## FEATURES

- 2A Output Current
- Up to 92\% Efficiency
- 4.75 V to 23 V Input Range
-20رA Shutdown Supply Current
$\bullet 380 \mathrm{kHz}$ Switching Frequency
- Adjustable Output Voltage from 1.22 V to $0.85 \cdot \mathrm{~V}_{\mathrm{IN}}$
-Cycle-by-Cycle Current Limit Protection
- Thermal Shutdown Protection
- Frequency Fold Back at Short Circuit
-Stability with Wide Range of Capacitors,
- MSOP-10 Package


## APPLICATIONS

- TFT LCD Monitors
- Portable DVDs
- Car-Powered or Battery-Powered Equipments
- Set-Top Boxes
-Telecom Power Supplies
- DSL and Cable Modems and Routers
-Termination Supplies


## GENERAL DESCRIPTION

The BM1411 is a current-mode step-down DC-DC converter that generates up to $2 A$ output current at 380 kHz switching frequency. The device utilizes advanced BCD process for operation with input voltage up to 23 V consuming only $20 \mu \mathrm{~A}$ in shutdown mode, the BM1411 is highly efficient with peak efficiency at $92 \%$ when in operation.

Protection features include cycle-by-cycle current limit, thermal shutdown, and frequency fold back at short circuit.

The BM1411 is available in msop-10 package and requires very few external devices for operation.


Figure 1. Typical Application Circuit

## ORDERING INFORMATION

| PART NUMBER | TEMPERATURE RANGE | PACKAGE | PINS |
| :--- | :--- | :--- | :--- |
| BM1411 | $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$ | MSOP-10 | $7,3 \mathrm{~N} / \mathrm{C}$ |

## PIN CONFIGURATION



| PIN No. | PIN NAME | PIN DESCRIPTION |
| :---: | :---: | :--- |
| 1 | NC | No Connected |
| 2 | BS | Bootstrap. This pin acts as the positive rail for the high-side switch's gate driver. Connect a 10nF between this <br> pin and SW. |
| 3 | NC | No Connected |
| 4 | IN | Input Supply. Bypass this pin to G with a low ESR capacitor. See Input Capacitor in Application Information |
| section. |  |  |

## ABSOLUTE MAXIMUM RATINGS

(Note: Do not exceed these limits to prevent damage to the device. Exposure to absolute maximum rating conditions for long periods may affect device reliability.)

| PARAMETER | VALUE | UNIT |
| :--- | :---: | :--- |
| IN Supply Voltage | -0.3 to 23 | V |
| SW Voltage | -1 to VIN +1 | V |
| BS Voltage | VSW -0.3 to VSW +6 | V |
| EN, FB, COMP Voltage | -0.3 to 6 | V |
| Continuous SW Current | Internally limited | A |
| Junction to Ambient Thermal Resistance $\left(\theta_{\text {JA }}\right)$ | 105 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| Operating Junction Temperature | -40 to 150 | ${ }^{\circ} \mathrm{C}$ |
| Storage Temperature | -55 to 150 | ${ }^{\circ} \mathrm{C}$ |
| Lead Temperature (Soldering, 10 sec$)$ | 300 | ${ }^{\circ} \mathrm{C}$ |

## ELECTRICAL CHARCXERISTICS

(VIN $=12 \mathrm{~V}, \mathrm{TJ}=25^{\circ} \mathrm{C}$ unless otherwise specified)

| PARAMETER | SYMBOL | TEST CONDITIONS | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Feedback Voltage | VFB | $4.75 \mathrm{~V} \leq \mathrm{VIN} \leq 18 \mathrm{~V}, \mathrm{VCOMP}=1.5 \mathrm{~V}$ | 1.184 | 1.22 | 1.258 | V |
| High-Side Switch On Resistance | RONH |  |  | 0.22 |  | $\Omega$ |
| Low-Side Switch On Resistance | RONL |  |  | 4.7 |  | $\Omega$ |
| SW Leakage |  | VEN $=0$ |  | 1 |  | $\mu \mathrm{A}$ |
| Current Limit | ILIM |  | 2.6 | 3.3 |  | A |
| COMP to Current Limit Transconductance | GCOMP |  |  | 1.8 |  | A/V |
| Error Amplifier Transconductance | GEA | $\Delta I C O M P= \pm 10 \mu \mathrm{~A}$ |  | 550 |  | $\mu \mathrm{A} / \mathrm{V}$ |
| Error Amplifier DC Gain | AVEA |  |  | 3200 |  | V/V |
| Switching Frequency | fsw |  | 330 | 380 | 430 | kHz |
| Short Circuit Switching Frequency |  | VFB $=0$ |  | 50 |  | kHz |
| Maximum Duty Cycle | DMAX | $\mathrm{VFB}=1.1 \mathrm{~V}$ |  | 90 |  | \% |
| Minimum Duty Cycle |  | $\mathrm{VFB}=1.4 \mathrm{~V}$ |  |  |  | \% |
| Enable Threshold Voltage |  | Hysteresis $=0.1 \mathrm{~V}$ | 2.0 | 2.2 |  | v |
| Enable Pull Up Current |  | Pin pulled up to 4.5 V typically when left unconnected |  | 2.5 |  | $\mu \mathrm{A}$ |
| Supply Current in Shutdown |  | VEN $=0$ |  | 20 |  | $\mu \mathrm{A}$ |
| IC Supply Current in Operation |  | $\mathrm{VEN}=3 \mathrm{~V}, \mathrm{VFB}=1.4 \mathrm{~V}$ |  | 1.0 | 1.5 | mA |
| Thermal Shutdown Temperature |  | Hysteresis $=10^{\circ} \mathrm{C}$ |  | 168 |  | ${ }^{\circ} \mathrm{C}$ |



Figure 2 . Functional Block Diagram

## FUNCTIONAL DESCRIPTION

As seen in Figure 2, Functional Block Diagram, the BM1411 is a current mode pulse width modulation (PWM) converter. The converter operates as follows:

A switching cycle starts when the rising edge of the Oscillator clock output causes the High-Side Power Switch to turn on and the Low-Side Power Switch to turn off. With the SW side of the inductor now connected to IN , the inductor current ramps up to store energy in the its magnetic field. The inductor current level is measured by the Current Sense Amplifier and added to the Oscillator ramp signal. If the resulting summation is higher than the COMP voltage, the output of the PWM Comparator goes high. When this happens or when Oscillator clock output goes low, the High-Side Power Switch turns off and the Low-Side Power Switch turns on. At this point, the SW side of the inductor swings to a diode voltage below ground, causing the inductor current to decrease and magnetic energy to be transferred to output. This state continues until the cycle starts again.

The High-Side Power Switch is driven by logic using BS bootstrap pin as the positive rail. This pin is charged to $\mathrm{Vsw}+6 \mathrm{~V}$ when the Low-Side Power Switch turns on.

The COMP voltage is the integration of the error between FB input and the internal 1.22 V reference. If FB is lower than the reference voltage, COMP tends to go higher to increase current to the output. Current limit happens when COMP reaches its maximum clam value of 2.55 V .

The Oscillator normally switches at 380 kHz . However, if FB voltage is less than 0.7 V , then the switching frequency decreases until it reaches a minimum of 50 kHz at $\mathrm{V}_{\mathrm{FB}}=0.5 \mathrm{~V}$.

## SHUTDOWN CONTROL

The BM1411 has an enable input EN for turning the IC on or off. When EN is less than 1.8 V , the IC is in $20 \mu \mathrm{~A}$ low current shutdown mode and output is discharged through the Low-Side Power Switch. When EN is higher than 2.0 V , the IC is in normal operation mode. EN is internally pulled up with a $2.5 \mu \mathrm{~A}$ current source and can be left unconnected for always-on operation. Note that EN is a low voltage input with a maximum voltage of 6 V ; it should never be directly connected to IN .

## THERMAL SHUTDOWN

The BM1411 automatically turns off when its junction temperature exceeds $168^{\circ} \mathrm{C}$.

## APPLICATION INFORMATION

OUTPUT VOLTAGE SETTING


Figure 3. Output Voltage Setting
Figure 3 shows the connections for setting the output voltage. Select the proper ratio of the two feedback resistors R $\mathrm{R}_{\mathrm{FB} 1}$ and $\mathrm{R}_{\text {FB2 }}$ based on the output voltage. Typically, use $\mathrm{R}_{\mathrm{FB} 2} \approx 10 \mathrm{k} \Omega$ and determine R Rb1 from the output voltage:

$$
\begin{equation*}
R_{F B 1}=R_{F B 2}\left(\frac{V_{O U T}}{1.22 V}-1\right) \tag{1}
\end{equation*}
$$

## INDUCTOR SELECTION

The inductor maintains a continuous current to the output load. This inductor current has a ripple that is dependent on the inductance value: higher inductance reduces the peak-to-peak ripple current. The trade off for high inductance value is the increase in inductor core size and series resistance, and the reduction in current handling capability. In general, select an inductance value $L$ based on ripple current requirement:

$$
\begin{equation*}
L=\frac{V_{\text {OUT }} \bullet\left(V_{\text {IN }}-V_{\text {OUT }}\right)}{V_{\text {IN }} f_{\text {SW }} I_{\text {OUTMAX }} K_{\text {RIPPLE }}} \tag{2}
\end{equation*}
$$

where Vis is the input voltage, Vout is the output voltage, fsw is the switching frequency, loutmax is the maximum output current, and Kripple is the ripple factor. Typically, choose KrIpple $=30 \%$ to correspond to the peak-to-peak ripple current being $30 \%$ of the maximum output current.

With this inductor value (Table 1), the peak inductor current is lout • $(1+$ KRIPPLE $/ 2)$. Make sure that this peak inductor current is less that the 3A current limit. Finally, select the inductor core size so that it does not saturate at 3 A .

Table 1. Typical Inductor Values

| Vout | 1.5 v | 1.8 v | 2.5 v | 3.3 v | 5 v | 12 v |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $\mathrm{L}(\mu \mathrm{H})$ | 6.8 | 6.8 | 10 | 15 | 22 | 47 |

## INPUT CAPACITOR

The input capacitor needs to be carefully selected to maintain sufficiently low ripple at the supply input of the converter. A low ESR capacitor is highly recommended. Since large current flows in and out of this capacitor during switching, its ESR also affects efficiency.

The input capacitance needs to be higher than $10 \mu \mathrm{~F}$. The best choice is the ceramic type; however, low ESR tantalum or electrolytic types may also be used provided that the RMS ripple current rating is higher than $50 \%$ of the output current. The input capacitor should be placed close to the IN and G pins of the IC, with shortest traces possible. In the case of tantalum or electrolytic types, they can be further away if a small parallel $0.1 \mu \mathrm{~F}$ ceramic capacitor is placed right next to the IC.

## OUTPUT CAPACITOR

The output capacitor also needs to have low ESR to keep low output voltage ripple. The output ripple voltage is:
$V_{\text {RIPPLE }}=$ IOUTMAX KRIPPLE $R E S R$

$$
\begin{equation*}
+\frac{V_{I N}}{28 \square f_{s w}{ }^{2} L C_{\text {OUT }}} \tag{3}
\end{equation*}
$$

where loutmax is the maximum output current, Kripple is the ripple factor, RESR is the ESR resistance of the output capacitor, fsw is the switching frequency, $L$ in the inductor value, Cout is the output capacitance. In the case of ceramic output capacitors, Resp is very small and does not contribute to the ripple. Therefore, a lower capacitance value can be used for ceramic type. In the case of tantalum or electrolytic type, the ripple is dominated by Resr multiplied by the ripple current. In that case, the output capacitor is chosen to have sufficiently low ESR.

For ceramic output type, typically choose a capacitance of about $22 \mu \mathrm{~F}$. For tantalum or electrolytic type, choose a capacitor with less than $50 \mathrm{~m} \Omega$ ESR.

## RECTIFIER DIODE

Use a Schottky diode as the rectifier to conduct current when the High-Side Power Switch is off. The Schottky diode must have current rating higher than the maximum output current and the reverse voltage rating higher than the maximum input voltage.

## STABILTY COMPENSATION



Ccomp2 in needed only for high ESR output capacitor
Figure 4. stability Compensation

The feedback system of the IC is stabilized by the components at COMP pin, as shown in Figure 4. The DC loop gain of the system is determined by the following equation:

$$
\begin{equation*}
A v D C=\frac{1.3 \mathrm{~V}}{\text { IoUT }} A_{V E A} \text { Gcomp } \tag{4}
\end{equation*}
$$

The dominant pole P1 is due to Cсомр:

$$
\begin{equation*}
f_{P 1}=\frac{G_{E A}}{2 \pi \text { AvBA } \text { СсомP }} \tag{5}
\end{equation*}
$$

The second pole P2 is the output pole:

$$
\begin{equation*}
C_{\text {COMP2 }}=\frac{\text { Cout }_{\text {ESRCOUT }}}{R_{\text {COMP }}} \tag{6}
\end{equation*}
$$

The first zero Z 1 is due to Rcomp and Ccomp:

$$
\begin{equation*}
f_{z 1}=\frac{1}{2 \pi R \operatorname{comp}\llcorner\text { Ссомр }} \tag{7}
\end{equation*}
$$

And finally, the third pole is due to Rсомp and Ccomp2 (if Ccomp2 is used):

$$
\begin{equation*}
f_{P 3}=\frac{1}{2 \pi R_{\text {сомР }} \sqsubset C_{\text {COMP } 2}} \tag{8}
\end{equation*}
$$

Follow the following steps to compensate the IC:

STEP 1. Set the cross over frequency at $1 / 10$ of the switching frequency via Rcomp:

$$
\begin{align*}
R_{\text {COMP }} & =\frac{2 \pi V_{\text {Out }} \text { Cout } f \text { sw }}{10 G_{\text {EA }} G_{\text {comp }} \square .3 V} \\
& =1.7 \square 10^{8} \text { оut } \operatorname{Cout}(\Omega) \tag{9}
\end{align*}
$$

but limit Rcomp to $15 \mathrm{k} \Omega$ maximum.
STEP 2. Set the zero $f_{z 1}$ at $1 / 4$ of the cross over frequency. If Rcomp is less than $15 \mathrm{k} \Omega$, the equation for Ccomp is:

$$
\begin{equation*}
\mathrm{C}_{\mathrm{COMP}}=\frac{1.8 \square 10^{-5}}{R_{\mathrm{COMP}}} \quad(F) \tag{10}
\end{equation*}
$$

If Rcomp is limited to $15 \mathrm{k} \Omega$, then the actual cross over frequency is 3.4 / (VOUTCOUT). Therefore:

$$
\begin{equation*}
C_{\text {COMP }}=1.2 \times 10^{-5} V_{\text {OUT }} C_{\text {OUT }} \tag{F}
\end{equation*}
$$

STEP 3. If the output capacitor's ESR is high enough to cause a zero at lower than 4 times the cross over frequency, an additional compensation capacitor Ссомp2 is required. The condition for using Ccompz is:
$R$ EsRCOUT

$$
\geq \operatorname{Min}\left(\frac{1.1 \times 10^{-6}}{C_{O U T}} 0.012 \times V_{\text {OUT }}\right)
$$

And the proper value for Ccomp2 is:
$C_{\text {COMP } 2}=\frac{\text { Cout } R_{\text {ESRCOUT }}}{R_{\text {COMP }}}$

Though Ccomp2 is unnecessary when the output capacitor has sufficiently low ESR, a small value Ccomp2 such as 100pF may improve stability against PCB layout parasitic effects.

Table 2 shows some calculated results based on the compensation method above.

Table 2. Typical Compensation for Different Output Voltages and Output Capacitors

| VOUT | COUT | RCOMP | CCOMP | CCOMP2 |
| :--- | :--- | :--- | :--- | :--- |
| 2.5 V | $22 \mu \mathrm{~F}$ Ceramic | $8.2 \mathrm{k} \Omega$ | 2.2 nF | None |
| 3.3 V | $22 \mu \mathrm{~F}$ Ceramic | $12 \mathrm{k} \Omega$ | 1.5 nF | None |
| 5 V | $22 \mu \mathrm{~F}$ Ceramic | $15 \mathrm{k} \Omega$ | 1.5 nF | None |
| 12 V | $22 \mu \mathrm{~F}$ Ceramic | $15 \mathrm{k} \Omega$ | 3.3 nF | None |
| 2.5 V | $22 \mu \mathrm{~F} \mathrm{SP} \mathrm{Cap}$ | $15 \mathrm{k} \Omega$ | 1.5 nF | None |
| 3.3 V | $22 \mu \mathrm{~F} \mathrm{SP} \mathrm{Cap}$ | $15 \mathrm{k} \Omega$ | 1.8 nF | None |
| 5 V | $22 \mu \mathrm{~F} \mathrm{SP} \mathrm{Cap}$ | $15 \mathrm{k} \Omega$ | 2.7 nF | None |
| 12 V | $22 \mu \mathrm{~F} \mathrm{SP} \mathrm{Cap}$ | $15 \mathrm{k} \Omega$ | 6.8 nF | None |
| 2.5 V | $470 \mu \mathrm{~F} / 6.3 \mathrm{~V} / 30 \mathrm{~m} \Omega$ | $15 \mathrm{k} \Omega$ | 15 nF | 1 nF |
| 3.3 V | $470 \mu \mathrm{~F} / 6.3 \mathrm{~V} / 30 \mathrm{~m} \Omega$ | $15 \mathrm{k} \Omega$ | 22 nF | 1 nF |
| 5 V | $470 \mu \mathrm{~F} / 6.3 \mathrm{~V} / 30 \mathrm{~m} \Omega$ | $15 \mathrm{k} \Omega$ | 27 nF | None |
| 12 V | $220 \mu \mathrm{~F} / 25 \mathrm{~V} / 30 \mathrm{~m} \Omega$ | $15 \mathrm{k} \Omega$ | 33 nF | None |

## Typical Application 3.3V/2A Output



## Typical Application 5.0V/2A Output



Figure5B: BM1411 5V/2A Output Application

Typical Application 2.5V/2A Output


Figure5C: BM1411 2.5V/2A Output Application

## TYPECIAL PERFORMANCE AND CHARACTERISTICS:



Figure8: Ripple Voltage vs Output Current


Figure5: Frequency vs Input Voltage


Figure3: Output Voltage vs Output Current


Figure4: Quiescent Current vs Input Voltage


Figure6: Duty Cycle vs Output Current

## PACKAGE OUTLINE

MSOP-10 PACKAGE OUTLINE AND DIMENSIONS


| Symbol | Dimensions In Millimeters |  | Dimensions In Inches |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Min | Max | Min | Max |
| A | 0.0820 | 1.100 | 0.032 | 0.043 |
| A1 | 0.020 | 0.150 | 0.001 | 0.006 |
| A2 | 0.750 | 0.950 | 0.030 | 0.037 |
| b | 0.180 | 0.280 | 0.007 | 0.011 |
| c | 0.090 | 0.230 | 0.004 | 0.009 |
| D | 2.900 | 3.100 | 0.114 | 0.122 |
| e | $0.50(B S C)$ |  | $0.020($ BSC $)$ |  |
| E | 2.900 | 3.100 | 0.114 | 0.122 |
| E1 | 4.750 | 5.050 | 0.187 | 0.199 |
| L | 0.400 | 0.800 | 0.016 | 0.031 |
| $\theta$ | $0^{0}$ | $6^{0}$ | $0^{0}$ | $6^{0}$ |

