

ACT4060

ACT4060 WIDE INPUT 2A STEP DOWN CONVERTER

FEATURES

- **2A Output Current**
- **Up to 95% Efficiency**
- **4.75V to 20V Input Range**
- **8µA Shutdown Supply Current**
- **410kHz Switching Frequency**
- **Adjustable Output Voltage**
- **Cycle-by-Cycle Current Limit Protection**
- **Thermal Shutdown Protection**
- **Frequency Fold Back at Short Circuit**
- Stability with Wide Range of Capacitors. **Including Low ESR Ceramic Capacitors**
- **SOP-8 Package**

APPLICATIONS

- **TFT LCD Monitors**
- **Portable DVDs**
- **Car-Powered or Battery-Powered Equipments**
- **Set-Top Boxes**
- Telecom Power Supplies
- **DSL and Cable Modems and Routers**
- **Termination Supplies**

GENERAL DESCRIPTION

The ACT4060 is a current-mode step-down DC-DC converter that generates up to 2A output current at 410kHz switching frequency. The
device utilizes Active-Semi's proprietary device utilizes Active-Semi's proprietary ISOBCD20 process for operation with input voltage up to 20V.

Consuming only 8μA in shutdown mode, the ACT4060 is highly efficient with peak efficiency at 95% when in operation. Protection features include cycle-by-cycle current limit, thermal shutdown, and frequency fold back at short circuit.

The ACT4060 is available in SOP-8 package and requires very few external devices for operation.

Figure 1. Typical Application Circuit

ORDERING INFORMATION

PIN CONFIGURATION

PIN DESCRIPTION

ABSOLUTE MAXIMUM RATINGS

(Note: Do not exceed these limits to prevent damage to the device. Exposure to absolute maximum rating conditions for long periods may affect device reliability.)

ELECTRICAL CHARACTERISTICS

(V_{IN} = 12V, T_J = 25°C unless otherwise specified)

FUNCTIONAL DESCRIPTION

As seen in Figure 2, *Functional Block Diagram*, the ACT4060 is a current mode pulse width modulation (PWM) converter. The converter operates as follows:

A switching cycle starts when the rising edge of the Oscillator clock output causes the High-Side Power Switch to turn on and the Low-Side Power Switch to turn off. With the SW side of the inductor now connected to IN, the inductor current ramps up to store energy in the its magnetic field. The inductor current level is measured by the Current Sense Amplifier and added to the Oscillator ramp signal. If the resulting summation is higher than the COMP voltage, the output of the PWM Comparator goes high. When this happens or when Oscillator clock output goes low, the High-Side Power Switch turns off and the Low-Side Power Switch turns on. At this point, the SW side of the inductor swings to a diode voltage below ground, causing the inductor current to decrease and magnetic energy to be transferred to output. This state continues until the cycle starts again.

The High-Side Power Switch is driven by logic using BS bootstrap pin as the positive rail. This pin is charged to V_{SW} + 6V when the Low-Side Power Switch turns on.

The COMP voltage is the integration of the error between FB input and the internal 1.293V reference. If FB is lower than the reference voltage, COMP tends to go higher to increase current to the output. Current limit happens when COMP reaches its maximum clamp value of 2.55V.

The Oscillator normally switches at 410kHz. However, if FB voltage is less than 0.7V, then the switching frequency decreases until it reaches a minimum of 50kHz at $V_{FB} = 0.5V$.

SHUTDOWN CONTROL

The ACT4060 has an enable input EN for turning the IC on or off. When EN is less than 0.7V, the IC is in 8μA low current shutdown mode and output is discharged through the Low-Side Power Switch. When EN is higher than 1.3V, the IC is in normal operation mode. EN is internally pulled up with a 1μA current source and can be left unconnected for always-on operation. Note that EN is a low voltage input with a maximum voltage of 6V; it should never be directly connected to IN.

THERMAL SHUTDOWN

The ACT4060 automatically turns off when its junction temperature exceeds 160°C.

APPLICATION INFORMATION

Figure 3. Output Voltage Setting

Figure 3 shows the connections for setting the output voltage. Select the proper ratio of the two feedback resistors RFB1 and RFB2 based on the output voltage. Typically, use $R_{FB2} \approx 10 \text{k}\Omega$ and determine R_{FB1} from the output voltage:

$$
R_{FB1} = R_{FB2} \left(\frac{V_{OUT}}{1.293V} - 1 \right) \tag{1}
$$

INDUCTOR SELECTION

The inductor maintains a continuous current to the output load. This inductor current has a ripple that is dependent on the inductance value: higher inductance reduces the peak-to-peak ripple current. The trade off for high inductance value is the increase in inductor core size and series resistance, and the reduction in current handling capability. In general, select an inductance value L based on ripple current requirement:

$$
L = \frac{V_{OUT} \bullet (V_{IN} - V_{OUT})}{V_{IN}f_{SW}I_{OUTMAX}K_{RIPILE}}
$$
 (2)

where V_{IN} is the input voltage, V_{OUT} is the output voltage, f_{SW} is the switching frequency, I_{OUTMAX} is the maximum output current, and KRIPPLE is the ripple factor. Typically, choose K_{RIPPLE} = 30% to correspond to the peak-to-peak ripple current being 30% of the maximum output current.

With this inductor value (Table 1), the peak inductor current is $I_{\text{OUT}} \cdot (1 + K_{\text{RIPPLE}} / 2)$. Make sure that this peak inductor current is less that the 3A current limit. Finally, select the inductor core size so that it does not saturate at 3A.

Table 1. Typical Inductor Values

V_{OUT}		$1.5V$ 1.8V 2.5V 3.3V 5V		
	$ 6.8$ µH $ 6.8$ µH $ 10$ µH $ 15$ µH $ 22$ µH $ $			

INPUT CAPACITOR

The input capacitor needs to be carefully selected to maintain sufficiently low ripple at the supply input of the converter. A low ESR capacitor is highly recommended. Since large current flows in and out of this capacitor during switching, its ESR also affects efficiency.

The input capacitance needs to be higher than 10µF. The best choice is the ceramic type; however, low ESR tantalum or electrolytic types may also be used provided that the RMS ripple current rating is higher than 50% of the output current. The input capacitor should be placed close to the IN and G pins of the IC, with shortest traces possible. In the case of tantalum or electrolytic types, they can be further away if a small parallel 0.1μ F ceramic capacitor is placed right next to the IC.

OUTPUT CAPACITOR

The output capacitor also needs to have low ESR to keep low output voltage ripple. The output ripple voltage is:

$$
V_{RIPPLE} = I_{OUTMAX} K_{RIPPLE} R_{ESR}
$$

+
$$
\frac{V_{IN}}{28 \cdot f_{SW}^2 LC_{OUT}}
$$
 (3)

where I_{OUTMAX} is the maximum output current. KRIPPLE is the ripple factor, RESR is the ESR $resistance$ of the output capacitor, f_{SW} is the switching frequency, L in the inductor value, C_{OUT} is the output capacitance. In the case of ceramic output capacitors, R_{ESR} is very small and does not contribute to the ripple. Therefore, a lower capacitance value can be used for ceramic type. In the case of tantalum or electrolytic type, the ripple is dominated by R_{ESR} multiplied by the ripple current. In that case, the output capacitor is chosen to have sufficiently low ESR.

For ceramic output type, typically choose a capacitance of about 22µF. For tantalum or electrolytic type, choose a capacitor with less than 50mΩ ESR.

RECTIFIER DIODE

Use a Schottky diode as the rectifier to conduct current when the High-Side Power Switch is off. The Schottky diode must have current rating higher than the maximum output current and the reverse voltage rating higher than the maximum input voltage.

STABILITY COMPENSATION

 † C_{COMP2} is needed only for high ESR output capacitor

Figure 4. Stability Compensation

The feedback system of the IC is stabilized by the components at COMP pin, as shown in Figure 4. The DC loop gain of the system is determined by the following equation:

$$
A_{VDC} = \frac{1.3V}{I_{OUT}} A_{VEA} G_{COMP}
$$
 (4)

The dominant pole P1 is due to CCOMP:

$$
f_{P1} = \frac{G_{EA}}{2\pi A_{VEA} C_{COMP}}\tag{5}
$$

The second pole P2 is the output pole:

$$
f_{P2} = \frac{I_{OUT}}{2\pi V_{OUT}C_{OUT}}\tag{6}
$$

The first zero $Z1$ is due to R_{COMP} and C_{COMP} :

$$
f_{Z1} = \frac{1}{2\pi R_{COMP}C_{COMP}}\tag{7}
$$

And finally, the third pole is due to R_{COMP} and CCOMP2 (if CCOMP2 is used):

$$
f_{P3} = \frac{1}{2\pi R_{COMP}C_{COMP2}}\tag{8}
$$

Follow the following steps to compensate the IC:

STEP 1. Set the cross over frequency at 1/10 of the switching frequency via R_{COMP}:

$$
R_{COMP} = \frac{2\pi V_{OUT}C_{OUT}f_{SW}}{10G_{EA}G_{COMP} \cdot 1.3V}
$$

$$
= 1.7 \times 10^8 V_{OUT}C_{OUT} \qquad (\Omega)
$$
 (9)

but limit R_{COMP} to 15kΩ maximum.

STEP 2. Set the zero f_{Z1} at 1/4 of the cross over frequency. If R_{COMP} is less than 15 $k\Omega$, the equation for C_{COMP} is:

$$
C_{COMP} = \frac{1.8 \times 10^{-5}}{R_{COMP}} \qquad (F)
$$
 (10)

If R_{coMP} is limited to 15kΩ, then the actual cross over frequency is 3.4 / $(V_{\text{OUT}}C_{\text{OUT}})$. Therefore:

$$
C_{COMP} = 1.2 \times 10^{-5} V_{OUT} C_{OUT} \qquad (F) \qquad (11)
$$

STEP 3. If the output capacitor's ESR is high enough to cause a zero at lower than 4 times the cross over frequency, an additional compensation capacitor C_{comp2} is required. The condition for using C_{COMP2} is:

RESRCOUT

$$
\geq Min \left(\frac{1.1 \times 10^{-6}}{C_{OUT}} , 0.012 \cdot V_{OUT} \right) \qquad (\Omega) \qquad (12)
$$

And the proper value for C_{COMP2} is:

$$
C_{COMP2} = \frac{C_{OUT}R_{ESRCOUT}}{R_{COMP}} \tag{13}
$$

Though C_{COMP2} is unnecessary when the output capacitor has sufficiently low ESR, a small value C_{COMP2} such as 100pF may improve stability against PCB layout parasitic effects.

Table 2 shows some calculated results based on the compensation method above.

Table 2. Typical Compensation for Different Output Voltages and Output Capacitors

VOUT	C_{OUT}	R _{COMP}	C_{COMP}	C_{COMP2}
2.5V	22µF Ceramic	$8.2k\Omega$	2.2nF	None
3.3V	22µF Ceramic	$12k\Omega$	1.5nF	None
5V	22µF Ceramic	$15k\Omega$	1.5nF	None
2.5V	47µF SP Cap	$15k\Omega$	1.5nF	None
3.3V	47µF SP Cap	$15k\Omega$	1.8nF	None
5V	47µF SP Cap	$15k\Omega$	2.7nF	None
2.5V	470μF/6.3V/30mΩ	$15k\Omega$	15nF	1nF
3.3V	470μF/6.3V/30mΩ	$15k\Omega$	22nF	1nF
5V	470μF/10V/30mΩ	$15k\Omega$	27nF	None

Figure 5 shows a sample ACT4060 application circuit generating 2.5V/2A output.

TYPICAL PERFORMANCE CHARACTERISTICS

Feedback Voltage vs. Junction Temperature

Shutdown Supply Current vs. Input Voltage

Switching Frequency vs. Input Voltage

PACKAGE OUTLINE

SOP-8 PACKAGE OUTLINE AND DIMENSIONS

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