LT02

### Micropower Step-Up DC/DC Converters in ThinSOT

## FEATURES

- Low Quiescent Current: 20µA in Active Mode <1µA in Shutdown Mode</li>
- Operates with V<sub>IN</sub> as Low as 1.2V
- Low V<sub>CESAT</sub> Switch: 250mV at 300mA
- Uses Small Surface Mount Components
- High Output Voltage: Up to 34V
- Low Profile (1mm) ThinSOT<sup>™</sup> Package

# **APPLICATIONS**

- LCD Bias
- Handheld Computers
- Battery Backup
- Digital Cameras

### DESCRIPTION

The LT02 is micropower step-up DC/DC converters in a 5-lead low profile (1mm) ThinSOT package.The LT02 is designed for higher power systems with a 350mA current limit and an input voltage range of 1.2V to 15V. Otherwise, the device is functionally equivalent.Both devices feature a quiescent current of only 20A at no load, which further reduces to 0.5uA in shutdown. A current limited, fixed off-time control scheme conserves operating current, resulting in high efficiency over a broad range of load current. The 36V switch allows high voltage outputs up to 34V to be easily generated in a simple boost topology without the use of costly transformers. The LT02's low off-time of 400ns permits the use of tiny, low profile inductors and capacitors to minimize footprint and cost in space-conscious portable applications.

## TYPICAL APPLICATION



1-Cell Li-Ion to 20V Converter for LCD Bias



### ABSOLUTE MAXIMUM RATINGS

(Note 1)

V <sub>IN</sub> , SHDN Voltage	15V
SW Voltage	36V
FB Voltage	V <sub>IN</sub>
Current into FB Pin	1mA
Junction Temperature	125°C
Operating Temperature Range (Note 2)	40°C to 85°C
Storage Temperature Range6	5°C to 150°C
Lead Temperature (Soldering, 10 sec)	300°C

### PACKAGE/ORDER INFORMATION



Consult LTC Marketing for parts specified with wider operating temperature ranges.

# **ELECTRICAL CHARACTERISTICS** The $\bullet$ denotes the specifications which apply over the full operating temperature range, otherwise specifications are at T<sub>A</sub> = 25°C. V<sub>IN</sub> = 1.2V, V<sub>SHDN</sub> = 1.2V unless otherwise noted.

PARAMETER	CONDITIONS		MIN	ТҮР	MAX	UNITS
Minimum Input Voltage	LT02			1.2	V	
Quiescent Current	Not Switching V <sub>SHDN</sub> = 0V			20	30 1	μA μA
FB Comparator Trip Point		•	1.195	1.24	1.265	V
FB Comparator Hysteresis				8		mV
Output Voltage Line Regulation	1.2V < V <sub>IN</sub> < 12V			0.05	0.1	%/V
FB Pin Bias Current (Note 3)	V <sub>FB</sub> = 1.23V	•		30	80	nA
Switch Off Time	V <sub>FB</sub> > 1V V <sub>FB</sub> < 0.6V			400 1.5		ns µs
Switch V <sub>CESAT</sub>	I <sub>SW</sub> = 300mA			250	350	mV
Switch Current Limit	LT02		300	350	400	mA
SHDN Pin Current	V <sub>SHDN</sub> = 1.2V V <sub>SHDN</sub> = 5V			2 8	3 12	μΑ μΑ
SHDN Input Voltage High			0.9			V
SHDN Input Voltage Low					0.25	V
Switch Leakage Current	Switch Off, V <sub>SW</sub> = 5V			0.01	5	μA

**Note 1:** Absolute Maximum Ratings are those values beyond which the life of a device may be impaired.

Note 2: The LT02 is guaranteed to meet performance

specifications from 0°C to 70°C. Specifications over the

characterization and correlation with statistical process controls. The LT02 is guaranteed to meet performance specifications over the  $-40^{\circ}$ C to  $85^{\circ}$ C operating temperature range.

Note 3: Bias current flows into the FB pin.

-40°C to 85°C operating temperature range are assured by design,

### **TYPICAL PERFORMANCE CHARACTERISTICS**



### PIN FUNCTIONS

**SW (Pin 1):** Switch Pin. This is the collector of the internal NPN power switch. Minimize the metal trace area connected to this pin to minimize EMI.

**GND (Pin 2):** Ground. Tie this pin directly to the local ground plane.

**FB (Pin 3):** Feedback Pin. Set the output voltage by selecting values for R1 and R2 (see Figure 1):

$$R1 = R2\left(\frac{V_{OUT}}{1.24} - 1\right)$$

**SHDN** (Pin 4): Shutdown Pin. Tie this pin to 0.9V or higher to enable the device. Tie below 0.25V to turn off the device.

 $V_{\text{IN}}$  (Pin 5): Input Supply Pin. Bypass this pin with a capacitor as close to the device as possible.

### **BLOCK DIAGRAM**



Figure 1. LT02 Block Diagram

# OPERATION

The LT02 uses a constant off-time control scheme to provide high efficiencies over a wide range of output current. Operation can be best understood by referring to the block diagram in Figure 1. Q1 and Q2 along with R3 and R4 form a bandgap reference used to regulate the output voltage. When the voltage at the FB pin is slightly above 1.23V, comparator A1 disables most of the internal circuitry. Output current is then provided by capacitor C2, which slowly discharges until the voltage at the FB pin drops below the lower hysteresis point of A1 (typical hysteresis at the FB pin is 8mV). A1 then enables the internal circuitry, turns on power switch Q3, and the current in inductor L1 begins ramping up. Once the switch current reaches 350mA, comparator A2 resets the oneshot, which turns off Q3 for 400ns. L1 then delivers current to the output through diode D1 as the inductor current ramps down. Q3 turns on again and the inductor

current ramps back up to 350mA, then A2 resets the oneshot, again allowing L1 to deliver current to the output. This switching action continues until the output voltage is charged up (until the FB pin reaches 1.23V), then A1 turns off the internal circuitry and the cycle repeats. The LTO2 contains additional circuitry to provide protection during start-up and under short-circuit conditions. When the FB pin voltage is less than approximately 600mV, the switch off-time is increased to 1.5 $\mu$ s and the current limit is reduced to around 250mA (70% of its normal value). This reduces the average inductor current and helps minimize the power dissipation in the LTO2 power switch and in the external inductor and diode.

# **APPLICATIONS INFORMATION**

#### Choosing an Inductor

Several recommended inductors that work well with the LT02 is listed in Table 1, although there

are many other manufacturers and devices that can be used. Consult each manufacturer for more detailed information and for their entire selection of related parts. Many different sizes and shapes are available. Use the equations and recommendations in the next few sections to find the correct inductance value for your design.

	Table 1.	Recommended	Inductor
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Value (µH)	MAX DCR ( $\Omega$ )	VENDOR			
4.7	0.26	Murata			
10	0.30	(814) 237-1431			
22	0.92	www.murata.com			
4.7	0.11	Sumida			
10	0.18	(847) 956-0666			
4.7	0.16	www.sumida.com			
10	0.20				
4.7	0.09	Coilcraft			
10	0.16	(847) 639-6400			
22	0.37	www.coilcraft.com			
	VALUE (µH)   4.7   10   22   4.7   10   4.7   10   4.7   10   4.7   10   4.7   22	VALUE (μH)MAX DCR (Ω)4.70.26100.30220.924.70.11100.184.70.16100.204.70.09100.16220.37			

#### Inductor Selection—Boost Regulator

The formula below calculates the appropriate inductor value to be used for a boost regulator using the LTO2. This value provides a good tradeoff in inductor size and system performance. Pick a standard inductor close to this value. A larger value can be used to slightly increase the available output current, but limit it to around twice the value calculated below, as too large of an inductance will increase the output voltage ripple without providing much additional output current. A smaller value can be used (especially for systems with output voltages greater than 12V) to give a smaller physical size. Inductance can be calculated as:

$$L = \frac{V_{OUT} - V_{IN(MIN)} + V_D}{I_{LIM}} t_{OFF}$$

where  $V_D = 0.4V$  (Schottky diode voltage),  $I_{LIM} = 350$ mA or 100mA, and  $t_{OFF} = 400$ ns; for designs with varying  $V_{IN}$  such as battery powered applications, use the minimum

 $V_{IN}$  value in the above equation. For most systems with output voltages below 7V, a 4.7µH inductor is the best choice, even though the equation above might specify a smaller value. This is due to the inductor current overshoot that occurs when very small inductor values are used (see Current Limit Overshoot section).

For higher output voltages, the formula above will give large inductance values. For a 2V to 20V converter (typical LCD Bias application), a  $21\mu$ H inductor is called for with the above equation, but a  $10\mu$ H inductor could be used without excessive reduction in maximum output current.

#### Inductor Selection—SEPIC Regulator

The formula below calculates the approximate inductor value to be used for a SEPIC regulator using the LT02. As for the boost inductor selection, a larger or smaller value can be used.

$$L = 2 \left( \frac{V_{OUT} + V_D}{I_{LIM}} \right) t_{OFF}$$

#### **Current Limit Overshoot**

For the constant off-time control scheme of the LT02, the power switch is turned off only after the 350mA (or 100mA) current limit is reached. There is a 100ns delay between the time when the current limit is reached and when the switch actually turns off. During this delay, the inductor current exceeds the current limit by a small amount. The peak inductor current can be calculated by:

$$I_{\text{PEAK}} = I_{\text{LIM}} + \left(\frac{V_{\text{IN(MAX)}} - V_{\text{SAT}}}{L}\right) 100 \text{ns}$$

Where  $V_{SAT} = 0.25V$  (switch saturation voltage). The current overshoot will be most evident for systems with high input voltages and for systems where smaller inductor values are used. This overshoot can be beneficial as it helps increase the amount of available output current for smaller inductor values. This will be the peak current seen by the inductor (and the diode) during normal operation. For designs using small inductance values (especially at

### **APPLICATIONS INFORMATION**

input voltages greater than 5V), the current limit overshoot can be quite high. Although it is internally current limited to 350mA, the power switch of the LT02 can handle larger currents without problem, but the overall efficiency will suffer. Best results will be obtained when  $I_{PEAK}$  is kept below 700mA for the LT02.

#### **Capacitor Selection**

Low ESR (Equivalent Series Resistance) capacitors should be used at the output to minimize the output ripple voltage. Multilayer ceramic capacitors are the best choice, as they have a very low ESR and are available in very small packages. Their small size makes them a good companion to the LT02's SOT-23 package. Solid tantalum capacitors (like the AVX TPS, Sprague 593D families) or OS-CON capacitors can be used, but they will occupy more board area than a ceramic and will have a higher ESR. Always use a capacitor with a sufficient voltage rating.

Ceramic capacitors also make a good choice for the input decoupling capacitor, which should be placed as close as possible to the LT02. A  $4.7\mu$  F input capacitor is sufficient for most applications. Table 2 shows a list of several capacitor manufacturers. Consult the manufacturers for more detailed information and for their entire selection of related parts.

#### **Diode Selection**

For most LT02 applications, the Motorora MBR0520 surface mount Schottky diode (0.5A, 20V) is an ideal choice. Schottky diodes, with their low forward voltage drop and fast switching speed, are the best match for the LT02. For higher output voltage applications the 30V MBR0530 can be used. Many different manufacturers make equivalent parts, but make sure that the component is rated to handle at least 0.35A.

#### Lowering Output Voltage Ripple

Using low ESR capacitors will help minimize the output ripple voltage, but proper selection of the inductor and the output capacitor also plays a big role. The LTO2 provides energy to the load in bursts by ramping up the inductor current, then delivering that current to the load. If too large of an inductor value or too small of a capacitor value is used, the output ripple voltage will increase because the capacitor will be slightly overcharged each burst cycle. To reduce the output ripple, increase the output capacitor value or add a 4.7pF feed-forward capacitor in the feedback network of the LTO2 (see the circuits in the Typical Applications section). Adding this small, inexpensive 4.7pF capacitor will greatly reduce the output voltage ripple.

CAPACITOR TYPE	VENDOR
Ceramic	Taiyo Yuden (408) 573-4150 www.t-yuden.com
Ceramic	AVX (803) 448-9411 www.avxcorp.com
Ceramic	Murata (714) 852-2001 www.murata.com

## TYPICAL APPLICATIONS

2-Cell to 3.3V Boost Converter



2-Cell to 3.3V Converter Efficiency



1-Cell Li-Ion to 3.3V SEPIC Converter



4-Cell to 5V SEPIC Converter



### TYPICAL APPLICATIONS



 $\pm 20V$  Dual Output Converter with Output Disconnect

# PACKAGE DESCRIPTION

S5 Package 5-Lead Plastic SOT-23



4		5	
2B			2A
A			
$\begin{array}{c c} B \\ \hline C \\ \hline 3 \end{array}$	DE	1	

### pad:

Pad	(X)	(Y)	Pad	(X)	(Y)
1	320.81	-288.62	А	-641.52	-141.60
2A	676.00	47.67	В	-641.52	-236.62
2B	-659.97	-33.53	С	-641.52	-335.74
3	-510.74	-320.92	D	-321.64	-351.91
4	-457.22	338.00	Е	-207.06	-351.91
5	284.00	375.57			

Padsize(1):80\*123.58

Padsize (A/B/C/D/E):60\*60-15\*15\*2

Padsize (2A):80\*127.28

Padsize (3/4/5):80\*80

Stepsize:1550\*980

Chipsize:1470\*890



# LT02 TestParameter

NO.	Symbol	Test Condition	LL	UL	UNIT
1	Icc1 3V	$V5 = 3V \qquad 2 \text{ Pin} \rightarrow \text{GND} \\ 5 \text{ Pin} \text{ TEST}$	-0.1	0.1	mA
2	Icc2 3V	$V5;V4 = 3V \qquad 2 \text{ Pin} \rightarrow \text{GND}$ 5 Pin TEST	0.2	2	mA
3	Icc3 10V	$V5; V4 = 10V \qquad 2 \text{ Pin} \rightarrow \text{GND}$ 5 Pin TEST	0.2	3	mA
4	Vout1 3V	V5;V4 = $3V$ 2 Pin $\rightarrow$ GNDS2 ON $25S,26F$ TEST	18	22	V
5	Icc4 5V	V5;V4 =8V2 Pin $\rightarrow$ GNDS1 ON5 Pin TEST	180	340	mA
6	Vout2 2V	V5;V4 = 2V2 Pin $\rightarrow$ GNDS2 ON25S,26F TEST	8	21	V
7	ΔVout 12V	$V5;V4 = 12V \qquad 2 \text{ Pin} \rightarrow \text{GND}$ S2 0N 25S,26F TEST No.7 - No.4	-0.2	+0.2	V
8	V3 3V	V5;V4 = $3V$ 2 Pin $\rightarrow$ GNDS2 ON $3S,4F$ TEST	1.205	1.26	V

### LT02 TEST Circuits:

