

Boost Controller

TDA4863

Power Factor Controller
IC for High Power Factor
and Low THD

Power Management & Supply



Never stop thinking.

Previous Version:

Page	Subjects (major changes since last revision)
	Document's layout has been changed: 2002-Sep.

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**Power Factor Controller
IC for High Power Factor
and Low THD**

TDA4863

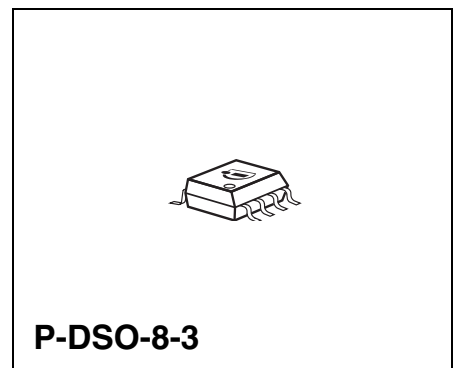
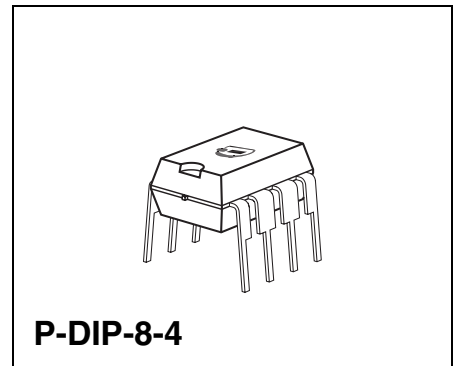
Final Data

Boost Controller

1 Overview

1.1 Features

- IC for sinusoidal line-current consumption
- Power factor achieves nearly 1
- Controls boost converter as active harmonic filter for low THD
- Start up with low current consumption
- Zero current detector for discontinuous operation mode
- Output overvoltage protection
- Output undervoltage lockout
- Internal start up timer
- Totem pole output with active shut down
- Internal leading edge blanking LEB



1.2 Improvements Referred to TDA 4862

- Suitable for universal input applications with low THD at low load conditions
- Very low start up current
- Accurate OVR and $V_{ISENSEmax}$ threshold
- Competition compatible V_{CC} thresholds
- Enable threshold referred to V_{VSENSE}

Type	Ordering Code	Package
TDA4863	Q67040-S4452	P-DIP-8-4
TDA4863G	Q67040-A4451	P-DSO-8-3

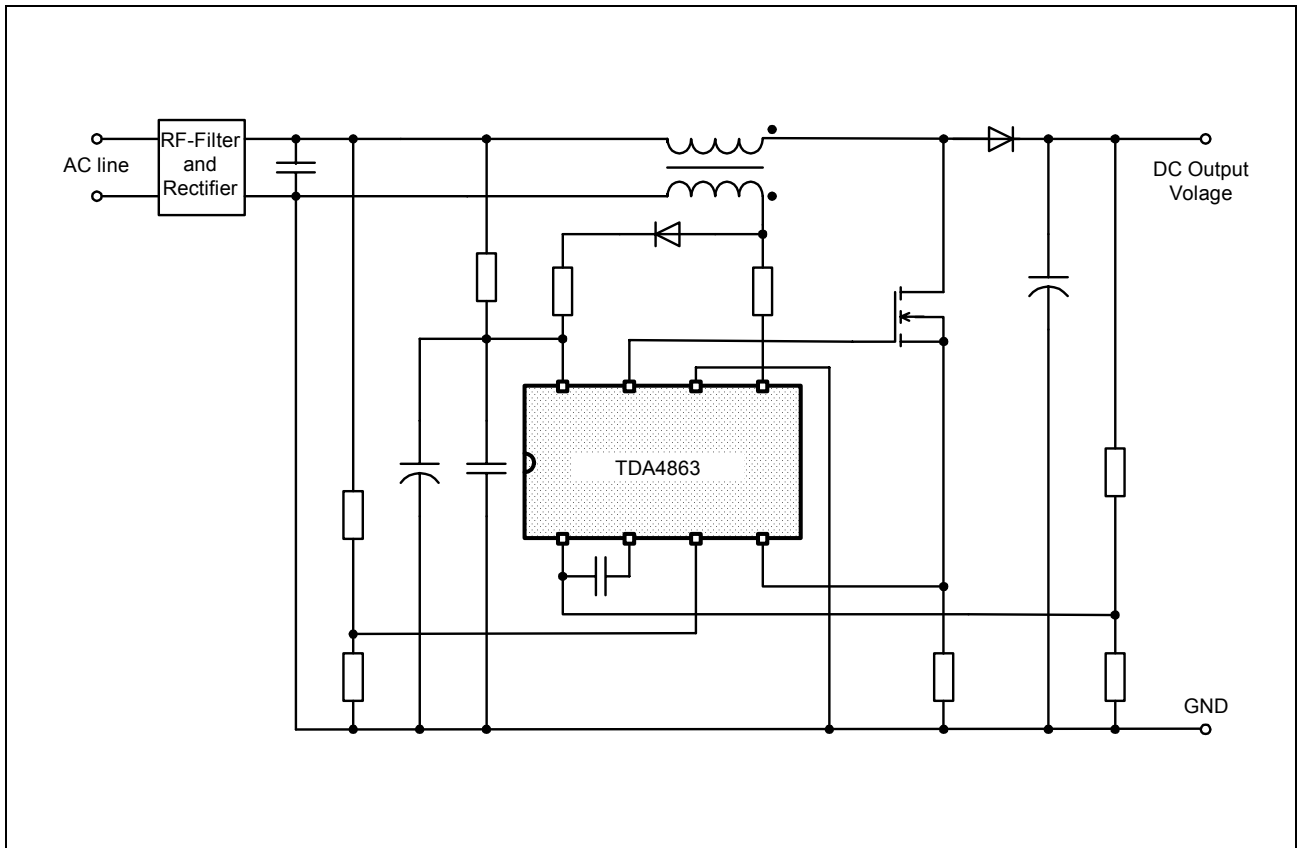


Figure 1 Typical application

1.3 Description

The TDA4863 IC controls a boost converter in a way that sinusoidal current is taken from the single phase line supply and stabilized DC voltage is available at the output. This active harmonic filter limits the harmonic currents resulting from the capacitor pulsed charge currents during rectification. The power factor which describes the ratio between active and apparent power is almost one. Line voltage fluctuations can be compensated very efficiently.

1.4 Pin Configuration

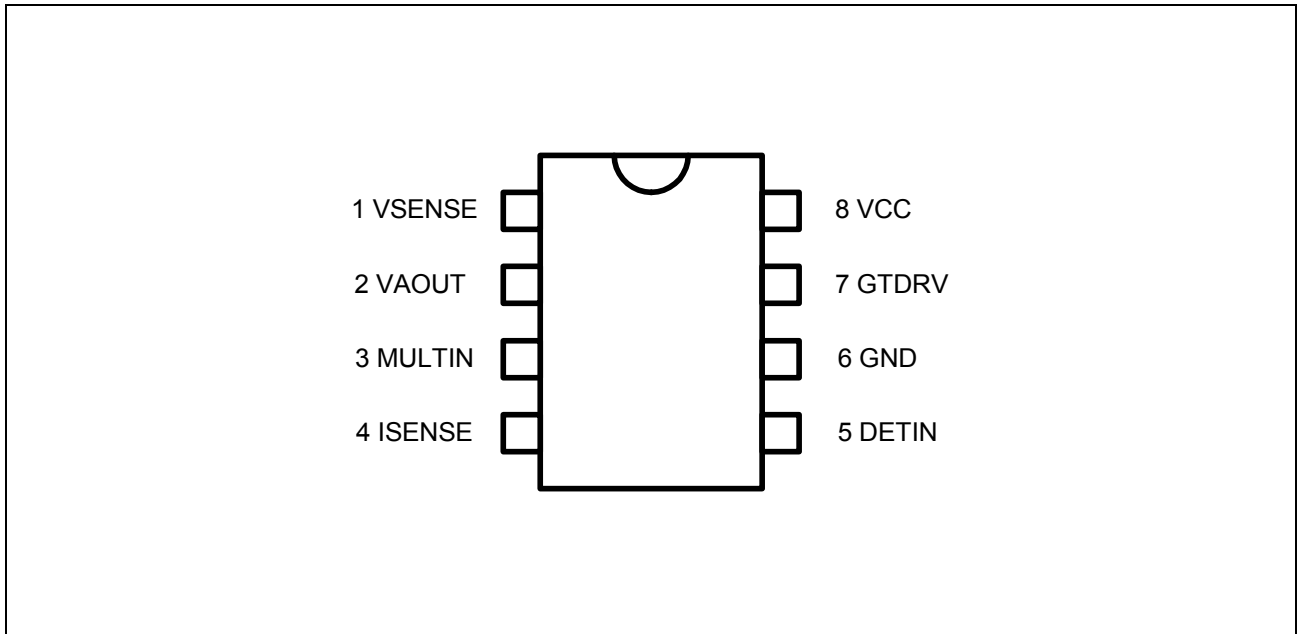


Figure 2 Pin Configuration of TDA4863

Pin Definitions and Functions

Pin	Symbol	Description
1	VSENSE	Voltage Amplifier Inverting Input VSENSE is connected via a resistive divider to the boost converter output. With a capacitor connected to VAOUT the internal error amplifier acts as an integrator.
2	VAOUT	Voltage Amplifier Output V_{VAOUT} is connected internally to the first multiplier input. To prevent overshoot the input voltage is clamped internally at 5 V. If V_{VAOUT} is less than 2.2 V the gate driver is inhibited. If the current flowing into this pin exceeds an internal threshold the multiplier output voltage is reduced to prevent the MOSFET from overvoltage damage.
3	MULTIN	Multiplier Input MULTIN is the second multiplier input and is connected via a resistive divider to the rectifier output voltage.
4	ISENSE	Current Sense Input ISENSE is connected to a sense resistor controlling the MOSFET source current. The input is internally clamped at -0.3 V to prevent negative input voltage interaction. A leading edge blanking circuitry suppresses voltage spikes when turning the MOSFET on.
5	DETIN	Zero Current Detector Input DETIN is connected to an auxiliary winding and monitors the zero crossing of the inductor current.
6	GND	Ground
7	GTDRV	Gate Driver Output GTDRV is the output of a totem-pole circuitry for direct driving a MOSFET. An active shutdown circuitry ensures that GTDRV is set to low if the IC is switched off.
8	VCC	Positive Voltage Supply If V_{CC} exceeds the turn-on threshold the IC is switched on. When V_{CC} falls below the turn-off threshold the IC is switched off. In switch off mode power consumption is very low. Two capacitors should be connected to VCC. An electrolytic capacitor and 100 nF ceramic capacitor which is used to absorb fast supply current spikes. Make sure that the electrolytic capacitor is discharged before the IC is plugged into the application board.

1.5 Block Diagram

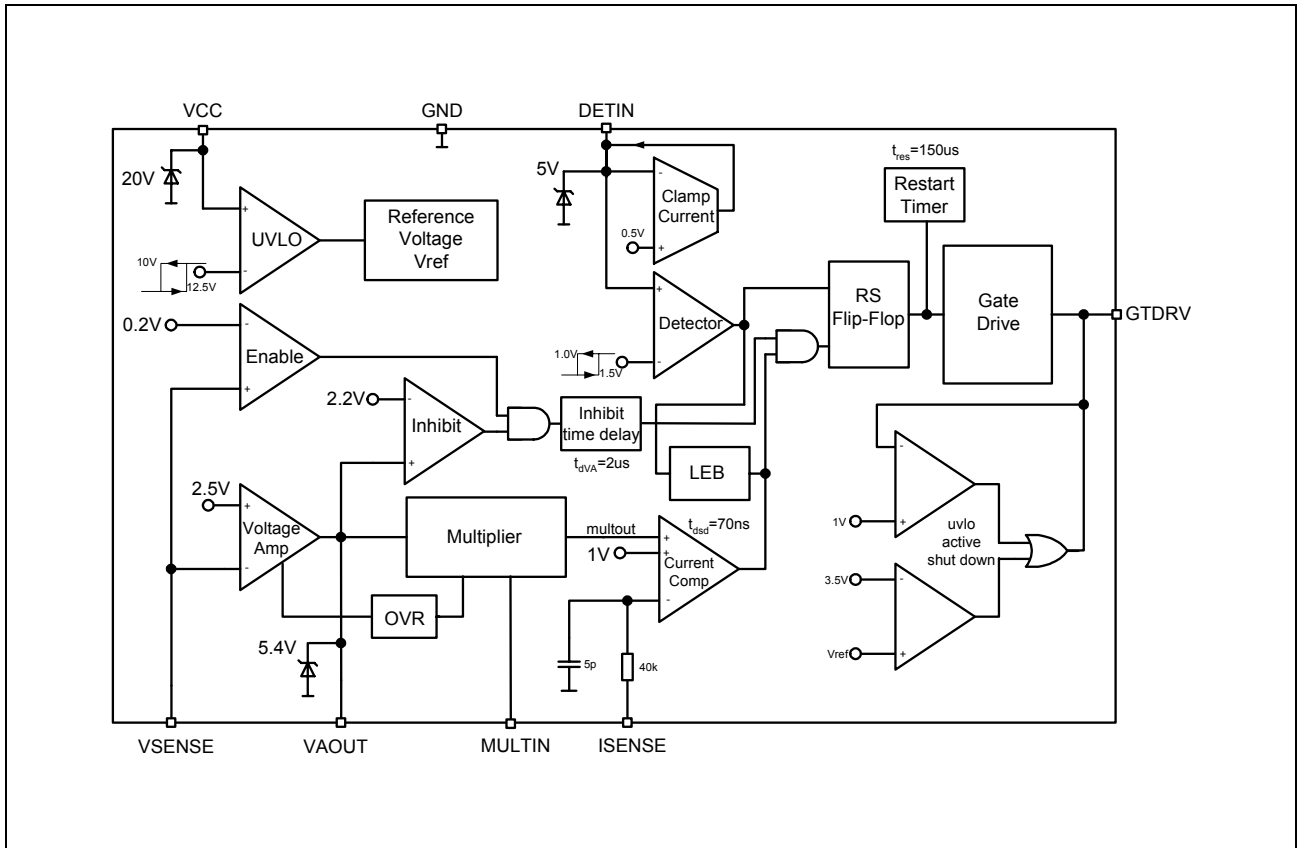


Figure 3 Internal Block Diagram

2 Functional Description

2.1 Introduction

Conventional electronic ballasts and switch mode power supplies are designed with a bridge rectifier and a bulk capacitor. Their disadvantage is that the circuit draws power from the line when the instantaneous AC voltage exceeds the capacitors voltage. This occurs near the line voltage peak and causes a high charge current spike with following characteristics: The apparent power is higher than the real power that means low power factor condition, the current spikes are non sinusoidal with a high content of harmonics causing line noise, the rectified voltage depends on load condition and requires a large bulk capacitor, special efforts in noise suppression are necessary.

With the TDA4863 preconverter a sinusoidal current is achieved which varies in direct instantaneous proportional to the input voltage half sine wave and so provides a power factor near 1. This is due to the appearance of almost any complex load like a resistive one at the AC line. The harmonic distortions are reduced and comply with the IEC555 standard requirements.

2.2 IC Description

The TDA4863 contains a wide bandwidth voltage amplifier used in a feedback loop, an overvoltage regulator, an one quadrant multiplier with a wide linear operating range, a current sense comparator, a zero current detector, a PWM and logic circuitry, a totem-pole MOSFET driver, an internal trimmed voltage reference, a restart timer and an undervoltage lockout circuitry.

2.3 Voltage Amplifier

With an external capacitor between the pins VSENSE and VAOUT the voltage amplifier acts like an integrator. The integrator monitors the average output voltage over several line cycles. Typically the integrator's bandwidth is set below 20 Hz in order to suppress the 100 Hz ripple of the rectified line voltage. The voltage amplifier is internally compensated and has a gain bandwidth of 5 MHz (typ.) and a phase margin of 80 degrees. The non-inverting input is biased internally to 2.5 V. The output is directly connected to the multiplier input.

The gate drive is disabled when VSENSE voltage is less than 0.2 V or VAOUT voltage is less than 2.2 V.

If the MOSFET is placed nearby the controller switching interferences have to be taken into account. The output of the voltage amplifier is designed in a way to minimize these interferences.

2.4 Overvoltage Regulator

Because of the integrator's low bandwidth fast changes of the output voltage can't be regulated within an adequate time. Fast output changes occur during initial start-up, sudden load removal, or output arcing. While the integrator's differential input voltage remains zero during this fast changes a peak current is flowing through the external capacitor into pin VAOUT. If this current exceeds an internal defined margin the overvoltage regulator circuitry reduces the multiplier output voltage. As a result the on time of the MOSFET is reduced.

2.5 Multiplier

The one quadrant multiplier regulates the gate driver with respect of the DC output voltage and the AC half wave rectified input voltage. Both inputs are designed to achieve good linearity over a wide dynamic range to represent an AC line free from distortion. Special efforts have been made to assure universal line applications with respect to a 90 to 270 V AC range.

The multiplier output is internally clamped to 1.3 V. So the MOSFET is protected against critical operating during start up.

2.6 Current Sense Comparator, LEB and RS Flip-Flop

The source current of the MOS transistor is transferred into a sense voltage via the external sense resistor. The multiplier output voltage is compared with this sense voltage. Switch on time of the MOS transistor is determined by the comparison result

To protect the current comparator input from negative pulses a current source is inserted which sends current out of the ISENSE pin every time when V_{ISENSE} -signal is falling below ground potential. An internal RC-filter is connected at the ISENSE pin which smoothes the switch-on current spike. The remaining switch-on current spike is blanked out via a leading edge blanking circuit with a blanking time of typ. 200 ns.

The RS Flip-Flop ensures that only one single switch-on and switch-off pulse appears at the gate drive output during a given cycle (double pulse suppression).

2.7 Zero Current Detector

The zero current detector senses the inductor current via an auxiliary winding and ensures that the next on-time of the MOSFET is initiated immediately when the inductor current has reached zero. This reduces the reverse recovery losses of the boost converter diode to a minimum. The MOSFET is switched off when the voltage drop of the shunt resistor exceeds the voltage level of the multiplier output. So the boost current waveform has a triangular shape and there are no deadtime gaps between the cycles. This leads to a continuous AC line current limiting the peak current to twice of the average current.

Functional Description

To prevent false tripping the zero current detector is designed as a Schmitt-Trigger with a hysteresis of 0.5 V. An internal 5 V clamp protects the input from overvoltage breakdown, a 0.6 V clamp prevents substrate injection. An external resistor has to be used in series with the auxiliary winding to limit the current through the clamps.

2.8 Restart Timer

The restart timer function eliminates the need of an oscillator. The timer starts or restarts the TDA4863 when the driver output has been off for more than 150 μs after the inductor current reaches zero.

2.9 Undervoltage Lockout

An undervoltage lockout circuitry switches the IC on when V_{CC} reaches the upper threshold V_{CCH} and switches the IC off when V_{CC} is falling below the lower threshold V_{CCL} . During start up the supply current is less than 100 μA .

An internal voltage clamp has been added to protect the IC from V_{CC} overvoltage condition. When using this clamp special care must be taken on power dissipation.

Start up current is provided by an external start up resistor which is connected from the AC line to the input supply voltage V_{CC} and a storage capacitor which is connected from V_{CC} to ground. Be aware that this capacitor is discharged before the IC is plugged into the application board. Otherwise the IC can be destroyed due to the high capacitor voltage.

Bootstrap power supply is created with the previous mentioned auxiliary winding and a diode (see [“Application Circuit” on Page 21](#)).

2.10 Gate Drive

The TDA4863 totem pole output stage is MOSFET compatible. An internal protection circuitry is activated when V_{CC} is within the start up phase and ensures that the MOSFET is turned off. The totem pole output has been optimized to minimize cross conduction current during high speed operation.

2.11 Signal Diagrams

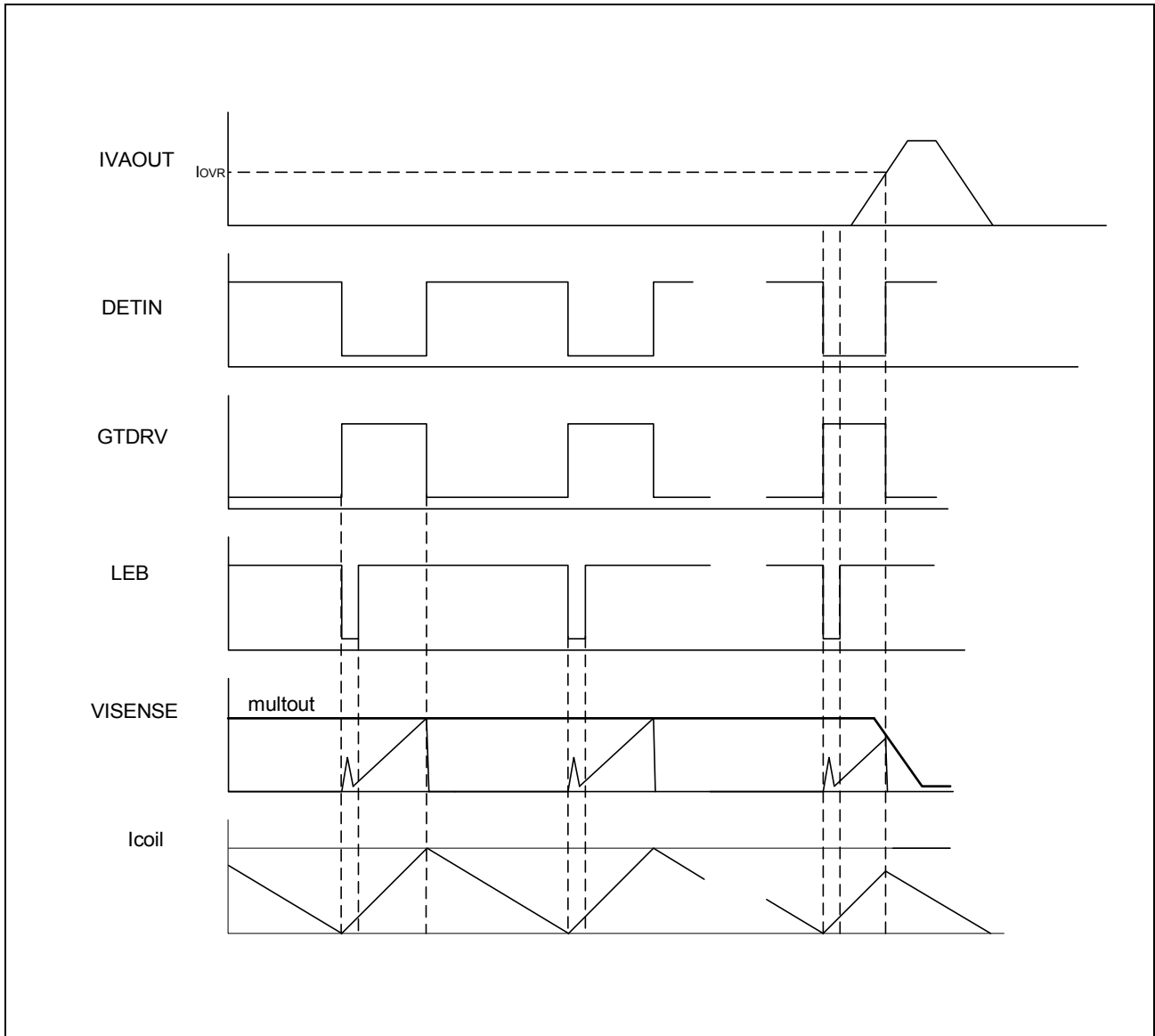


Figure 4 Typical signals

3 Electrical Characteristics

3.1 Absolute Maximum Ratings

Parameter	Symbol	Limit Values		Unit	Remarks
		min.	max.		
Supply + Zener Current	$I_{CCH} + I_Z$		20	mA	
Supply Voltage	V_{CC}	-0.3	V_Z	V	$V_Z = \text{Zener Voltage}$ $I_{CC} + I_Z = 20 \text{ mA}$
Voltage at Pin 1,3,4		-0.3	6.5		
Current into Pin 2	I_{VAOUT}	-10	40	mA	$V_{VAOUT} = 4 \text{ V}$, $V_{VSENSE} = 2.8 \text{ V}$ $V_{VAOUT} = 0 \text{ V}$, $V_{VSENSE} = 2.3 \text{ V}$ $t < 1 \text{ ms}$
Current into Pin 5	I_{DETIN}	-10	10		$DETIN > 6 \text{ V}$ $DETIN < 0.4 \text{ V}$ $t < 1 \text{ ms}$
Current into Pin 7	I_{GTDRV}	-500	500		$t < 1 \text{ ms}$
ESD Protection			2000	V	MIL STD 883C method 3015.6, 100 pF, 1500 Ω
Storage Temperature	T_{stg}	-50	150	$^{\circ}\text{C}$	
Operating Junction Temperature	T_J	-40	150		
Thermal Resistance Junction-Ambient	R_{thJA}		100 180	K/W	P-DIP-8-4 P-DSO-8-3

Electrical Characteristics
3.2 Characteristics

 Unless otherwise stated, $-40^{\circ}\text{C} < T_j < 150^{\circ}\text{C}$, $V_{CC} = 14.5\text{ V}$

Parameter	Symbol	Limit Values			Unit	Test Condition
		min.	typ.	max.		
Start-Up circuit						
Zener Voltage	V_Z	18	20	22	V	$I_{CC} + I_Z = 20\text{ mA}$
Start-up Supply Current	I_{CCL}		20	100	μA	$V_{CC} = V_{CCON} - 0.5\text{ V}$
Operating Supply Current	I_{CCH}		4	6	mA	Output low
V_{CC} Turn-ON Threshold	V_{CCON}	12	12.5	13	V	
V_{CC} Turn-OFF Threshold	V_{CCOFF}	9.5	10	10.5		
V_{CC} Hysteresis	V_{CCHY}		2.5			
Voltage Amplifier						
Voltage feedback Input Threshold	V_{FB}	2.45	2.5	2.55	V	
Line Regulation	V_{FBLR}			5	mV	$V_{CC} = 12\text{ V to }16\text{ V}$
Open Loop Voltage Gain ¹⁾	G_V		100		dB	
Unity Gain Bandwidth ¹⁾	B_W		5		MHz	
Phase Margin ¹⁾	M		80		Degr	
Bias Current VSENSE	$I_{BVSENSE}$	-1.0	-0.3		μA	
Enable Threshold	V_{VSENSE}	0.17	0.2	0.25	V	
Inhibit Threshold Voltage	V_{VAOUTI}	2.1	2.2	2.3		$V_{ISENSE} = -0.38\text{ V}$
Inhibit Time Delay	t_{dVA}		3		μs	$V_{ISENSE} = -0.38\text{ V}$
Output Current Source	I_{VAOUTH}		-6		mA	$V_{VAOUT} = 0\text{ V}$ $V_{VSENSE} = 2.3\text{ V}$, $t < 1\text{ ms}$
Output Current Sink	I_{VAOUTL}		35			$V_{VAOUT} = 4\text{ V}$ $V_{VSENSE} = 2.8\text{ V}$, $t < 1\text{ ms}$
Upper Clamp Voltage	V_{VAOUTH}	4.8	5.4	6.0	V	$V_{VSENSE} = 2.3\text{ V}$, $I_{VAOUT} = -0.2\text{ mA}$
Lower Clamp Voltage	V_{VAOUTL}	0.8	1.1	1.4	V	$V_{VSENSE} = 2.8\text{ V}$, $I_{VAOUT} = 0.5\text{ mA}$

¹⁾ Guaranteed by design, not tested

Electrical Characteristics
3.2 Characteristics (cont'd)

 Unless otherwise stated, $-40^{\circ}\text{C} < T_j < 150^{\circ}\text{C}$, $V_{CC} = 14.5\text{ V}$

Parameter	Symbol	Limit Values			Unit	Test Condition
		min.	typ.	max.		

Overvoltage Regulator

Threshold Current	I_{OVR}	35	40	45	μA	$T_j = 25^{\circ}\text{C}$, $V_{VAOUT} = 3.5\text{ V}$
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Current Comparator

Input Bias Current	$I_{BISENSE}$	-1	-0.2	1	μA	$V_{ISENSE} = 0\text{ V}$
Input Offset Voltage ($T_j = 25^{\circ}\text{C}$)	$V_{ISENSEO}$		25		mV	$V_{VAOUT} = 2.7\text{ V}$ $V_{MULTIN} = 0\text{ V}$
Max Threshold Voltage	$V_{ISENSEM}$	0.95	1.0	1.05	V	
Threshold at OVR	$V_{ISENOVR}$		0.05			$I_{OVR} = 50\ \mu\text{A}$
Leading Edge Blanking	t_{LEB}	100	200	300	ns	
Shut Down Delay	t_{DISG}		80	130		

Detector

Upper Threshold Voltage	V_{DETINU}		1.5	1.6	V	
Lower Threshold Voltage	V_{DETINL}	0.95	1.1			
Hysteresis	$V_{DETINHY}$	0.25	0.4	0.55		
Input Current	I_{BDETIN}	-1	-0.2	1	μA	$V_{DETIN} = 2\text{ V}$
Input Clamp Voltage High State	$V_{DETINHC}$	4.5	4.9	5.4	V	$I_{DETIN} = 5\text{ mA}$
Low State	$V_{DETINLC}$	0.1	0.4	0.7		$I_{DETIN} = -5\text{ mA}$

Multiplier

Input bias current	$I_{BMULTIN}$	-1	-0.2	1	μA	$V_{MULTIN} = 0\text{ V}$
Dynamic voltage range MULTIN	V_{MULTIN}		0 to 4		V	$V_{VAOUT} = 2.75\text{ V}$
Dynamic voltage range VAOUT	V_{VAOUT}		V_{FB} to $V_{FB} + 1.5$			$V_{MULTIN} = 1\text{ V}$
Multiplier Gain	K_{low} K_{high}		0.3 0.7			$V_{VAOUT} < 3\text{ V}$, $V_{MULTIN} = 1\text{ V}$ $V_{VAOUT} > 3.5\text{ V}$, $V_{MULTIN} = 1\text{ V}$

 $K = \Delta V_{ISENSE} / \Delta V_{VAOUT}$ at $V_{MULTIN} = \text{constant}$

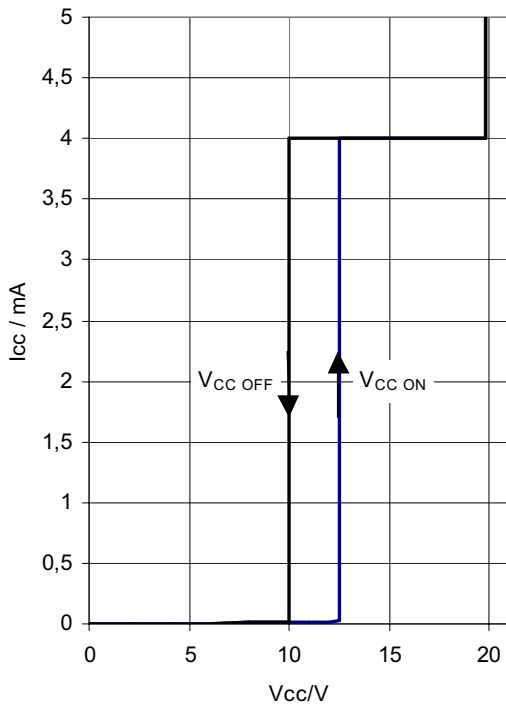
Electrical Characteristics
3.2 Characteristics (cont'd)

 Unless otherwise stated, $-40^{\circ}\text{C} < T_j < 150^{\circ}\text{C}$, $V_{CC} = 14.5\text{ V}$

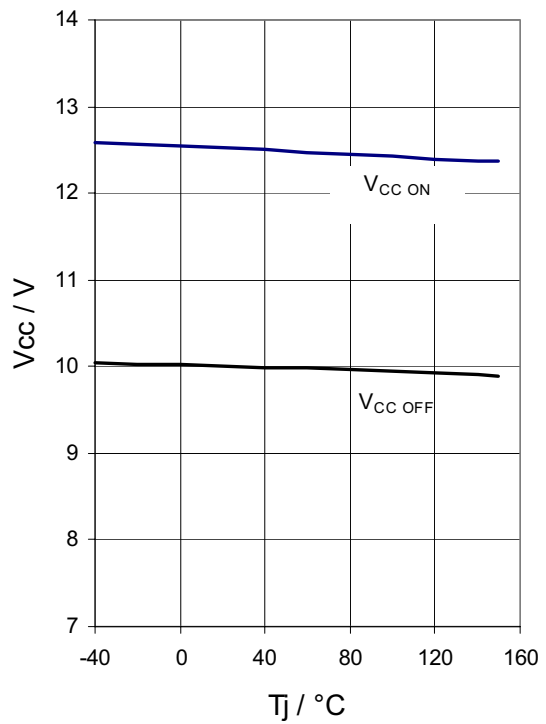
Parameter	Symbol	Limit Values			Unit	Test Condition
		min.	typ.	max.		
Restart Timer						
Restart time	t_{RES}	100	160	250	μs	
Gate Drive						
Output voltage low state	V_{GTL}		0.3		V	$I_{GT} = 0\text{ mA}$
Output voltage low state	V_{GTL}		1.0		V	$I_{GT} = 2\text{ mA}$
			1.7			$I_{GT} = 20\text{ mA}$
			2.2			$I_{GT} = 200\text{ mA}$
Output voltage high state	V_{GTH}		10.8		ns	$I_{GT} = -5\text{ mA}$, see “Gate Drive Voltage High State versus V_{CC}” on Page 20
Output voltage active shut down	V_{GTSD}		1	1.25		$I_{GT} = 20\text{ mA}$, $V_{CC} = 9\text{ V}$
Rise time	t_{rise}		80	130		$C_{GT} = 4.7\text{ nF}$
Fall time	t_{fall}		55	130		$V_{GT} = 2\dots 8\text{ V}$

3.3 Electrical Diagrams

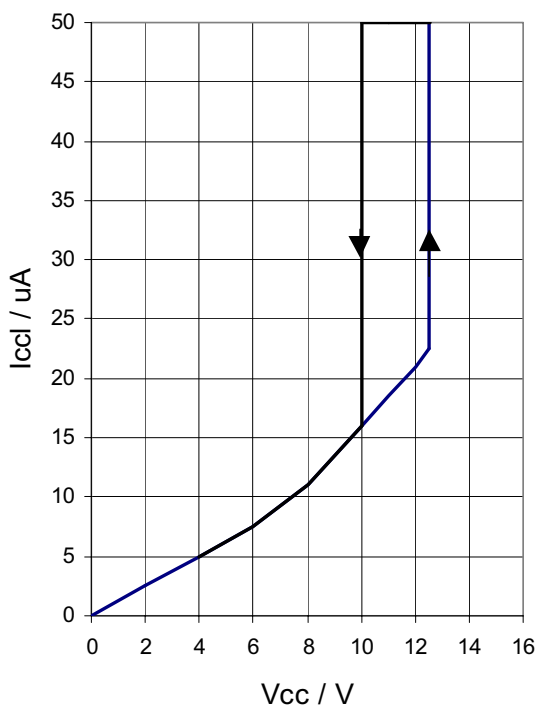
I_{CC} versus V_{CC}



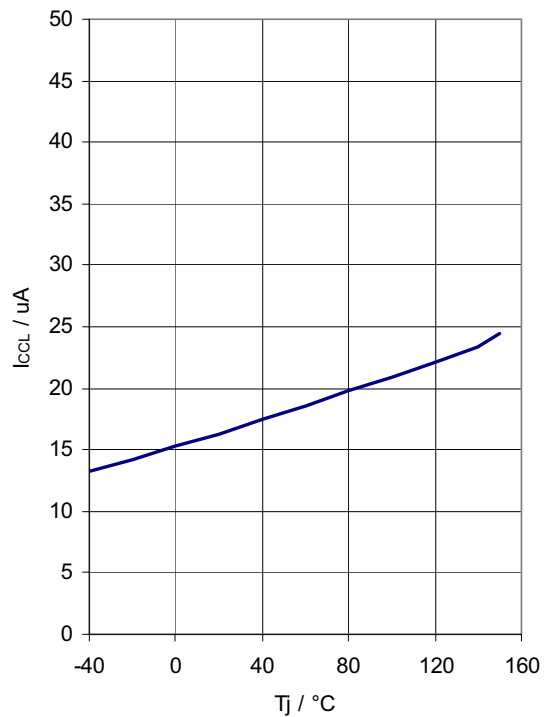
$V_{CCON/OFF}$ versus Temperature



I_{CCL} versus V_{CC}

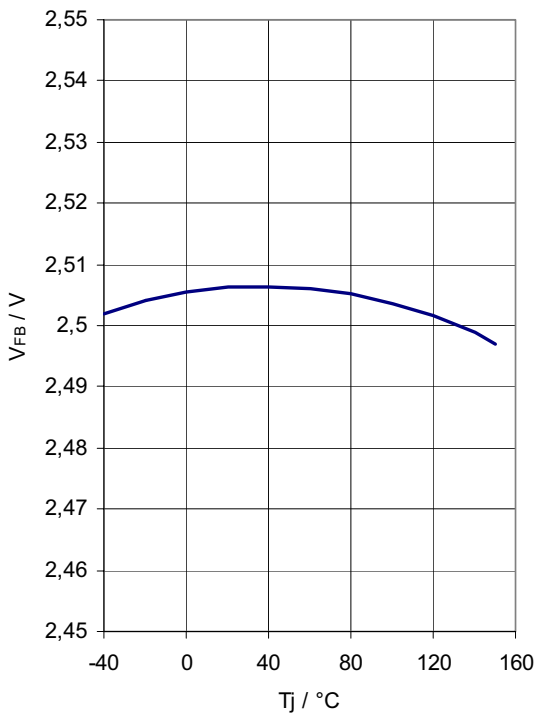


I_{CCL} versus Temperature, $V_{CC} = 10\text{ V}$

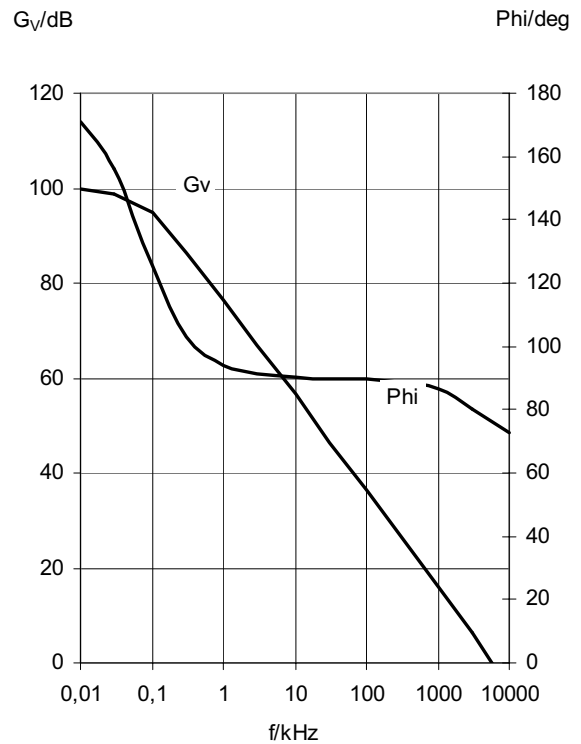


Electrical Characteristics

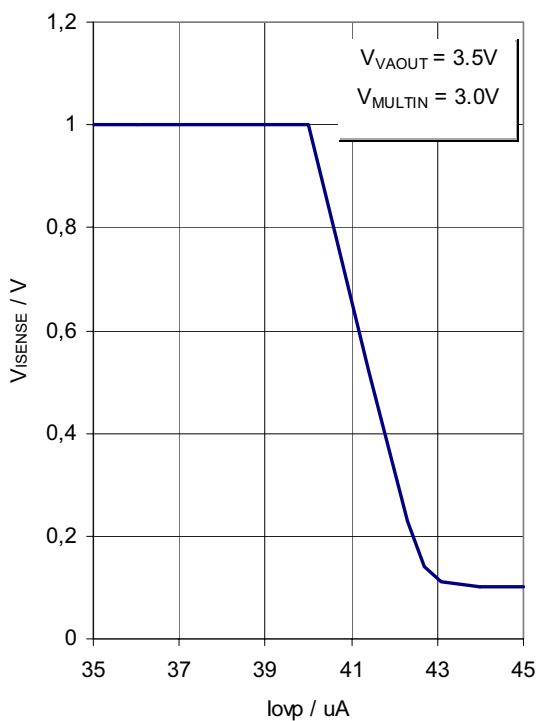
**V_{FB} versus Temperature
(pin1 connected to pin2)**



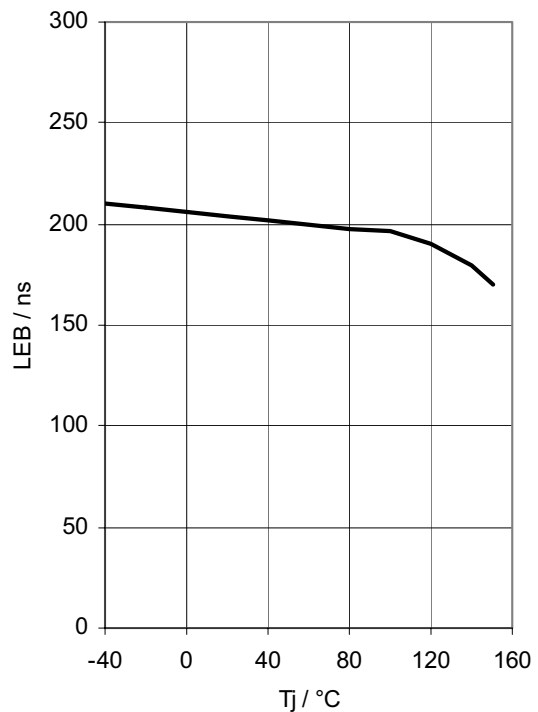
Open Loop Gain and Phase versus Frequency



Overvoltage Regulator V_{ISENSE} versus Threshold Voltage

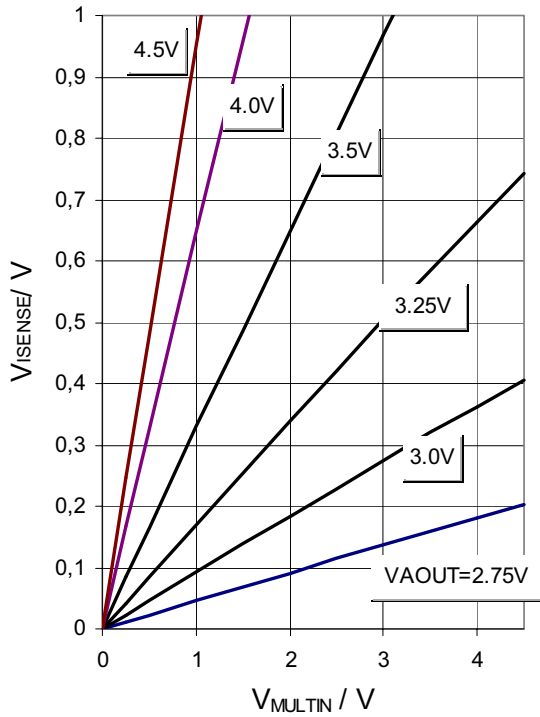


Leading Edge Blanking versus Temperature

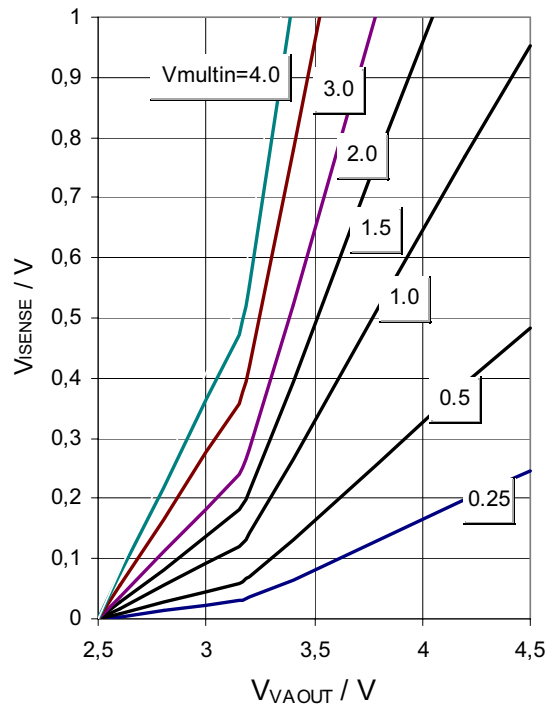


Electrical Characteristics

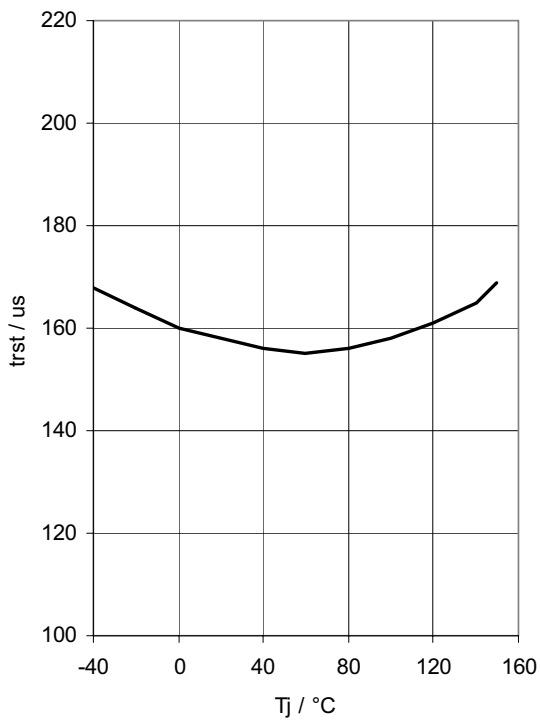
Current Sense Threshold V_{ISENSE} versus V_{MULTIN}



Current Sense Threshold V_{ISENSE} versus V_{VAOUT}

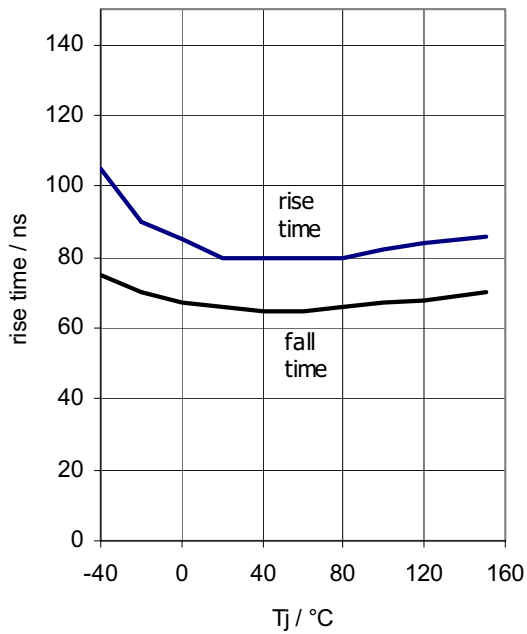


Restart Time versus Temperature

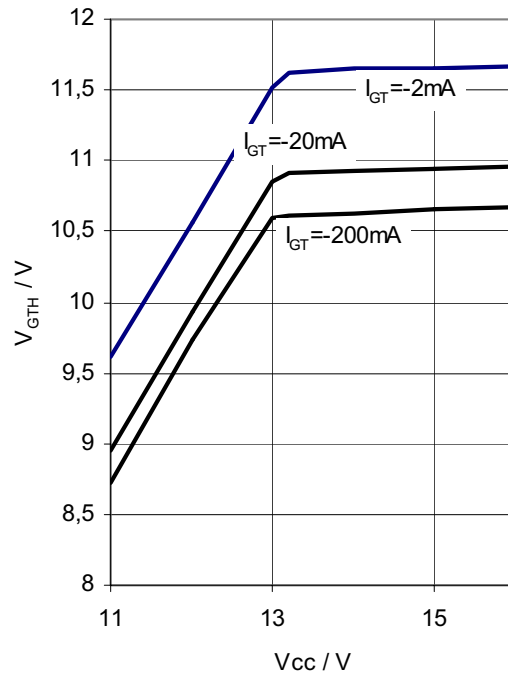


Electrical Characteristics

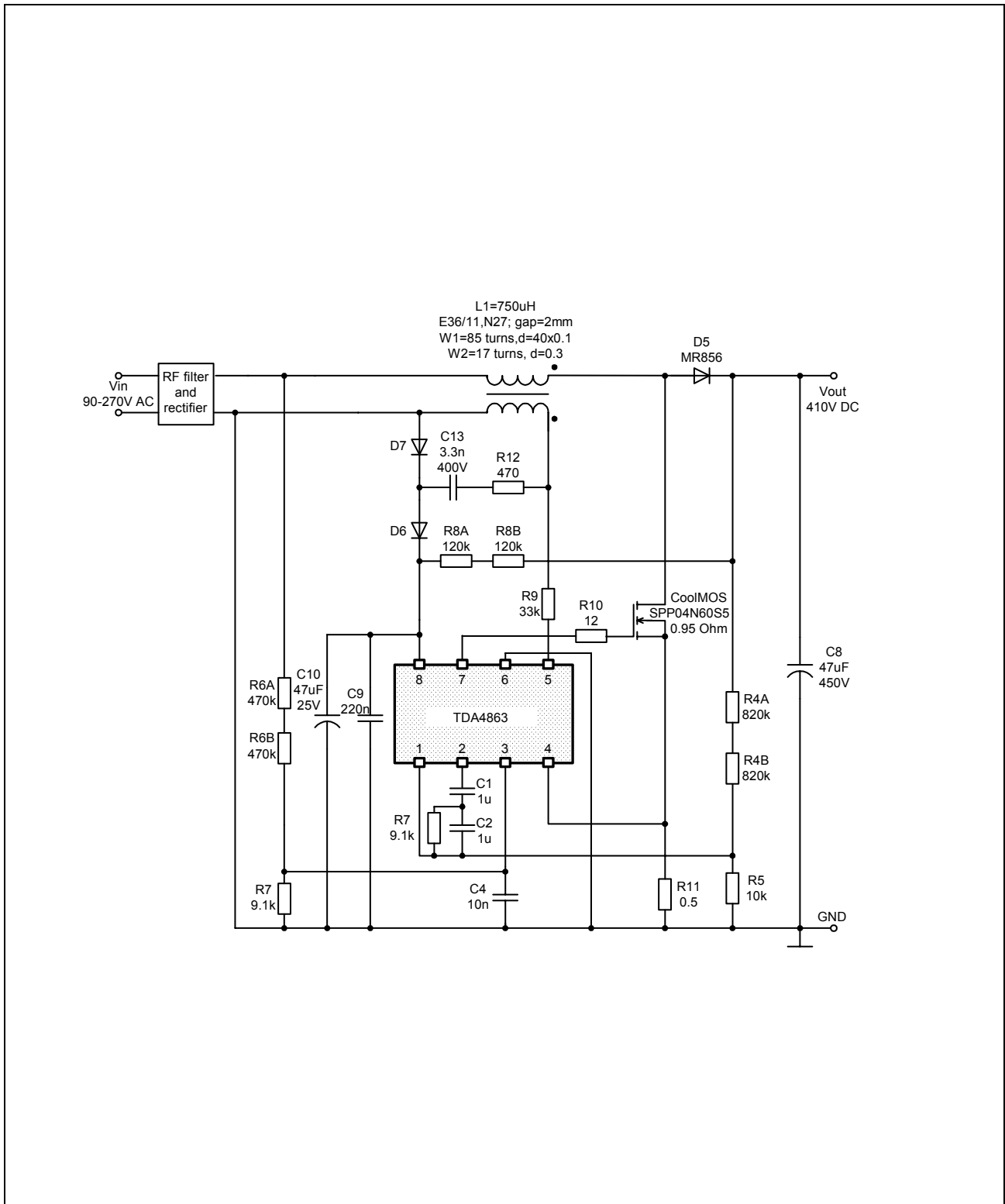
Gate Drive Rise Time and Fall Time versus Temperature



Gate Drive Voltage High State versus V_{cc}



4 Application Circuit



4.1 Results of THD Measurements with Application Board $P_{out} = 110\text{ W}$

(Measurements according to IEC61000-3-2.

150% limit (red line): Momentary measured value must be below this limit.

100% limit (blue line): Average of measured values must be below this limit.

The worst measured momentary value is shown in the diagrams.)

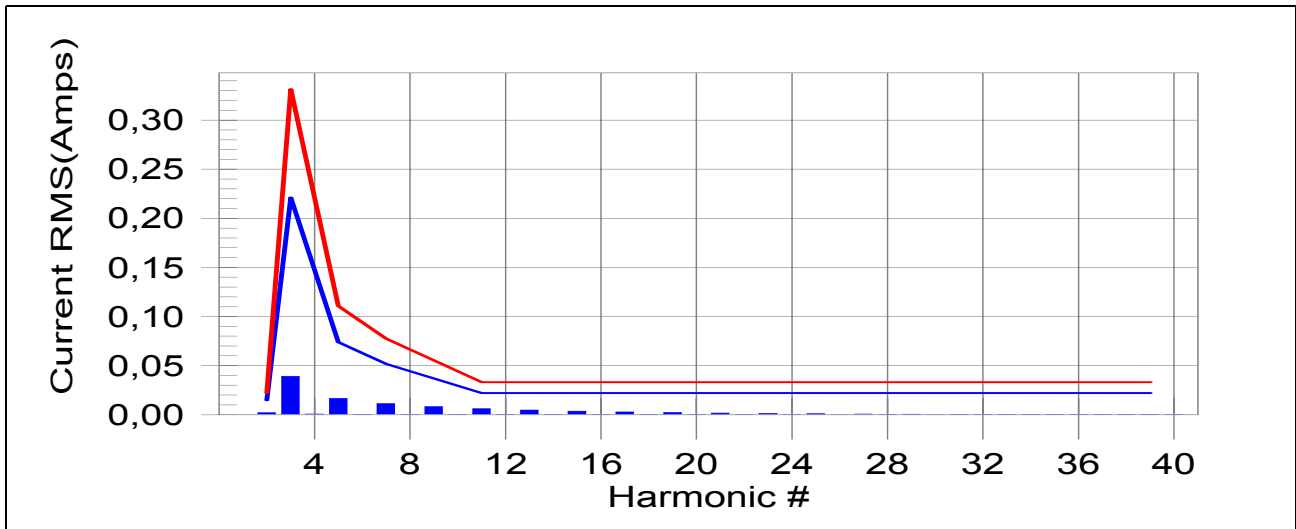


Figure 6 THD Class C:
 $P_{max} = 110\text{ W}$, $V_{inac} = 90\text{ V}$, $I_{out} = 250\text{ mA}$, $V_{out} = 420\text{ V}$, $PF = 0.998$

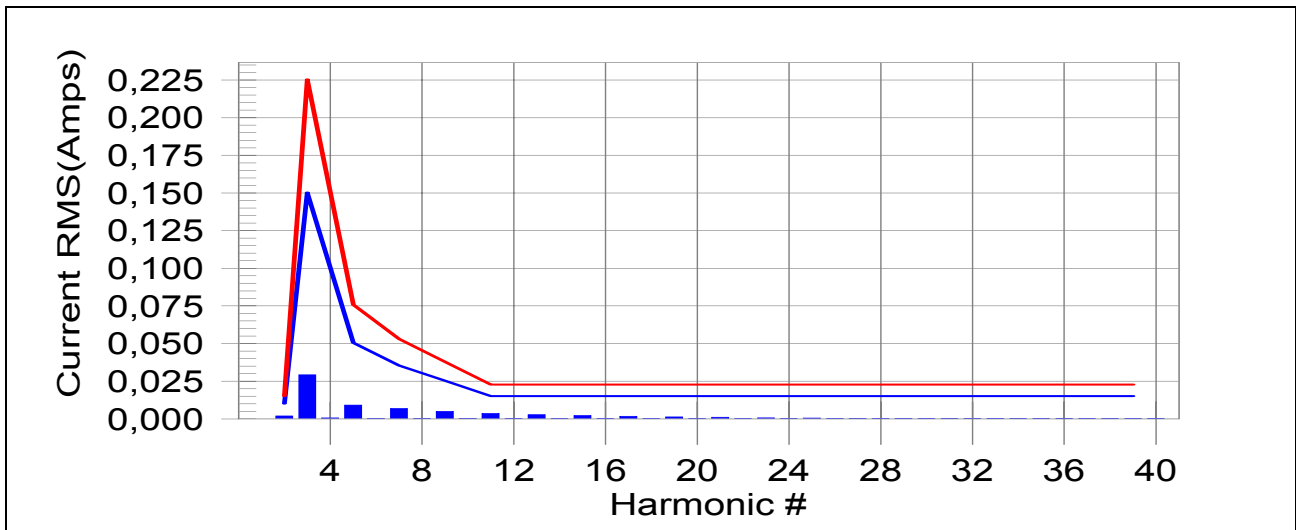


Figure 7 THD Class C:
 $P_{max} = 110\text{ W}$, $V_{inac} = 220\text{ V}$, $I_{out} = 250\text{ mA}$, $V_{aout} = 420\text{ V}$, $PF = 0.992$

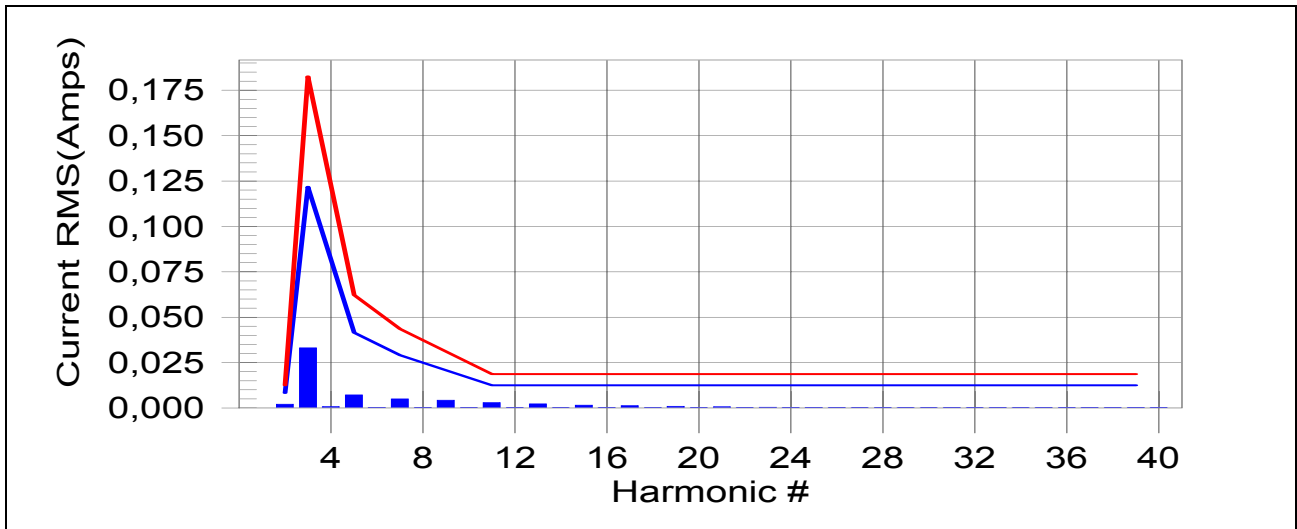


Figure 8 THD Class C:
 $P_{max} = 110 \text{ W}$, $V_{inac} = 270 \text{ V}$, $I_{out} = 250 \text{ mA}$, $V_{aout} = 420 \text{ V}$, $PF = 0.978$

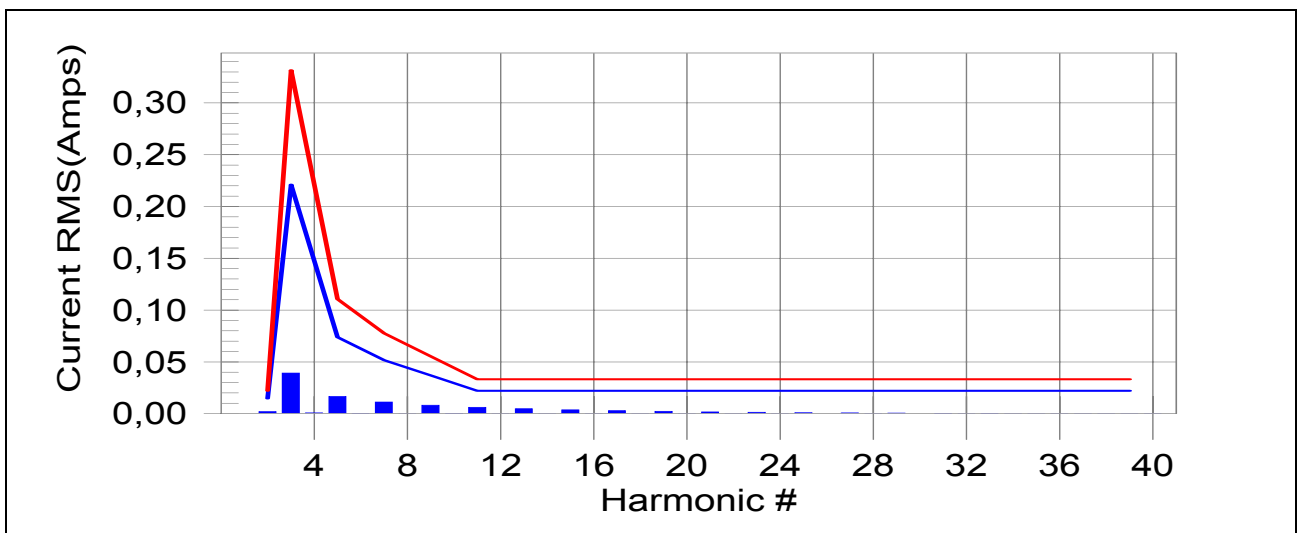


Figure 9 THD Class C:
 $P_{max} = 110 \text{ W}$, $V_{inac} = 90 \text{ V}$, $I_{out} = 140 \text{ mA}$, $V_{aout} = 420 \text{ V}$, $PF = 0.999$

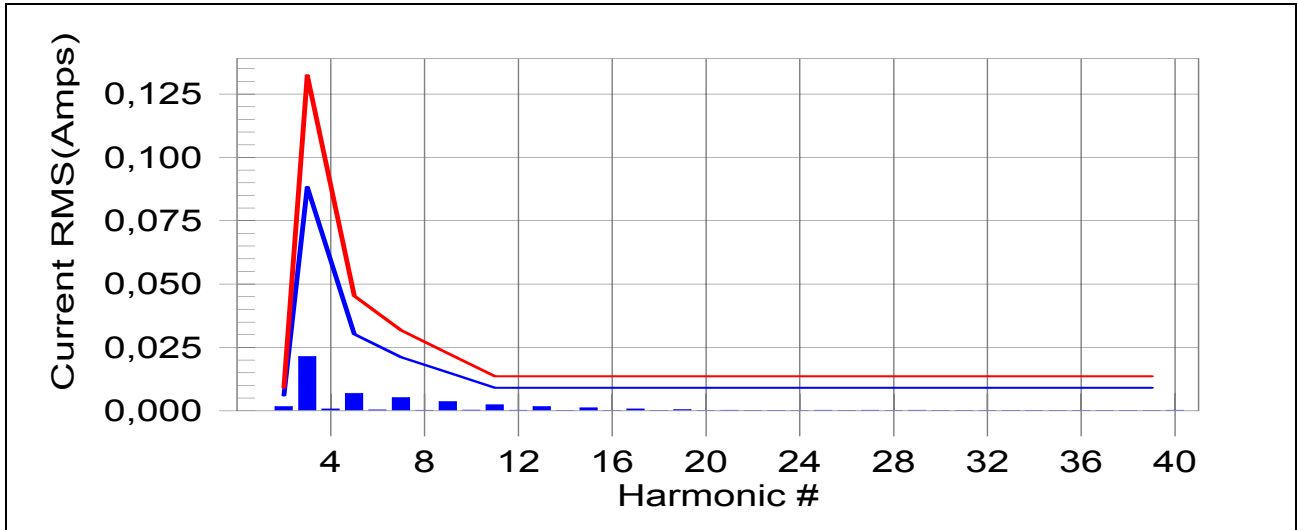


Figure 10 THD Class C:

$P_{max} = 110 \text{ W}$, $V_{inac} = 220 \text{ V}$, $I_{out} = 140 \text{ mA}$, $V_{aout} = 420 \text{ V}$, $PF = 0.975$

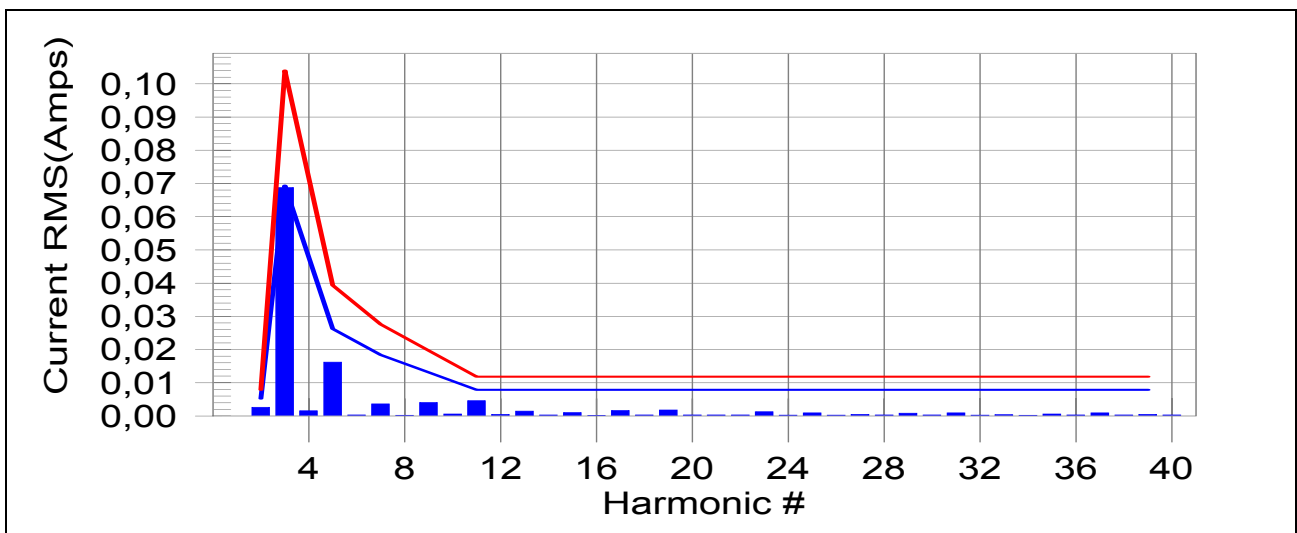
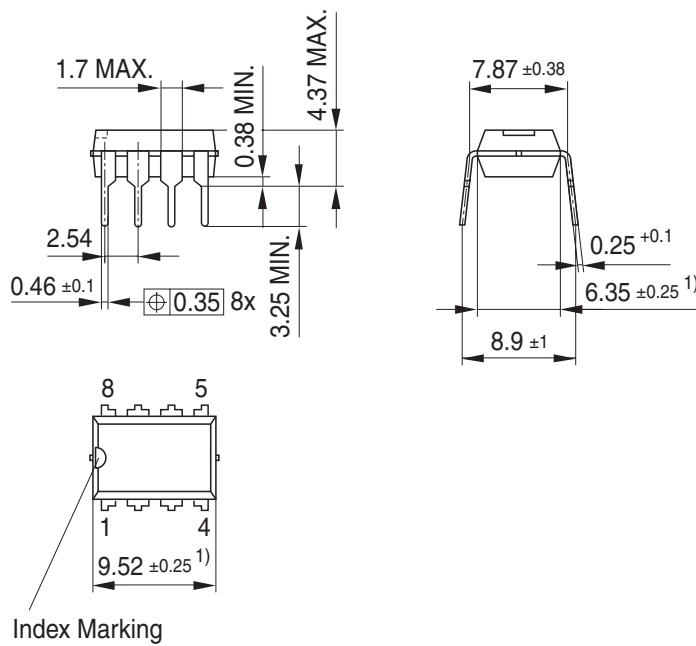


Figure 11 THD Class C:

$P_{max} = 110 \text{ W}$, $V_{inac} = 270 \text{ V}$, $I_{out} = 140 \text{ mA}$, $V_{aout} = 420 \text{ V}$, $PF = 0.883$

5 Package Outlines

P-DIP-8-4 (Plastic Dual In-line Package)

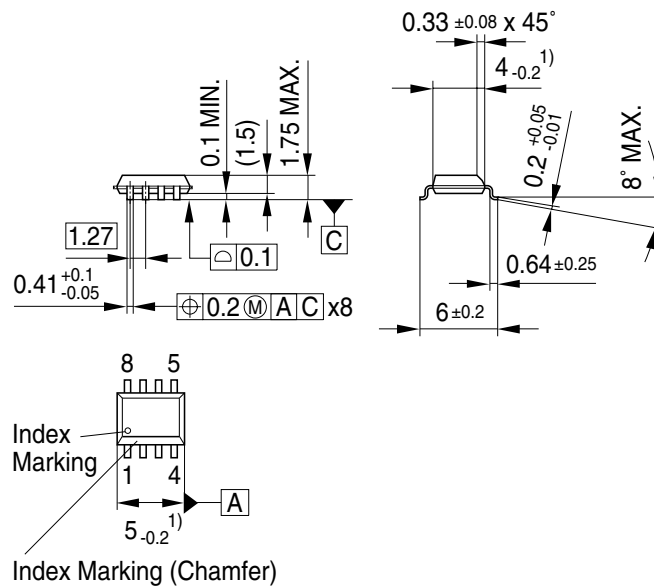


¹⁾ Does not include plastic or metal protrusion of 0.25 max. per side

GPD05583

Figure 12

P-DSO-8-3
(Plastic Dual Small Outline)



¹⁾ Does not include plastic or metal protrusion of 0.15 max. per side

GPS09032

Figure 13

You can find all of our packages, sorts of packing and others in our Infineon Internet Page “Products”: <http://www.infineon.com/products>.

Dimensions in mm

Infineon goes for Business Excellence

“Business excellence means intelligent approaches and clearly defined processes, which are both constantly under review and ultimately lead to good operating results.

Better operating results and business excellence mean less idleness and wastefulness for all of us, more professional success, more accurate information, a better overview and, thereby, less frustration and more satisfaction.”

Dr. Ulrich Schumacher

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