## APPENDIX

This worksheet calculates the relevant currents and voltages as well as losses in PFC boost topologies. Constant output voltage and continuos conduction mode (CCM) and critical conduction mode (CRM) operation is assumed.

Constants:

$$p := 10^{-12}$$
 nano  $:= 10^{-9}$   $u := 10^{-6}$   $m := 10^{-3}$   $k := 10^{3}$  MEG  $:= 10^{6}$   $j := \sqrt{-1}$ 

 $i:=0..\,200 \qquad y:=1..\,5 \qquad x:=0..\,4 \qquad Fs:=100\,k$ 

Vout := 385 VAC\_min := 85 VAC := 120

Pout := 200 
$$\eta$$
 := 0.95 Pin :=  $\frac{Pout}{\eta}$  Iload :=  $\frac{Pout}{Vout}$ 

Pin\_var allows input power to be varied over a range to compare losses.

$$Pin_var_x := Pin(x + 1)$$

$$j := 0..5$$

$$VAC2 := \begin{pmatrix} 85 \\ 120 \\ 132 \\ 215 \\ 240 \\ 265 \end{pmatrix}$$

$$Vin_{i} := \sqrt{2} \cdot VAC \cdot \left| sin \left( i \cdot \frac{\pi}{200} \right) \right|$$

Boost converter duty cycle

$$D_i := \frac{Vout - Vin_i}{Vout}$$

Average boost inductor current in CCM.

$$IAC_i := \frac{Vin_i \cdot Pin}{VAC^2}$$

## A. Calculate currents in the CCM boost RMS switch current

Iq\_rms\_ccm := 
$$\frac{\text{Pin}}{\text{VAC}} \cdot \sqrt{1 - \frac{8}{3 \cdot \pi} \cdot \frac{\sqrt{2} \cdot \text{VAC}}{\text{Vout}}}$$

 $Iq\_rms\_ccm = 1.388$ 

RMS switch current varying as a function of input power.

Iq\_rms\_ccm\_var\_x := 
$$\frac{\text{Pin}_var_x}{\text{VAC}} \cdot \sqrt{1 - \frac{8}{3 \cdot \pi} \cdot \frac{\sqrt{2} \cdot \text{VAC}}{\text{Vout}}}$$

Peak inductor current

IL\_pk\_ccm := 
$$\frac{\sqrt{2} \cdot \text{Pin}}{\text{VAC}} + 0.1 \cdot \frac{\sqrt{2} \cdot \text{Pin}}{\text{VAC}}$$

Let delta i in CCM inductor be 20% of peak current at low line.

IL\_ripple := 
$$0.2 \cdot \frac{\sqrt{2} \cdot \text{Pin}}{\text{VAC}}$$

Pk current is Iin avg + 1/2 delta i

Peak inductor current as a function of input power

IL\_pk\_ccm\_var<sub>x</sub> := 
$$\frac{\sqrt{2} \cdot \text{Pin}_var_x}{\text{VAC}} + 0.1 \cdot \frac{\sqrt{2} \cdot \text{Pin}_var_x}{\text{VAC}}$$

Inductor current valley

IL\_valley\_ccm := 
$$\frac{\sqrt{2} \cdot \text{Pin}}{\text{VAC}} - \left(0.1 \cdot \frac{\sqrt{2} \cdot \text{Pin}}{\text{VAC}}\right)$$

$$IL_valley_ccm = 2.233$$

IL\_valley\_ccm\_var<sub>x</sub> := 
$$\frac{\sqrt{2} \cdot \text{Pin}_v \text{var}_x}{\text{VAC}} - \left(0.1 \cdot \frac{\sqrt{2} \cdot \text{Pin}_v \text{var}_x}{\text{VAC}}\right)$$

Peak diode current is equal to the peak inductor current.

Idiode\_pk\_ccm := IL\_pk\_ccm

## B. Calculate currents in the CRM boost converter:

IL\_pk\_crm := 
$$2\sqrt{2} \cdot \frac{P_{III}}{VAC}$$
  
IL\_pk\_crm = 4.962

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Peak current in CRM is twice the CCM current, neglecting the ripple current for CCM.

IL\_pk\_crm\_var<sub>x</sub> := 
$$2\sqrt{2} \cdot \frac{\text{Pin}_var_x}{\text{VAC}}$$
  
IL\_pk\_crm\_var<sub>x</sub> :=  $2\sqrt{2} \cdot \frac{\text{Pin}_var_x}{\text{VAC}}$   
Iq\_rms\_crm :=  $\sqrt{\frac{1}{6} - 4 \cdot \sqrt{2} \frac{\text{VAC}}{9 \cdot \pi \cdot \text{Vout}}} \cdot \text{IL}_p\text{k}_c\text{crm}$   
Iq\_rms\_crm = 1.603

Iq\_rms\_crm\_var<sub>x</sub> := 
$$\sqrt{\frac{1}{6} - 4 \cdot \sqrt{2} \frac{\text{VAC}}{9 \cdot \pi \cdot \text{Vout}} \cdot \text{IL}_p\text{k}_c\text{crm}_v\text{ar}_x}$$

Idiode\_pk\_crm := IL\_pk\_crm

## C. Calculate loss components.

Calculate diode related losses:

Assume di/dt at turn off is 100A/us.

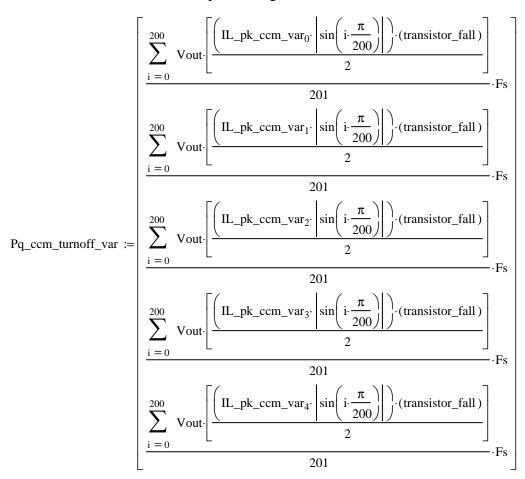
For the purpose of calculation use the 8ETH06 IR diode as reference. Also assume IRF840 for MOSFET

trr := 50 nano Qrr := 120 nano Irrm := 4.8 didf := 
$$100\frac{1}{u}$$
 Rdson := 0.85  
transistor\_rise := 75 nano  
transistor\_fall := 75 nano  
Irrm\_pfc<sub>i</sub> := Irrm  $\left| sin \left( i \cdot \frac{\pi}{200} \right) \right|$ 

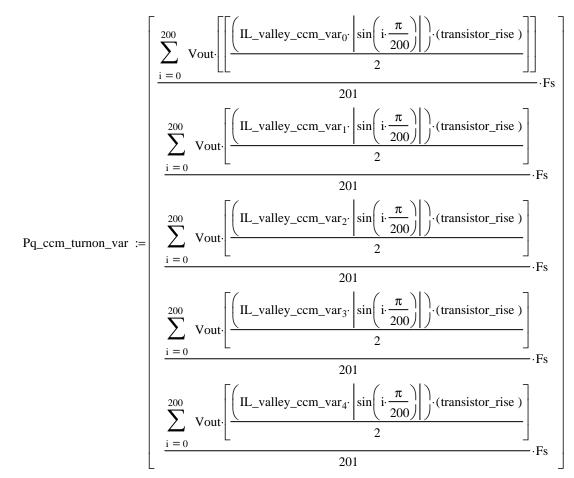
Loss in MOSFET due to reverse recovery current from boost diode. Only valid for CCM operation.

$$\Pr_{r=ccm\_var} := \begin{bmatrix} \sum_{i=0}^{200} \operatorname{Vout}\left[\left(\frac{\operatorname{Irm\_pfc_i}}{2} \cdot \frac{\operatorname{Irm\_pfc_i}}{\operatorname{didf}}\right) + \frac{\operatorname{Irm\_pfc_i}}{4} \cdot \left(\operatorname{trr} - \frac{\operatorname{Irm\_pfc_i}}{\operatorname{didf}}\right)\right] \\ \xrightarrow{201} \cdot \operatorname{Fs} \\ \frac{200}{201} \operatorname{Vout}\left[\left(\frac{1.5\operatorname{Irm\_pfc_i}}{2} \cdot \frac{\operatorname{Irm\_pfc_i}}{\operatorname{didf}}\right) + \frac{(1.5\operatorname{Irm\_pfc_i})}{4} \cdot \left(\operatorname{trr} - \frac{\operatorname{Irm\_pfc_i}}{\operatorname{didf}}\right)\right] \\ \xrightarrow{201} \cdot \operatorname{Fs} \\ \frac{200}{201} \operatorname{Vout}\left[\left(\frac{(2\operatorname{Irrm\_pfc_i})}{2} \cdot \frac{\operatorname{Irrm\_pfc_i}}{\operatorname{didf}}\right] + \frac{(2\operatorname{Irrm\_pfc_i})}{4} \cdot \left(\operatorname{trr} - \frac{\operatorname{Irrm\_pfc_i}}{\operatorname{didf}}\right)\right] \\ \xrightarrow{1=0} \cdot \operatorname{Fs} \\ \frac{200}{201} \operatorname{Vout}\left[\left(\frac{(2.5\operatorname{Irrm\_pfc_i})}{2} \cdot \frac{\operatorname{Irrm\_pfc_i}}{\operatorname{didf}}\right] + \frac{2.5\operatorname{Irrm\_pfc_i}}{4} \cdot \left(\operatorname{trr} - \frac{\operatorname{Irrm\_pfc_i}}{\operatorname{didf}}\right)\right] \\ \xrightarrow{1=0} \cdot \operatorname{Fs} \\ \frac{200}{201} \operatorname{Vout}\left[\left(\frac{(3\operatorname{Irrm\_pfc_i})}{2} \cdot \frac{\operatorname{Irrm\_pfc_i}}{\operatorname{didf}}\right] + \frac{(3\operatorname{Irrm\_pfc_i})}{4} \cdot \left(\operatorname{trr} - \frac{\operatorname{Irrm\_pfc_i}}{\operatorname{didf}}\right)\right] \\ \xrightarrow{1=0} \cdot \operatorname{Fs} \\ \frac{200}{201} \operatorname{Vout}\left[\left(\frac{(3\operatorname{Irrm\_pfc_i})}{2} \cdot \frac{\operatorname{Irrm\_pfc_i}}{\operatorname{didf}}\right) + \frac{(3\operatorname{Irrm\_pfc_i})}{4} \cdot \left(\operatorname{trr} - \frac{\operatorname{Irrm\_pfc_i}}{\operatorname{didf}}\right)\right] \\ \xrightarrow{1=0} \cdot \operatorname{Fs} \\ \frac{200}{201} \operatorname{Vout}\left[\left(\frac{(3\operatorname{Irrm\_pfc_i})}{2} \cdot \frac{\operatorname{Irrm\_pfc_i}}{\operatorname{didf}}\right) + \frac{(3\operatorname{Irrm\_pfc_i})}{4} \cdot \left(\operatorname{trr} - \frac{\operatorname{Irrm\_pfc_i}}{\operatorname{didf}}\right)\right] \\ \xrightarrow{1=0} \cdot \operatorname{Fs} \\ \frac{201}{201} \operatorname{Vout}\left[\left(\frac{(3\operatorname{Irrm\_pfc_i})}{2} \cdot \frac{\operatorname{Irrm\_pfc_i}}{\operatorname{didf}}\right) + \frac{(3\operatorname{Irrm\_pfc_i})}{4} \cdot \left(\operatorname{trr} - \frac{\operatorname{Irrm\_pfc_i}}{\operatorname{didf}}\right)\right] \\ \xrightarrow{1=0} \cdot \operatorname{Fs} \\ \frac{201}{201} \operatorname{Vout}\left[\left(\frac{(3\operatorname{Irrm\_pfc_i})}{2} \cdot \frac{\operatorname{Irrm\_pfc_i}}{\operatorname{didf}}\right) + \frac{(3\operatorname{Irrm\_pfc_i})}{4} \cdot \left(\operatorname{trr} - \frac{\operatorname{Irrm\_pfc_i}}{\operatorname{didf}}\right)\right] \\ \xrightarrow{1=0} \cdot \operatorname{Fs} \\ \frac{201}{201} \operatorname{Vout}\left[\left(\frac{(3\operatorname{Irrm\_pfc_i})}{2} \cdot \frac{\operatorname{Irrm\_pfc_i}}{\operatorname{didf}}\right) + \frac{(3\operatorname{Irrm\_pfc_i})}{4} \cdot \left(\operatorname{trr} - \frac{\operatorname{Irrm\_pfc_i}}{\operatorname{didf}}\right)\right] } \\ \xrightarrow{1=0} \cdot \operatorname{Fs} \\ \frac{201}{201} \operatorname{Vout}\left[\left(\frac{(3\operatorname{Irrm\_pfc_i})}{2} \cdot \frac{\operatorname{Irrm\_pfc_i}}{\operatorname{didf}}\right) + \frac{\operatorname{Irrm\_pfc_i}}{4} \cdot \left(\operatorname{Irr=\operatorname{Irrm\_pfc_i}}\right) + \operatorname{Irrm\_pfc_i}\right) } \\ \frac{1}{201} \operatorname{Vout}\left[\left(\frac{(3\operatorname{Irrm\_pfc_i})}{2} \cdot \frac{\operatorname{Irrm\_pfc_i}}{2} \cdot \frac{\operatorname{Irrm\_p$$

Losses in MOSFET due to turn-off overlap of voltage and current:



Losses in MOSFET due to turn-on overlap of voltage and current:



Conduction losses in the MOSFET:

$$Pq\_ccm\_rms\_var := \begin{bmatrix} (Iq\_rms\_ccm\_var_0)^2 \cdot Rdson \\ (Iq\_rms\_ccm\_var_1)^2 \cdot Rdson \\ (Iq\_rms\_ccm\_var_2)^2 \cdot Rdson \\ (Iq\_rms\_ccm\_var_3)^2 \cdot Rdson \\ (Iq\_rms\_ccm\_var_4)^2 \cdot Rdson \end{bmatrix}$$

Diode conduction losses:

$$Pdiode\_ccm\_var := \begin{bmatrix} \sum_{i=0}^{200} \left[ \left( IL\_pk\_ccm\_var_{0} \cdot \left| \sin\left(i \cdot \frac{\pi}{200}\right) \right| \right) \cdot VFF(1 - D_{i}) \right] \\ \frac{\sum_{i=0}^{200} \left[ \left( IL\_pk\_ccm\_var_{1} \cdot \left| \sin\left(i \cdot \frac{\pi}{200}\right) \right| \right) \cdot VFF(1 - D_{i}) \right] \\ 201 \\ 201 \\ 201 \\ 201 \\ 201 \\ \frac{\sum_{i=0}^{200} \left[ \left( IL\_pk\_ccm\_var_{2} \cdot \left| \sin\left(i \cdot \frac{\pi}{200}\right) \right| \right) \cdot VFF(1 - D_{i}) \right] \\ 201 \\ \frac{\sum_{i=0}^{200} \left[ \left( IL\_pk\_ccm\_var_{3} \cdot \left| \sin\left(i \cdot \frac{\pi}{200}\right) \right| \right) \cdot VFF(1 - D_{i}) \right] \\ 201 \\ 201 \\ 201 \\ 201 \\ 201 \\ 201 \\ 201 \end{bmatrix}$$

Diode bridge conduction losses:

$$Pdiodebridge\_ccm\_var := \begin{bmatrix} \sum_{i=0}^{200} \left[ \left( IL\_pk\_ccm\_var_{0} \cdot \left| sin\left(i \cdot \frac{\pi}{200}\right) \right| \right) \cdot VFF(2) \right] \\ \frac{\sum_{i=0}^{200} \left[ \left( IL\_pk\_ccm\_var_{1} \cdot \left| sin\left(i \cdot \frac{\pi}{200}\right) \right| \right) \cdot VFF(2) \right] \\ 201 \\ \frac{\sum_{i=0}^{200} \left[ \left( IL\_pk\_ccm\_var_{2} \cdot \left| sin\left(i \cdot \frac{\pi}{200}\right) \right| \right) \cdot VFF(2) \right] \\ 201 \\ \frac{\sum_{i=0}^{200} \left[ \left( IL\_pk\_ccm\_var_{3} \cdot \left| sin\left(i \cdot \frac{\pi}{200}\right) \right| \right) \cdot VFF(2) \right] \\ 201 \\ \frac{\sum_{i=0}^{200} \left[ \left( IL\_pk\_ccm\_var_{4} \cdot \left| sin\left(i \cdot \frac{\pi}{200}\right) \right| \right) \cdot VFF(2) \right] \\ 201 \\ \frac{201}{201} \end{bmatrix}$$

 $P1 := Prr\_ccm\_var + Pq\_ccm\_turnoff\_var + Pq\_ccm\_turnon\_var$ 

P2 := Pq\_ccm\_rms\_var + Pdiode\_ccm\_var + Pdiodebridge\_ccm\_var

$$P_{loss\_semi\_ccm\_var} := P1 + P2$$

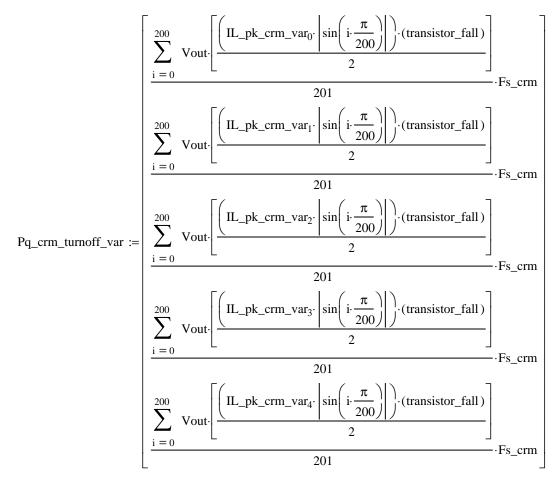
$$P\_loss\_semi\_ccm\_var = \begin{pmatrix} 11.176 \\ 24.342 \\ 40.784 \\ 60.5 \\ 83.491 \end{pmatrix}$$

Calculate losses in the CRM boost.

Let the average Fs for CRM operation be 80kHz.

 $Fs\_crm := 80 \cdot k$ 

Losses in MOSFET due to turn-off overlap of voltage and current:



MOSFET conduction losses:

$$Pq\_crm\_rms\_var := \begin{bmatrix} (Iq\_rms\_crm\_var_0)^2 \cdot Rdson \\ (Iq\_rms\_crm\_var_1)^2 \cdot Rdson \\ (Iq\_rms\_crm\_var_2)^2 \cdot Rdson \\ (Iq\_rms\_crm\_var_3)^2 \cdot Rdson \\ (Iq\_rms\_crm\_var_4)^2 \cdot Rdson \end{bmatrix}$$

Diode conduction losses:

$$Pdiode\_crm\_var := \begin{bmatrix} \sum_{i=0}^{200} \left[ \left( IL\_pk\_crm\_var_{0} \cdot \left| \sin\left(i \cdot \frac{\pi}{200}\right) \right| \right) \cdot VFF(1 - D_{i}) \right] \\ \hline 201 \\ \hline 201$$

Bridge diode conduction losses:

$$Pdiodebridge\_crm\_var := \begin{bmatrix} \sum_{i=0}^{200} \left[ \left( IL\_pk\_crm\_var_{0} \cdot \left| sin\left(i \cdot \frac{\pi}{200}\right) \right| \right) \cdot VFF(2) \right] \\ 201 \\ \sum_{i=0}^{200} \left[ \left( IL\_pk\_crm\_var_{1} \cdot \left| sin\left(i \cdot \frac{\pi}{200}\right) \right| \right) \cdot VFF(2) \right] \\ 201 \\ 201 \\ 201 \\ 201 \\ \sum_{i=0}^{200} \left[ \left( IL\_pk\_crm\_var_{2} \cdot \left| sin\left(i \cdot \frac{\pi}{200}\right) \right| \right) \cdot VFF(2) \right] \\ 201 \\ 201 \\ 201 \\ 201 \\ 201 \\ 201 \\ 201 \\ 201 \\ 201 \end{bmatrix}$$

Total semiconductor losses in CRM:

P3 := Pq\_crm\_turnoff\_var + Pq\_crm\_rms\_var

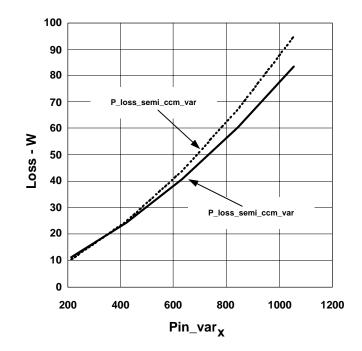
P4 := Pdiode\_crm\_var + Pdiodebridge\_crm\_var

P\_loss\_semi\_crm\_var := P3 + P4

$$P\_loss\_semi\_crm\_var = \begin{pmatrix} 10.238 \\ 24.843 \\ 43.814 \\ 67.15 \\ 94.853 \end{pmatrix} P\_loss\_semi\_ccm\_var = \begin{pmatrix} 11.176 \\ 24.342 \\ 40.784 \\ 60.5 \\ 83.491 \end{pmatrix}$$

for  $Fs\_crm = 80kHz$ 

This plot compares the semiconductor losses for CCM vs. CRM as a function of input power.



Efficiency comparison of CCM vs. CRM as a function of input power.

