = Hg \bullet Lg \text{ ------------ (1)}$$

b) Total magnetic flux going through center of permanent magnet is equal to magnetic flux going through void.

$$Bd \bullet Am = Bg \bullet Ag \text{ ------------ (2)}$$

Using CGS unit, it can be said that Hg = Bg. Therefore, if (1) x (2),

$$Hd \cdot Bd = \frac{Bg^2 \cdot Lg \cdot Ag}{Lm \cdot Am}$$

On condition that:

Am: Cross section of magnet
Lm : Length of magnet
Bd : Magnetic flux density at an operating point
Hd : Intensity of magnetic field at an operating point
Ag : Cross section of void
Lg : Length of void
Bg : Magnetic flux density in void
Hg : Intensity of magnetic field in void

Therefore, in order to minimize Lm • Am of permanent magnet, it is necessary to select the point of maximum energy product on demagnetization curve of permanent magnet at which Bd • Hd is maximized. Then, after selecting Hd and Bd, it is required to examine whether magnetic field Bd which is needed for necessary void (Volume = Ag • Lg) can be generated. But actually, loss of magnetomotive force and leakage of magnetic flux is so large the drastic modification of equation (1) and (2) will be required. This modification method is known as loss coefficient of magnetomotive force (reluctance coefficient) and leakage coefficient.

When these values are represented as:

f: Leakage coefficient
r: Reluctance coefficient

The following equation will be established:

$$F = Hd \bullet Lm = r \bullet Bg \bullet Lg \text{ (Magnetomotive force) ------ (1)'}$$

$$ø = Bd \bullet Am = f \bullet Bg \bullet Ag \text{ (Magneic flux) ---------------- (2)'}$$

Reluctance coefficient r is the correction coefficient to be used for the case in which magnetomotive force generated from permanent magnet is consumed in yoke or joint section between yoke and magnet. Except when design of the magnet is not ordinal, the value should be between 1.1 and 1.5 (usually 1.3).

Leakage coefficient is the correction coefficient to be used for the case in which magnetic flux generated from permanent magnet is leaked form around void or yoke. This value varies depending upon the state of magnetic circuit.

Example 1: Find the value of Bg

Now, in case shape and dimensions of magnetic circuit is already decided, and f is found, the equation established from (1)' and (2)' will be:

$$p = \frac{Bd}{Hd} = \frac{Lm \cdot Ag \cdot f}{Am \cdot Lg \cdot r}$$

Since Lm and Lg are already decided, permeance coefficient can also be decided. On the other hand, Bd and Hd can be found from demagnetization curve.

From (2)', $Bg = \frac{Bd \cdot Am}{f \cdot Ag}$

Therefore the value of Bg can be found. The case of finding Bg using this equation is only when f can be estimated using similar magnetic circuit.

Leakage Coefficient and Permeance

Leakage coefficient f can be found by closely assuming flow of magnetic flux and calculate it as equivalent circuit related in Table 11.

Leakage Coefficient vs. Magnetic Circuit

Table 11

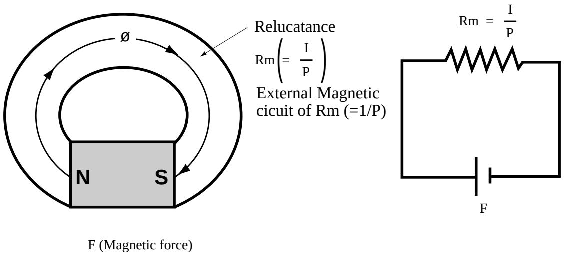
Magnetomotive force F	Electromotive force V
Magnetic flux ø	Current I
Reluctance Rm	Resistance R
$Rm = \frac{1}{\mu S}$	$R = \frac{1}{\sigma S}$
Permeability μ	Conductivity
Permeance P	Conductance G
$P = \frac{1}{Rm}$	$G = \frac{1}{R}$
F=NI=Rm ø	V=R • I

In circuit shown in Table 27, permeance P of external magnet is defined as P = ø/F.

On the other hand, from the equation F = Hd • Lm, ø = Bd • Am, the following equation will be established:

$$p = \frac{Bd}{Hd} = P\cdot\frac{Lm}{Am} \quad \text{--------------} \ (3)$$

Therefore, permeance coefficient P is equivalent to Permeance P in case length of magnet Lm and cross section Sm is equal to the size of the unit. So it can also be called unit permeance.



Magnetic Circuit

Equivalent Electric Circuit

Fig. 27. Magnetic Circuit and Equivalent Electric Circuit

In the next stage, in case external magnetic circuit is separated into two systems, the following equation will be established from Fig. 28.

$$F = øg/Pg = øf/P_f$$
$$ø = øg + ø_f$$
$$= F(Pg + P_f)$$

When total permeance is set is PT,

$$PT = Pg + P_f.$$

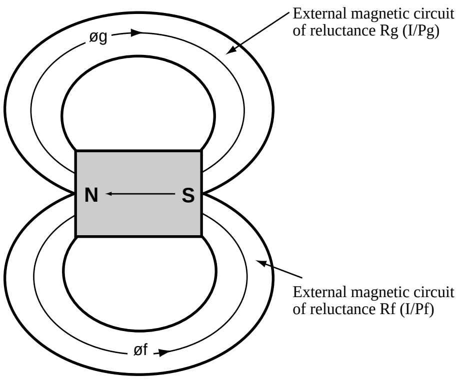
When defining Pg as permeance in gap and Pf as permeance in leakage section, leakage coefficient f will be defined as:

$$f = \frac{\text{Total magnetic flux (ø)}}{\text{Total magnetic flux in the gap}} = \frac{Pg + Pf}{Pg} = \frac{P_T}{Pg}$$

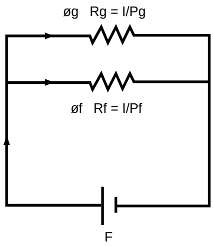
In addition, permeance coefficient of permanent magnet can be defined from equation (3):

$$p = P_T\cdot\frac{Lm}{Am\cdot r}$$

Fig. 29 presents an example leakage condtion of magnetic circuit.



Magnetic Circuit



Equivalent Electric Circuit

Fig. 28 Magnetic Circuit with 2 External Magnetic Fields

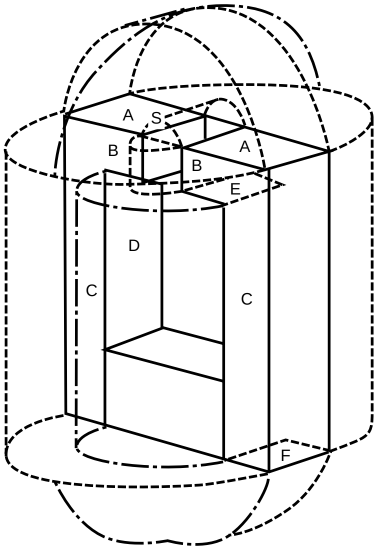
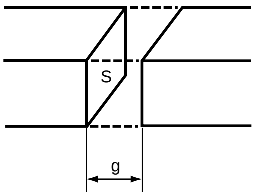
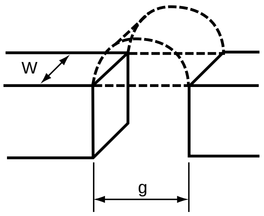
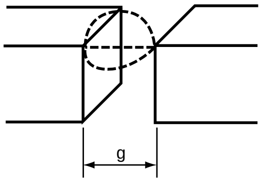
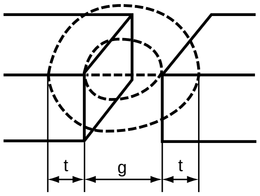
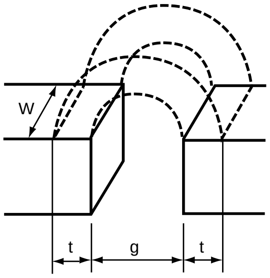


Fig. 29 Example of Leakage Flux

Place	Equation
Parallel, plain Permeance between two surfaces  	S ; Area of magnetic pole g ; Void distance $P = \frac{s}{g}$
Barrel-shape permeance from straight line  	W; Width of yoke or magent $P = 0.264W$
Permeance corresponding to a quater of the ball from the corner  	g ; Void distance $P = 0.077g$
Permeance correspoding to a quater of the ball from side line  	t ; Distance considered g ; Void distance $P = \frac{t}{4}$
Barrel-shape permeance from side panels  	W; Width of yoke or magnet t ; Distance considered g ; Void distance ① When g≥3t, $P = 0.637\frac{W}{1+g/t}$ ② When g<3t, $P = \frac{W}{\pi}\ell n\frac{g+2t}{g}$

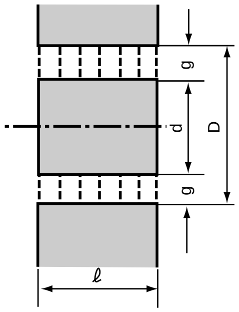
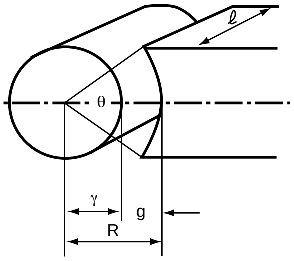
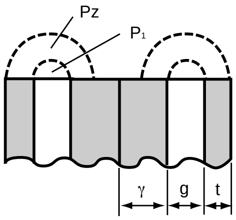
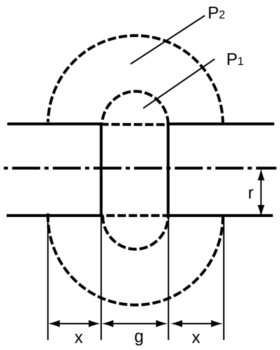
Place	Equation
Peameance between surfaces of concentric tubes  	ℓ ; Length of cylindrical tube D, d ; Outer/inner diameter of cylindrical tube g ; Void distance $P = 2\pi\ell/\ell n\frac{D}{d}$ (When g is smaller than d and g/d<0.01: P = πd ℓ/g)
Permeance between circular surfaces  	ℓ ; Length of arc R, γ ; Radius of arc θ ; Angle of arc (Radian) g ; Void distance $P = \theta\ell/\ell n\frac{R}{\gamma}$ (When g is smaller than γ, P =θγℓ/g)
Permeance between surfaces of cylindrical void  	$P = P_1 + P_2$ $(\gamma > t)$ $= (\gamma + \frac{g}{2})\{1.66 + 2\ell n(1+2t/g)\}$ $(\gamma < t)$ $= (\gamma + \frac{g}{2})\{1.66 + 2\ell n(1+2\gamma/g)\}$
Permeance between surfaces of cylindrical side panels  	$P = P_1+P_2$ $= 1.65(\gamma + 0.212g)$ $+\{2r + \sqrt{g(g + 2x)}\}\ell n(1+2x/g)$

Fig. 30 Permeance of Various Void

Example 2 Finding Leakage Coefficient

Design method in case permeance is parallel and exists in large numbers:

1) Flow of magnetic field around the void should be set as close as to Fig. 30. (including gap)
2) Using Fig. 30, find permeance Pg, Pf1 ------ Pfm of each section.
3) Find P1 = Pg + Pf1 + ----------- + Pfm
4) Find f = PT/Pg
5) Find Am so that p = PT X (Lm/Am) can be optimum considering Demagnetizing properties. In this case, Lm = (rBg • Lg)/Hd.
6) Confirm f again when dimensions is decided.

This methods uses the fact in which permanent magnets are uniformerly magnetized and, if the strenght of those magnets are I, their magnetic density per unit area in cross section perpendicular to the direction of magenetization.

When there is magnetic pole I at one point, magnetic field generated by that magnetic pole at the point with distance of R from the original point will be the following based on Coulomb's law:

$$H = \frac{I}{\ell^2}$$

Therefore, if surface density l are distributed on a disk whose diameter is ro, the magnetic field at the point on its central axis with distance of R will be:

$$H = 2\pi I\left(1 - \frac{\ell}{\sqrt{\ell^2 + r_0^2}}\right) \text{(Oe)} \text{ --------(4)}$$

The essential condition using this method is that magnetic poles are uniformly distributed. Therefore, this method is effective only when the operating point exists in the region when angle of demagnetization curve is 45˚. In another words, it is effective for all ferrite magnets and rare-earth magnets if the operating point exists above turning point of demagnetization curve.

Example 1 Magnetic Field of Central Axis of Cylindrical Magnets

In this case, substitute dimensions shown in Fig. 31 and $2\pi I = \frac{Br}{2}$ and $\gamma_o = \frac{D}{2}$ into equation (4). Plus adding these to the sum of magnetic fields generated by magnetic poles of the front and rear circle. Therefore magnetic field will be the following equation:

$$H = \frac{Br}{2}\left(\frac{(\ell + Lm)}{\sqrt{(\ell + Lm)^2 + \frac{D^2}{4}}} - \frac{\ell}{\sqrt{\ell^2 + \frac{D^2}{4}}}\right) \text{ ---------(5)}$$

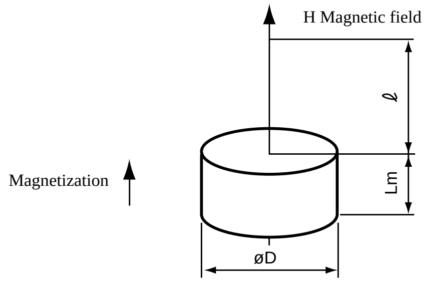


Fig. 31 Cylindrical Magnets

Example 2 In Case of Facing Cylindrical Magnets

In case of facing magnets shown in Fig. 31, magnetic field on their central point will be twice the equation (5).

Example 3 In Case of Facing Cylindrical Magnets and Connecting Their Rear Surface by Yoke

In this case, magnetic field on rear surface of Fig. 32 will be erased. Therefore double of equation (4) can be used.

$$H = Br\left(1 - \frac{\ell}{\sqrt{\ell^2 + \frac{D^2}{4}}}\right)$$

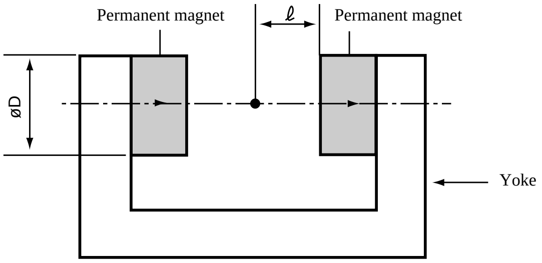


Fig. 32 n Case of Connecting Yokes

The smaller ratio of dimensions of magnet (D/L), error rate is smaller.

Example 4 In Case of Square Magnets

By applying dimensions shown in Fig. 33 (angle is radian), the following equation is established:

$$H = \frac{Br}{\pi}\left[\tan^{-1}\frac{ab}{2\ell\sqrt{4\ell^2 + a^2 + b^2}} - \tan^{-1}\frac{ab}{2(\ell + Lm)\sqrt{4(\ell + Lm)^2 + a^2 + b^2}}\right] \text{ ---------(6)}$$

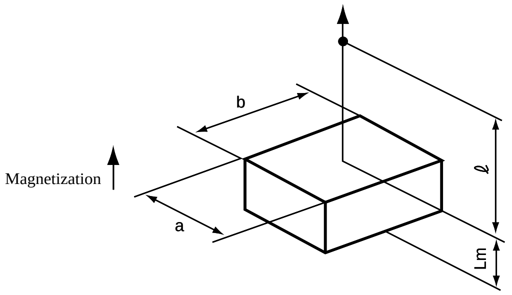


Fig. 33 Square Magnets

Applying these methods, magnetic fields inside and outside perforated magnets can be found.

In every cases, error compared with practical value occurs. The reason is that magnetic poles are not distributed uniformly and they exists on other faces mentioned in this section.

Method to Find Permeance Coefficient of Single Magnets

Permeance coefficient of all single magnets can be found using equation (5) and (6). First, substitute $\ell = -\frac{Lm}{2}$ for these equations and find H. And this will be diamagnetic field Hd. Secondly, if demagnetization curve has gradient of 45˚, *Bd = Br - Hd* is established. Therefore permeance coefficient can be found using the following equasion:

$$p = \frac{Bd}{Hd} = \frac{Br-Hd}{Hd}$$

By adding correction coefficient to improve accuracy, the following equation will be established.

Permeance coefficient of cylindrical magnet

$$p = 1.3\,\frac{Lm}{D}\left(\sqrt{1+\left(\frac{Lm}{D}\right)^{2}}+\frac{Lm}{D}\right)$$

Permeance coefficient of square magnet (angle is radian)

$$p = 1.2\left[\frac{\pi}{2}\left\{\tan^{-1}\frac{ab}{Lm\sqrt{a^{2}+b^{2}+Lm^{2}}}\right\}^{-1}-1\right]$$

(Refer to Fig. 31 and Fig. 33. for dimensions)

This calculation uses charge method. Therefore, when permeance coefficient is below turning point of demagnetization curve, it is necessary to use apparent Bd minor loop in case of drawing minor loop form that point.

Units of Magnets

The following equation represents SI Unit (International Unit) and CGS Unit.

SI Unit

$\mu_0 = \mu_0$

$$B = \mu_0 H + \mu_0 M$$
$$= \mu_0 H + J$$

$$B = \mu_0 (H+M)$$

$$\mu_0 = \frac{1}{\varepsilon_0 c^2} \text{ (H/m)}$$
$$= 4\pi \times 10^{-7} \text{(H/m)}$$

CGS Unit

$\mu_0 = 1$

$$B = H + M$$
$$= H + 4\pi J$$

Please refer to the following page for details.

Conversion of SI and CGS Unit

Volume	Symbol	Unit				SI to CGS Unit	CGS to SI Unit
		SI Unit		CGS Unit			
		Name (Equation)	Symbol	Name (Equation)	Symbol		
Magnetic flux	Φ	Weber ($\Phi=BA$)	Wb	Maxwell ($\Phi=BA$)	Maxwell	1Wb=10^8 Maxwell	1 Maxwell=10^{-8} Wb
Magnetic flux density Magnetic induction	B	Tesla	T	Gauss	G	1T=10^4 G	1G=10^{-4} T
Magnetic constant (Vaccum permeability)	μ_o	Henry per meter	H/m	Absolute number ($\mu_o=1$)	—	—	—
Magnetic intensity	H	Ampere per meter	A/m	Oersted	Oe	1A/m=$\frac{4\pi}{10^3}$Oe=1.25664×10^{-2}Oe	1Oe= $\frac{10^3}{4\pi}$A/m=79.5775A/m
Magnetic flux density compatible with magnetic intensity		Tesla ($\mu_o H$)	T	Oersted	Oe	1T=10^4 Oe	1Oe=10^{-4} T
Magnetization *	M	Ampère per meter ($M=\frac{J}{\mu_o}$)	A/m	Gauss ($M=4\pi J$)	G	1A/m=10^3 G	1G=10^{-3} A/m
Magnetic polarization	J	Tesla ($J=\mu_o M$)	T	Gauss ($J=\frac{M}{4\pi}$)	G	1T=$\frac{10^4}{4\pi}$G	1G=$4\pi\times10^{-4}$ T
Permeability (Absolute permeability)	μ	Henry per meter	H/m	Absolute number	—	1H/m=$\frac{10^7}{4\pi}$=7.95775×10^5	1=$\frac{4\pi}{10^7}$H/m=1.25664×10^{-6}H/m
Permeability (Permeance coefficient)	μ_r	Absolute number ($\mu_r=\frac{\mu}{\mu_o}$)	—	Absolute number ($\mu_r=\mu$)	—	SI and CGS Unit are identical	
Magnetomotive force Magnetic difference	Fm Um	Amperè ** ($Fm=HL$) ($Um=H\Delta L$)	A	Gilbert ($Fm=HL$) ($Um=H\Delta L$)	Gilbert	1A= $\frac{4\pi}{10}$ Gilbert =1.25664 Gilbert	1 Gilbert=$\frac{10}{4\pi}$A =0.795775A
Permeance	Λ	Henry ($\Lambda=\frac{\Phi}{Fm}$)	H	Maxwell per Gilbert ($\Lambda=\frac{\Phi}{Fm}$)	Maxwell/Gilbert	1H=$\frac{10^9}{4\pi}$ Maxwell/Gilbert =7.95775×10^{-7} Gilbert/Maxwell	1 Gilbert/Maxwell=$\frac{4\pi}{10^9}$ H =1.25664×10^{-8}H
Magnetic resistivity	Rm	Henry ($Rm=\frac{Fm}{\Phi}$)	H^{-1}	Maxwell per Gilbert ($Rm=\frac{Fm}{\Phi}$)	Gilbert/Maxwell	$1H^{-1}$=$\frac{4\pi}{10^9}$ Gilbert/Maxwell =1.25664×10^{-8} Gilbert/Maxwell	1 Gilbert/Maxwell=$\frac{10^9}{4\pi}$ H^{-1} =$7.95775\times10^7 H^{-1}$
Magnetic energy product		Joule per cubic meter (BH)	J/m^3	Gauss Oersted or Erg per cubic centimeter (BH)	G Oe erg/cm^3	1J/m^3=$4\pi\times10$GOe =1.25664×10^2 GOe =1.25664×10^2 erg/cm^3	1GOe= $\frac{1}{4\pi}\times10^{-1}$ J/m^3 =7.95775×10^{-3} J/m^3 =1erg/cm^3
Magnetic energy	E	Joule ($\frac{BH\bullet AL}{2}$)	J	Erg ($\frac{BH\bullet AL}{8\pi}$)	erg	1J=10^7 erg	1erg=10^{-7}J
Magnetic absorption	F	Newton ($\frac{B^2A}{2\mu_o}$)	N,	Dyne ($\frac{B^2A}{8\pi}$)	dyn	1N=10^5 dyn (1N=0.101972kgf)	1dyn=10^{-5}N (1kgf=9.80665N)

(Based on Electronic Materials Association standard EMAS-7003)

Note: 1. A= Cross section
2. L = Length of magnetic route
3. ΔL = Length of partial magnetic route
* Magnetization means magnetizing intensity
** Conventionally, Ampère Turn had been used. However, Ampère is used instead for SI Unit.

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⚠

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