
New LED Lighting IPD

MIP553

2nd Dev. group, Discrete Device Dev. Centre,
Semiconductor Company, Panasonic

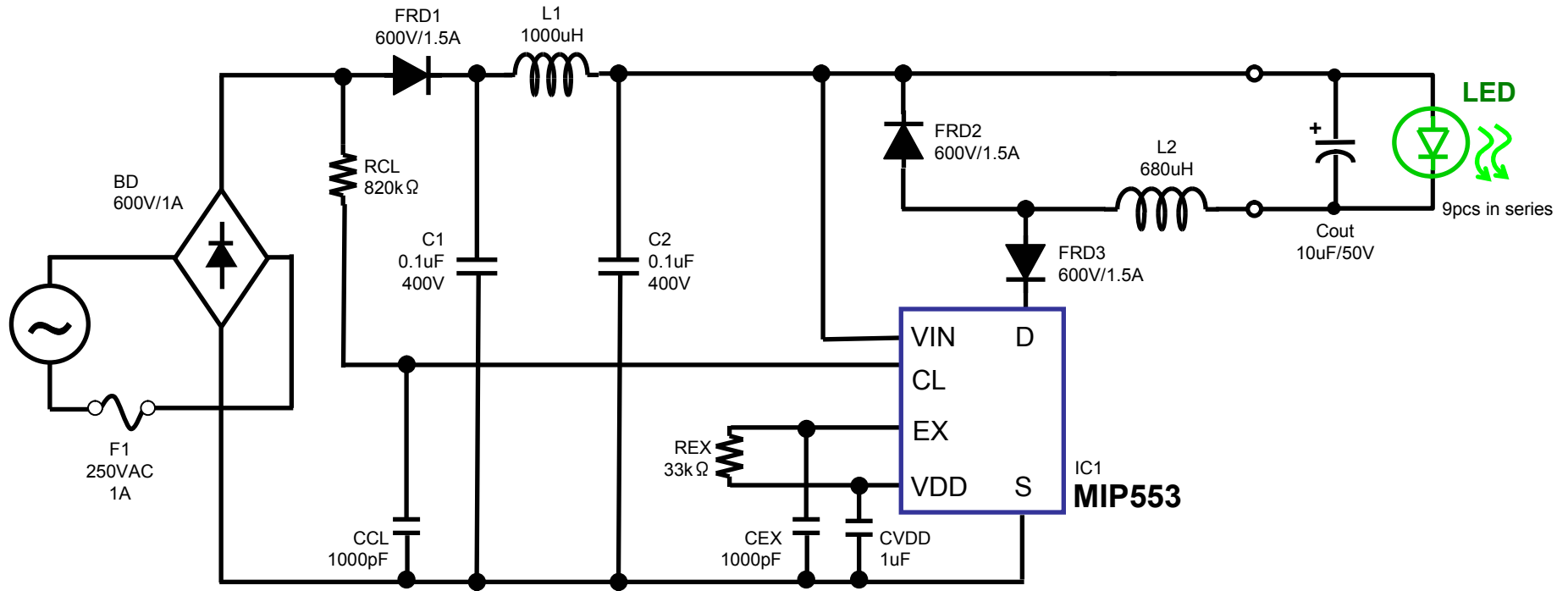
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Example of application circuit

Effective for low output voltage specification and high efficiency



“High efficiency and high PF is achieved with low component count”

Components : 16

$\eta = 85.8\%$, $\text{PF} = 0.93$

Reference data (When LED12pcs load in series is driven)

VAC = 120V , VLED = 28.6V , ILED = 0.390A , Po = 11.1W , Pin = 13.0W

$\eta = 85.8\%$, $\text{pF} = 0.93$

LED current can be adjusted by the constant L2, RCL and REX.

However, the efficiency and PF will change, so please confirm.



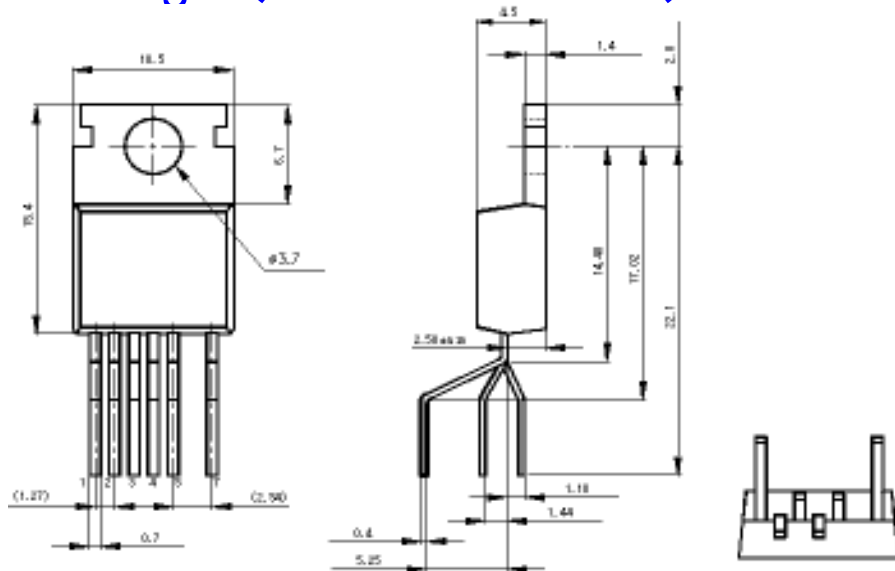
Panasonic ideas for life

MIP553

- Breakdown voltage = 700V *
- On-resistance = 3.5 Ω (typ.)
- DRAIN peak current = 1.5A (typ.)
 - ⇒ LED average current ≤ 0.70A (standard)
- Fixed Off-Time Control (Toff:16us, MaxOn:80us)
- Protection functions
 - Low Input voltage detection
 - LED Short Circuit (skip mode)
 - Over Temperature protection (140 °C, self-recovery)

* : Reliability test applied voltage 630V

Package (TO-220IPD7-A2)



※Not compatible pin name, pin arrangement and function with MIP552.

※There is minor difference in function with MIP554.

Pin arrangement & function

| PinNo. | Pin name | Function |
|--------|----------|---|
| 1 | VIN | Current supply pin for internal circuit & Input voltage detection |
| 2 | EX | External adjustment pin to set peak current value |
| 3 | CL | Peak current control pin according to input voltage |
| 4 | SOURCE | Power MOSFET Source, Circuit GND pin |
| 5 | VDD | Reference voltage pin for internal IPD circuit |
| 7 | DRAIN | Power MOSFET Drain Pin |

Pin comparison with MIP552

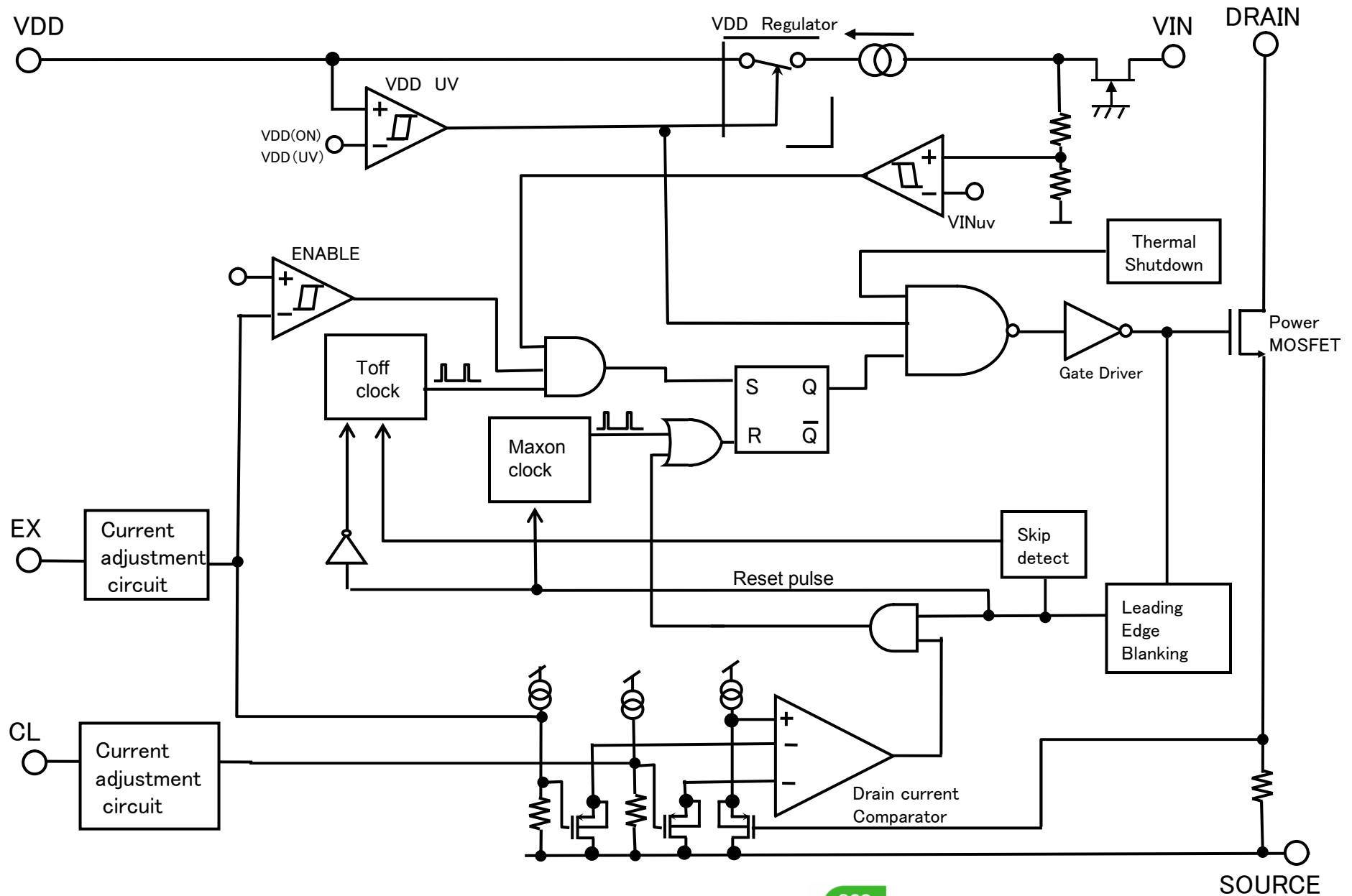
| Pin No. | MIP553 | MIP552 |
|---------|--------|--------|
| 1 | VIN | EX |
| 2 | EX | L |
| 3 | CL | VDD |
| 4 | SOURCE | SOURCE |
| 5 | VDD | VIN |
| 7 | DRAIN | DRAIN |

MIP553 vs MIP552 Characteristics Comparison

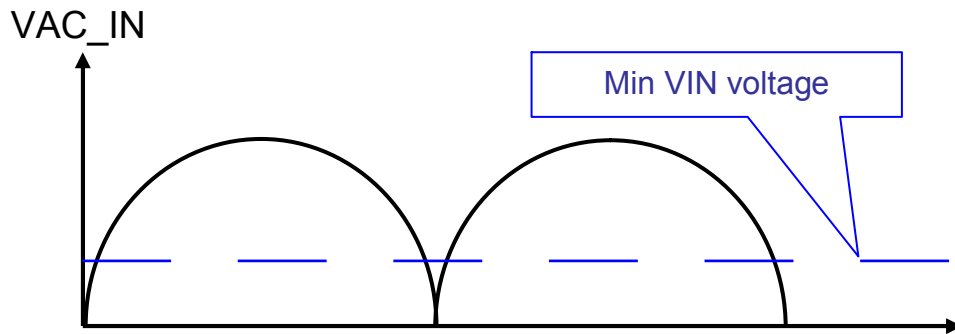
| Items | MIP553 | MIP552 |
|--|--|--|
| Control method | Fix OFF time (16us) | PWM control (44kHz) |
| Ron | 3.5Ω | 6.0Ω |
| ILIMIT | 1.5A | 1.0A |
| Driving input voltage | Low input voltage detection function by VIN pin >24V | >45V |
| EX terminal function | ILIMIT is adjusted by current Remote on/off function for <u>PWM dimmer</u> | ILIMIT is adjusted by voltage Remote on/off function for <u>PWM dimmer</u> |
| CL terminal function (Modified from L terminal function of MIP552) | ILIMIT is adjusted by current For <u>simple PFC</u> or <u>TRIAC dimmer</u> | - |
| VDD(ON) | 6.5V | 5.8V |
| Protection function | Over temperature protection: 140°C (self recovery Δ70°C) LED short protection (skip mode) | Over temperature protection: 140°C (self recovery Δ70°C) LED short protection (skip mode) |



Block diagram

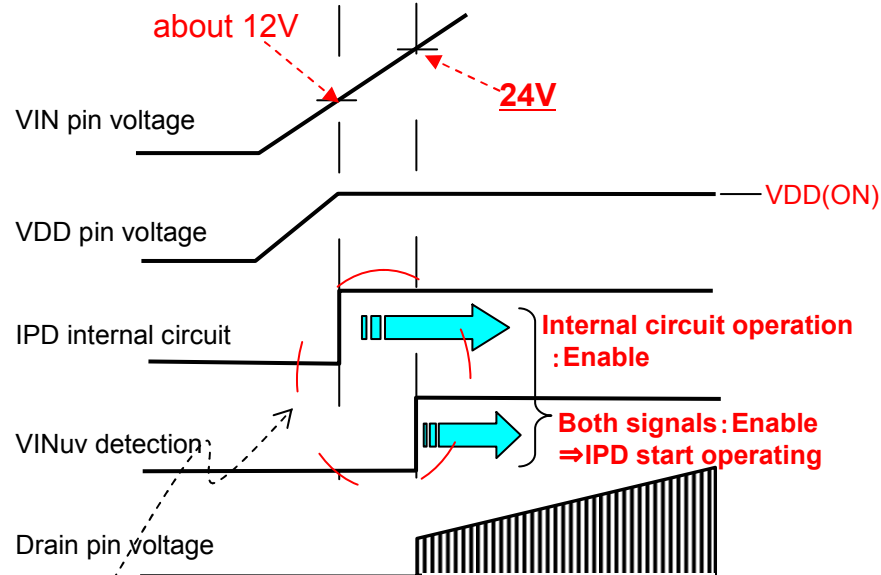


Fixed Driving voltage



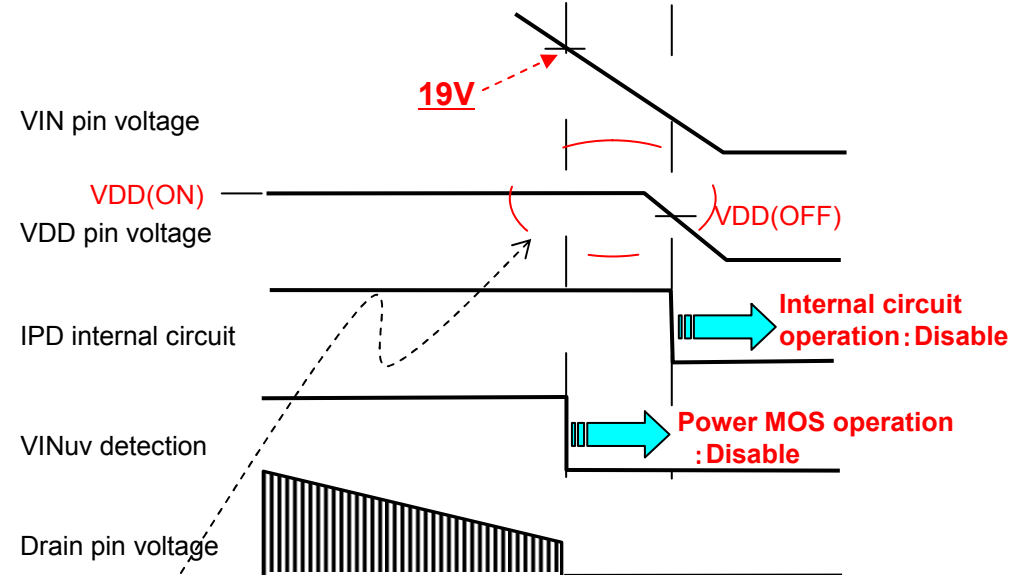
- VDD reaches to startup voltage around $VIN \doteq 12V$ by enhancing current charging capability of VIN pin.
- Start-up driving voltage is set by VIN voltage detecting function. Moreover, hysteresis operation can prevent any unstable operation just after operation start.

Each pin waveform at startup & input voltage rising

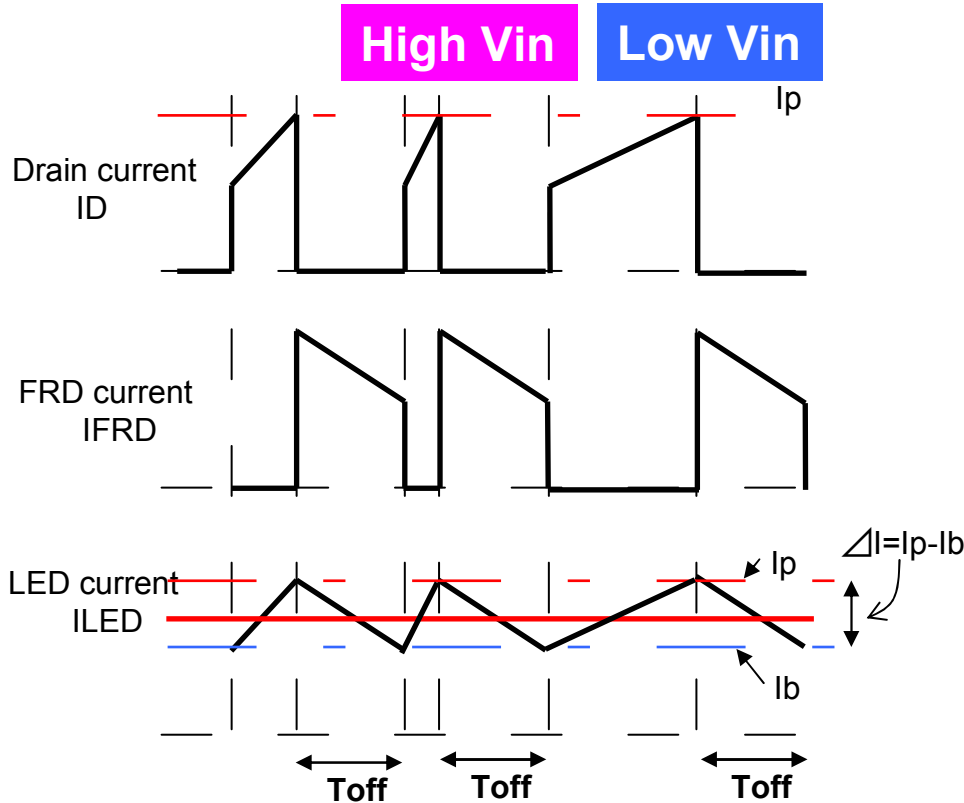


When VDD pin becomes $>VDD(ON)$ and also VIN pin becomes $>VINuv$, IPD starts operation.
 As the charging time to VDD pin capacitor is necessary when power supply startup, VDD pin voltage might become $VDD(ON)$ only after VIN pin becomes $>VINuv$. This will be different from the figure above.

Each pin waveform at stopping & input voltage dropping



VDD pin maintains $VDD(ON)$ even though IPD oscillation stops. In this case, when input voltage becomes $>VINuv$, IPD restarts the operation. However when input voltage continues to drop, VDD pin becomes $<VDD(OFF)$ due to lower charging capability, and internal circuit also stops the operation.



• MOS turn-on duration

$$I_D = I_b + \frac{(V_{in} - V_o)}{L} \times T_{on} \quad \dots \text{formula ①}$$

• MOS turn-off duration

$$I_D = I_p - \frac{V_o}{L} \times T_{off} \quad \dots \text{formula ②}$$

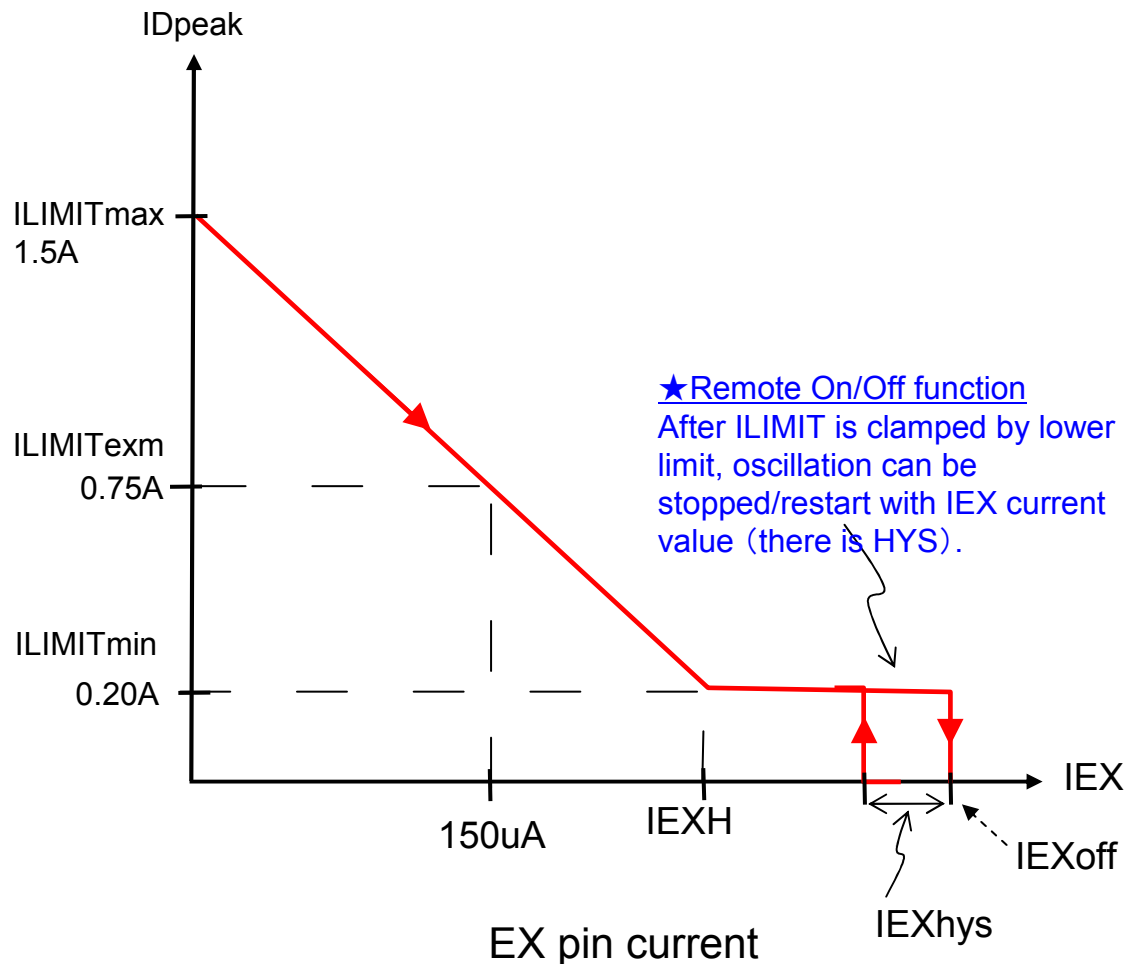
• **Average current (I_o) flowed into LED**

$$I_o = \frac{I_p + I_b}{2} = I_p - \frac{V_o}{2L} \times T_{off} \quad \dots \text{formula ③}$$

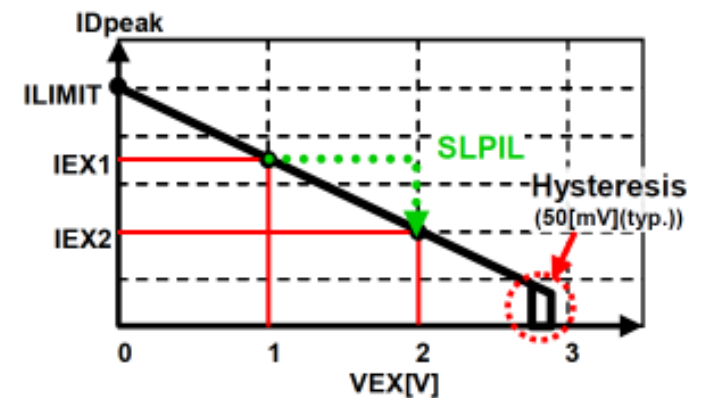
- ★ On-time period of Power MOS is depending on Input voltage, (Refer to formula ①). On-time period becomes shorter at high V_{in} and longer at low V_{in} .
- On-time is restricted by MAXduty in case of PWM method, and Power MOS might turn off before peak current detection point is reached when V_{in} is low.
- However **Power MOS can turn on up to peak current detection value in case of Off time fixed control.**
 (Limitation of Maxon time is set actually.)
- Ripple current ΔI does not depend on input voltage when it is constantly controlled in continuous mode, and **ILED (Average current value) that flows into LED can be always controlled constantly.**
- ★ Oscillation frequency changes depending on input voltage.
This jitter function can reduce EMI average noise
- ★ I_o (LED current) is shown simply as formula ③ and so application designing could be easier.

External setting of peak current detection value by EX pin

- IDpeak detection value can be set externally by supplying DC current into EX pin.
- IDpeak detection value becomes lower with higher IEX supplied current, and it is clamped at ILIMIT(min).
- Apart from IDpeak control function by CL pin, IDpeak detection value can be set individually.
(IDpeak detection value set by EX pin has the priority.)
- Oscillation stops at IEXoff , with hysteresis of IEXhys. It is possible for PWM dimmer control application.



MIP52 EX pin control method

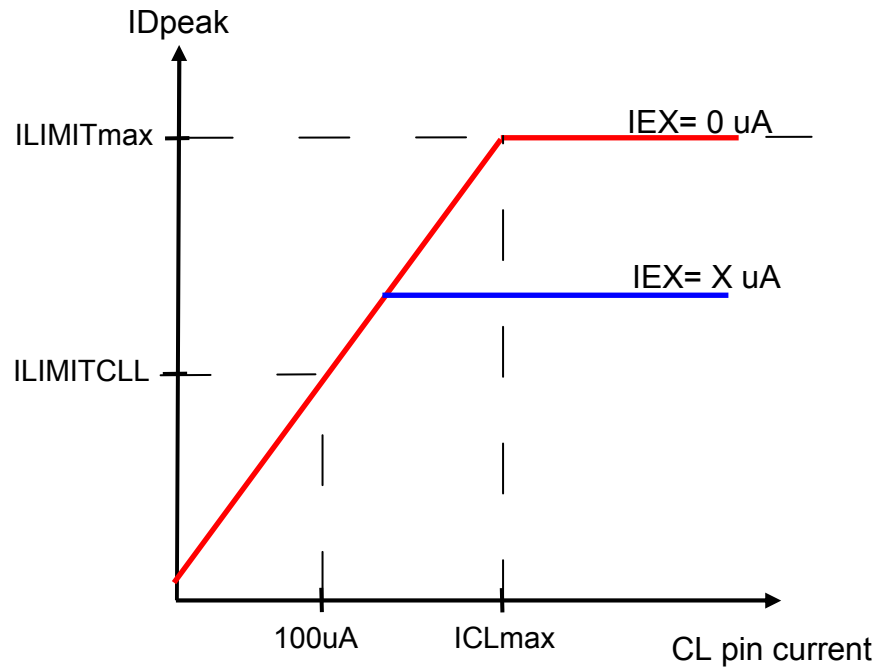


※Control method of EX pin are different for MIP53 and MIP52

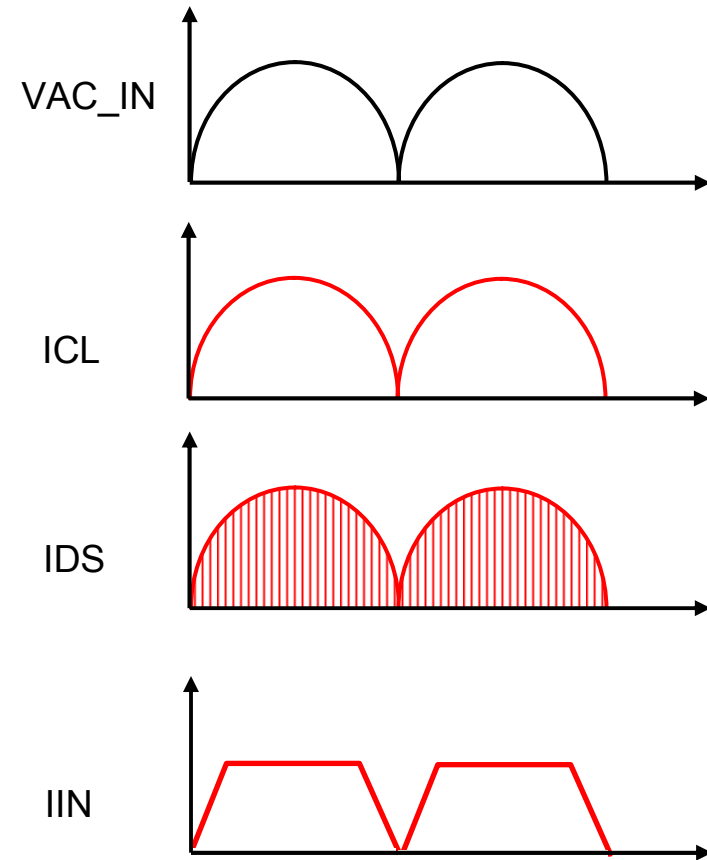
In **MIP52**, IDpeak is controlled by EX pin voltage as shown in the figure above. IDpeak decreases when VEX increases.

In **MIP53**, IDpeak is controlled by EX pin current . IDpeak decreases when IEX increases.

IDpeak vs. ICL Characteristic



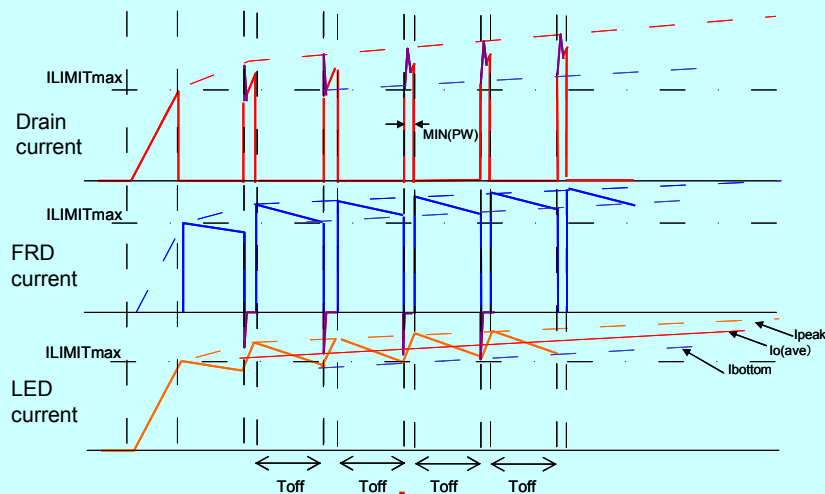
- ID_{peak} detection value changes according to the DC current supplied into CL pin.
- Please connect a resistor between VDD and CL when the CL function is not used.
- ID_{peak} level can be changed by EX pin current.



- Input voltage after total rectification is added to CL pin through the resistor and CL current changes linearly depending on input voltage waveform.
- ID_{peak} detection value changes according to DC current supplied into CL pin.
- When the current value flowed into IPD changes depending on the change of input voltage by the control above, Input current flows during almost all the period as the figure above. Power factor can be improved as a result.

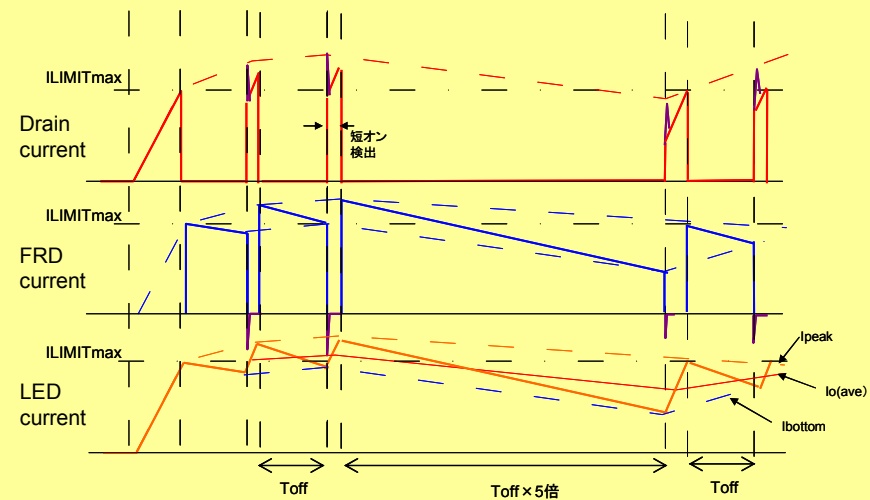
MIN(PW) that Power MOS of this IPD can turn on is designed to be about 410ns.
(Depending on on-time blanking width (TBLK) & Peak current detection delayed time ($t_d(OCL)$)
Peak current control is not effective during the operation within minimum pulse width.
In order to avoid this operation, off time is increased to 5 times longer, when on-time of power MOS becomes close to minimum pulse width. (Skip(PW): About 510ns)
Therefore current value at turn on timing of next pulse becomes smaller and on-time becomes longer. This prevents minimum pulse operation.

Without skip mode function



Output current increases when min pulse operation is repeated.

With skip mode function



Output current is decreased/increased repeatedly due to the detection before the pulse becomes minimum.

Main specs item

The specs value is tentative. It will be subjected to change in the future.

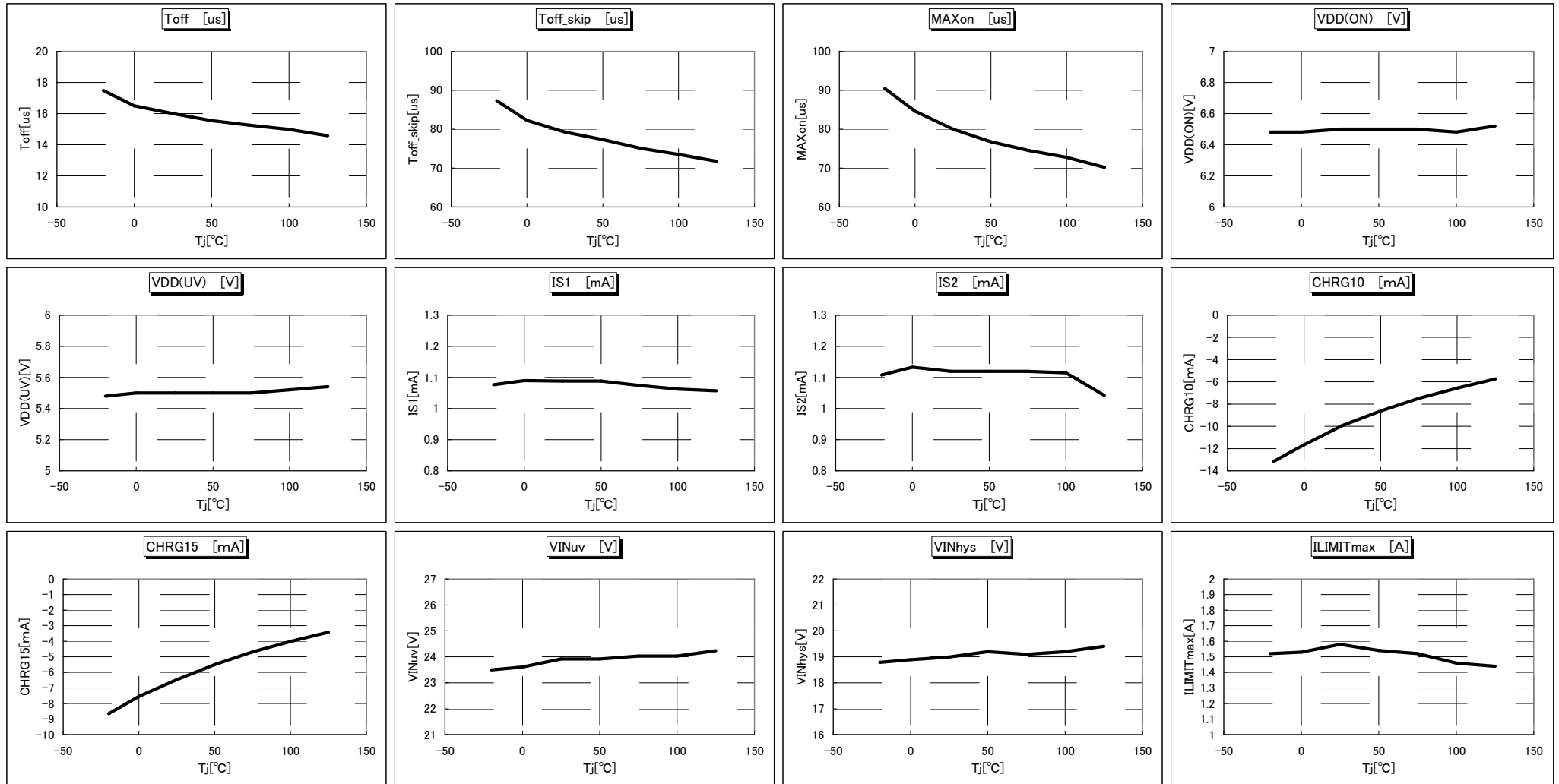
* Design guarantee item. The final test is not executed.

| NO | Item | Symbol | Condition | SPEC | | | Unit |
|-----|--|------------|---|----------|------|------|------|
| | | | | typ | min | max | |
| 1 | Constant OFF time | Toff | VDD=VDD(ON)+0.1V, VD=5V, VIN=50V, IEX=0uA, ICL=ICLmax+50uA | 16 | 14.4 | 17.6 | us |
| 2 | Skip mode Constant OFF time | Toff skip | VDD=VDD(ON)+0.1V, VD=5V, VIN=50V, IEX=0uA, ICL=ICLmax+50uA Ton<Skip(PW) | 5.0×Toff | TBD | TBD | us |
| 3 | Maximum ON time | MAXon | VDD=VDD(ON)+0.1V, VD=5V, VIN=50V, IEX=0uA, ICL=ICLmax+50uA | 80 | TBD | TBD | us |
| 4 | VDD Start Voltage | VDD(ON) | VIN=50V, VD=5V, VEX=0uA, ICL=ICLmax+50uA | 6.5 | TBD | TBD | V |
| 5 | VDD Stop Voltage | VDD(UV) | VIN=50V, VD=5V, VEX=0uA, ICL=ICLmax+50uA | 5.5 | TBD | TBD | V |
| 6 | Circuit Current before Strat | IS1 | VDD=VDD(ON)-0.2V, IEX=0uA, ICL=ICLmax+50uA | 1.09 | TBD | TBD | mA |
| 7 | Circuit Current under Switching | IS2 | VDD=VDD(ON)+0.1V, IEX=0uA, ICL=ICLmax+50uA | 1.12 | TBD | TBD | mA |
| *8 | EX Pin Current for setting ILIMITmin | IEXH | VDD=VDD(ON)+0.1V, VIN=50V, ICL=ICLmax+50uA, ILIMIT⇒ILIMITmin | 260 | | | μA |
| 9 | EX Pin Current at oscillation stop | IEXoff | VDD=VDD(ON)+0.1V, VIN=50V, ICL=ICLmax+50uA | 430 | TBD | TBD | μA |
| 10 | EX Pin Current Hysteresis at oscillation restart | IEXhys | VDD=VDD(ON)+0.1V, VIN=50V, ICL=ICLmax+50uA | 50 | | | μA |
| 11 | EX Pin Voltage | VEXM | VDD=VDD(ON)+0.1V, VIN=50V, IEX=150uA | 2.55 | TBD | TBD | V |
| | | VEXH | VDD=VDD(ON)+0.1V, VIN=50V, IEX=IEXH | 2.8 | TBD | TBD | V |
| | | VEXoff | VDD=VDD(ON)+0.1V, VIN=50V, IEX=IEXoff | 3.2 | TBD | TBD | V |
| 12 | EX Pin Short Current | IEXSVDD | VEX=VDD, VDD=VDD(ON)+0.1V, VIN=50V | 1.0 | TBD | TBD | mA |
| | | IEX0 | VEX=0V, VDD=VDD(ON)+0.1V, VIN=50V | 0 | | | μA |
| 13 | CL Pin Current for setting ILIMITmax | ICLmax | VDD=VDD(ON)+0.1V, VIN=50V, IEX=0uA, ILIMIT=ILIMITmax | 300 | TBD | TBD | μA |
| 14 | CL Pin Voltage | VCLmax | VDD=VDD(ON)+0.1V, VIN=50V, ICL=ICLmax | 2.9 | TBD | TBD | V |
| 15 | CL Pin Short Current | ICLSVDD | VDD=VDD(ON)+0.1V, VIN=50V, VCL=VDD | 1.30 | TBD | TBD | mA |
| | | ICL0 | VDD=VDD(ON)+0.1V, VIN=50V, VCL=0V | 0 | | | μA |
| 16 | Maximum Peak Current Limit | ILIMITmax | VDD=VDD(ON)+0.1V, VIN=50V, IEX=0uA, ICL=ICLmax+50uA | 1.5 | 1.38 | 1.62 | A |
| *17 | ILIMIT ICL100 | ILIMITCLL | VDD=VDD(ON)+0.1V, VIN=50V, IEX=0uA, ICL=100uA | 0.6 | | | A |
| 18 | ILIMIT IEX150 | ILIMITexm | VDD=VDD(ON)+0.1V, VIN=50V, IEX=150uA, ICL=ICLmax+50uA | 0.75 | 0.69 | 0.81 | A |
| 19 | Minimum Clamp ILIMIT | ILIMITmin | VDD=VDD(ON)+0.1V, VIN=50V, IEX=IEXH+20uA, ICL=ICLmax+50uA | 0.2 | TBD | TBD | A |
| *20 | Leading Edge Blanking Delay | ton(BLK) | | 200 | 150 | 250 | ns |
| *21 | Peak Current Limit Delay | td(OCL) | | 200 | | | ns |
| 22 | Minimum on-pulse width | MIN(PW) | VIN=50V, VD=35V, VDD=open, IEX=0uA, ICL=ICLmax+50uA | 410 | TBD | TBD | ns |
| *23 | Skip detect on-pulse width | Skip(PW) | VIN=50V, VDD=VDD(ON)+0.1V, IEX=0uA, ICL=ICLmax+50uA | 510 | | | ns |
| *24 | Thermal Shutdown Junction Temperature | TOTPj | | 140 | 130 | 150 | °C |
| *25 | Thermal Shutdown Hysteresis | ΔTOP | | 70 | | | °C |
| 26 | ON-State Resistance | RDS(ON) | VDD=VDD(ON)+0.1V, VIN=50V, IEX=0uA, ICL=ICLmax+50uA, IDS=300mA | 3.5 | | TBD | Ω |
| 27 | OFF-State leakage Current of DRAIN Pin | IDSS | VDD=VDD(ON)+0.1V, VCL=0V, IEX=IEXoff+10uA, VDS=630V | 1 | | TBD | μA |
| 28 | Breakdown Voltage of DRAIN Pin | VDSS | VDD=VDD(ON)+0.1V, VCL=0V, IEX=IEXoff+10uA, IDS=100uA | | 700 | | V |
| 29 | Rise Time | tr | VDD=VDD(ON)+0.1V, VIN=50V, IEX=0uA, | 100 | | | ns |
| 30 | Fall Time | tf | ICL=ICLmax+50uA, VDS=5V | 50 | | 80 | ns |
| 31 | OFF-State leakage Current of VIN Pin | IIN (LEAK) | VDD=VDD(ON)+0.1V, VCL=0V, IEX=IEXoff+10uA, VIN=450V | 26 | | TBD | μA |
| 32 | Breakdown Voltage of VIN Pin | BVVIN | VDD=VDD(ON)+0.1V, VCL=0V, IEX=IEXoff+10uA, IIN=100uA | | 500 | | V |
| 33 | VDD Charging Current | CHRG10 | VIN=40V, VDD=0V, EX, CL: open | -10 | TBD | TBD | mA |
| | | CHRG15 | VIN=40V, VDD=5.5V, EX, CL: open | -6.5 | TBD | TBD | mA |
| 34 | VIN start Voltage | VINuv | VDD: open, VD=5V, IEX=0uA, ICL=ICLmax+50uA | 24 | TBD | TBD | V |
| 35 | VIN start Voltage Hysteresis | VINhys | VDD: open, VD=5V, IEX=0uA, ICL=ICLmax+50uA | 19 | | | V |



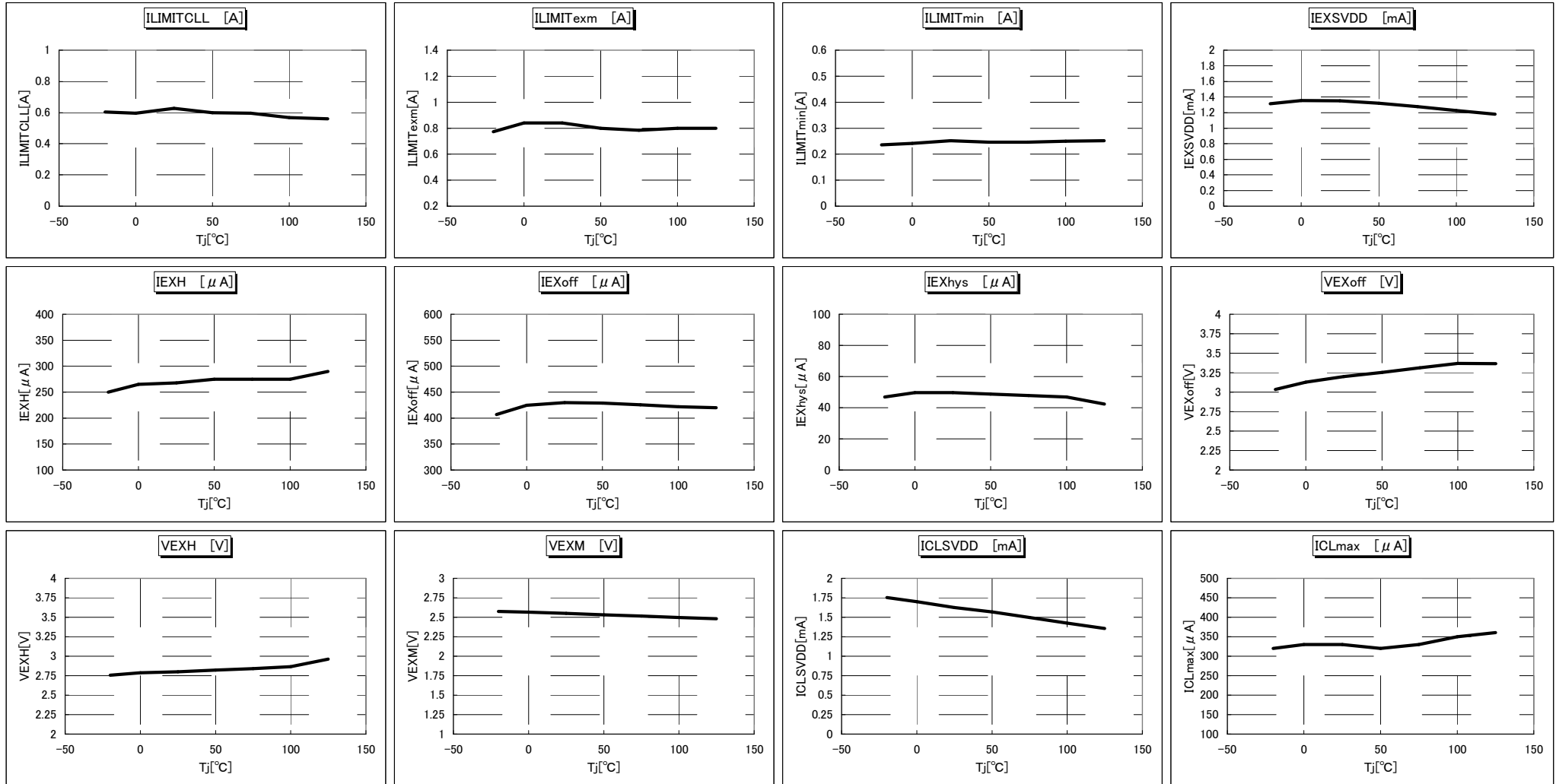
Temperature characteristic data ①

※This is reference data for WS. There may be changes in the end-product.



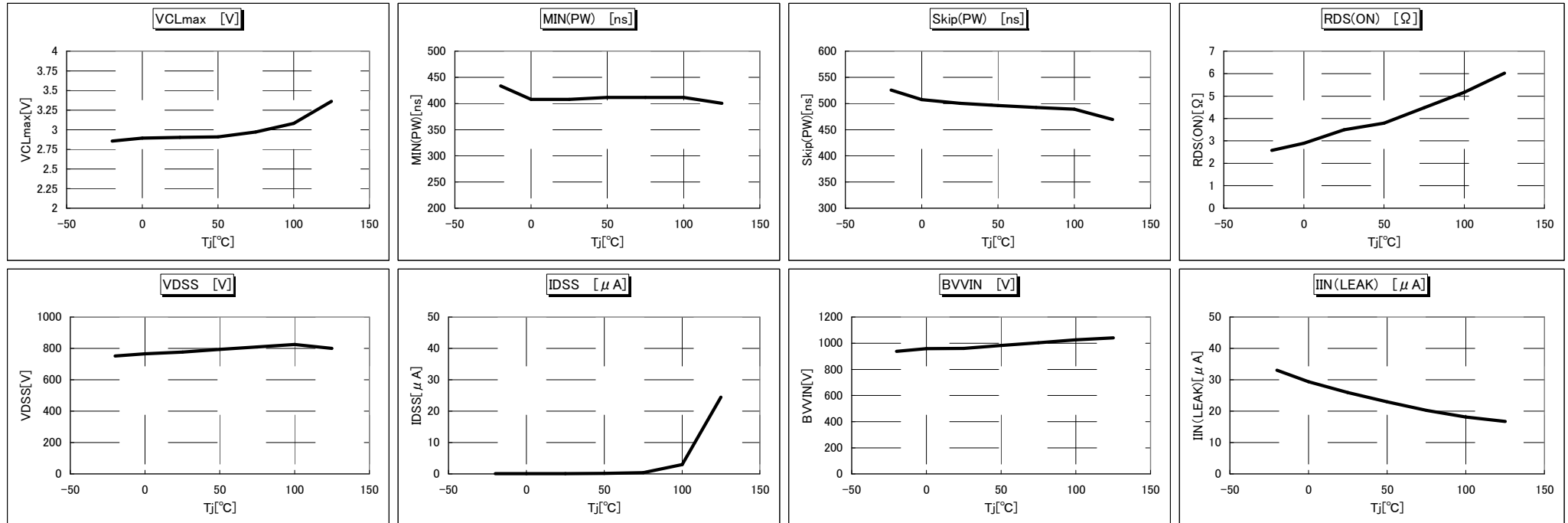
Temperature characteristic data ②

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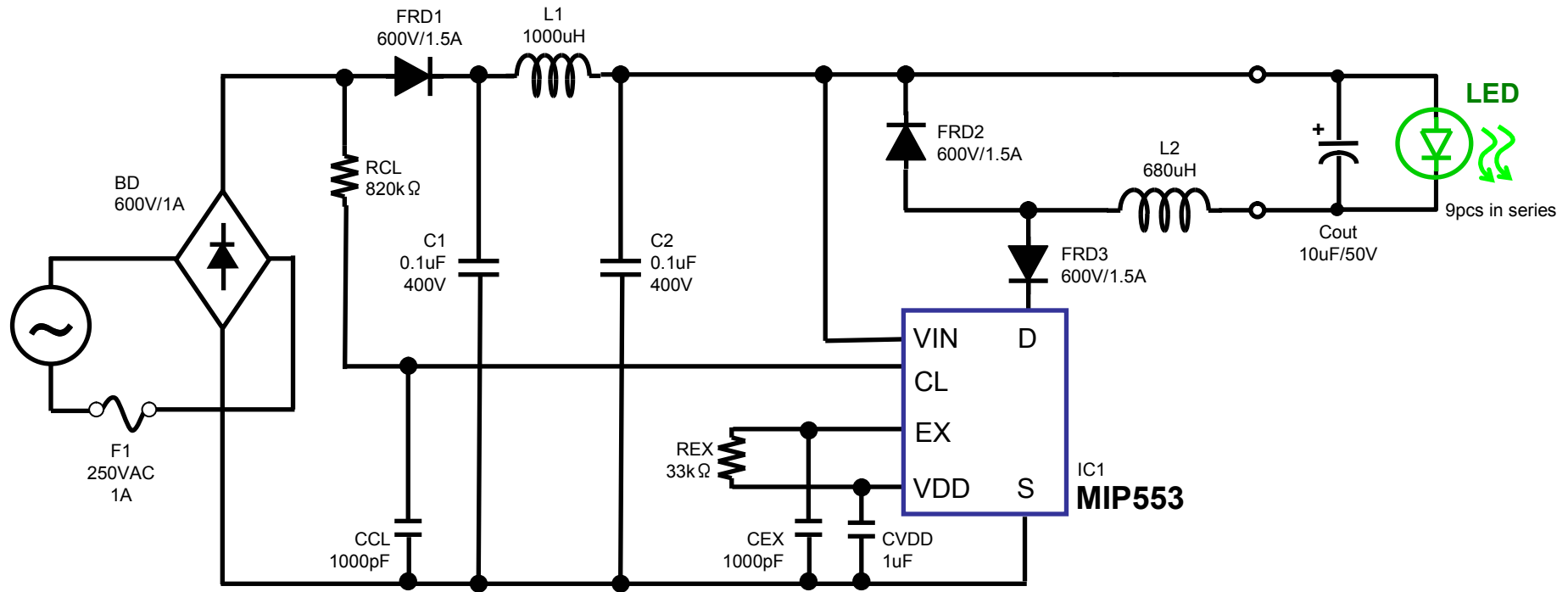


Temperature characteristic data ③

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Effective for low output voltage specification and high efficiency



“High efficiency and high PF is achieved with low component count”

Components : 16

$\eta = 85.8\%$, $PF = 0.93$

Reference data (When LED12pcs load in series is driven)

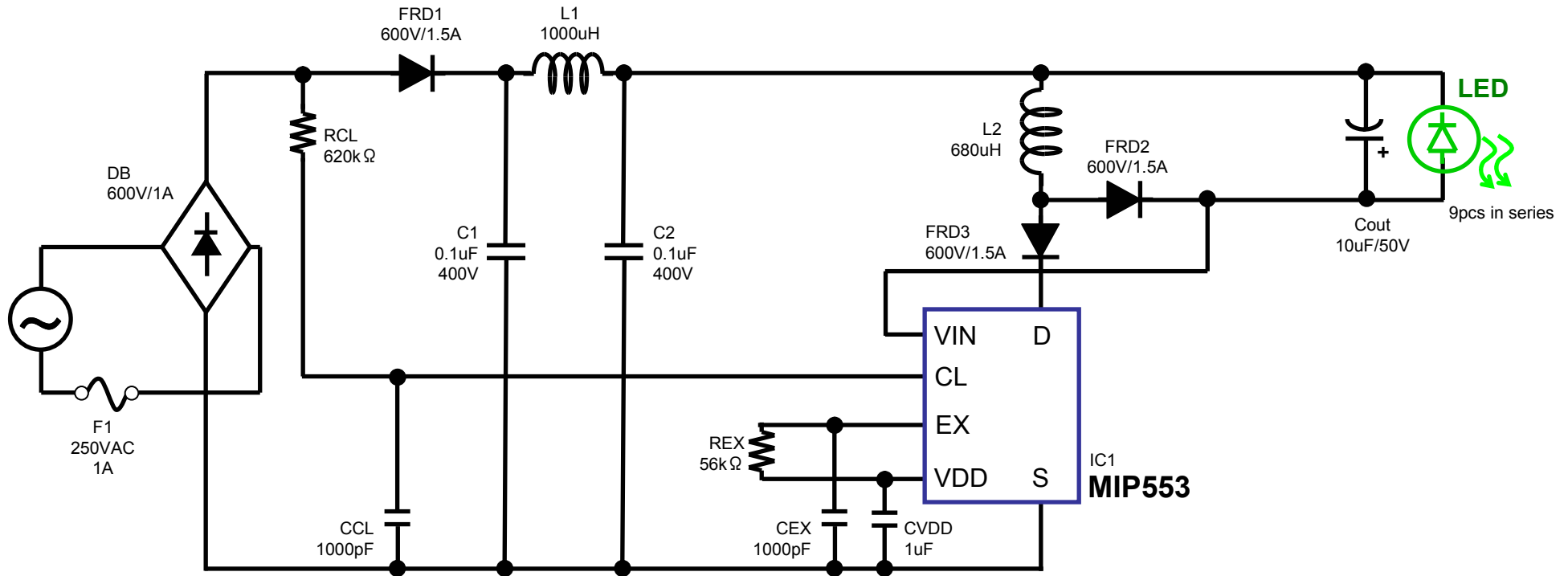
VAC = 120V , VLED = 28.6V , ILED = 0.390A , Po = 11.1W , Pin = 13.0W

$\eta = 85.8\%$, $PF = 0.93$

LED current can be adjusted by the constant L2, RCL and REX.

However, the efficiency and PF will change, so please confirm.

Effective for high output voltage specification and high PF



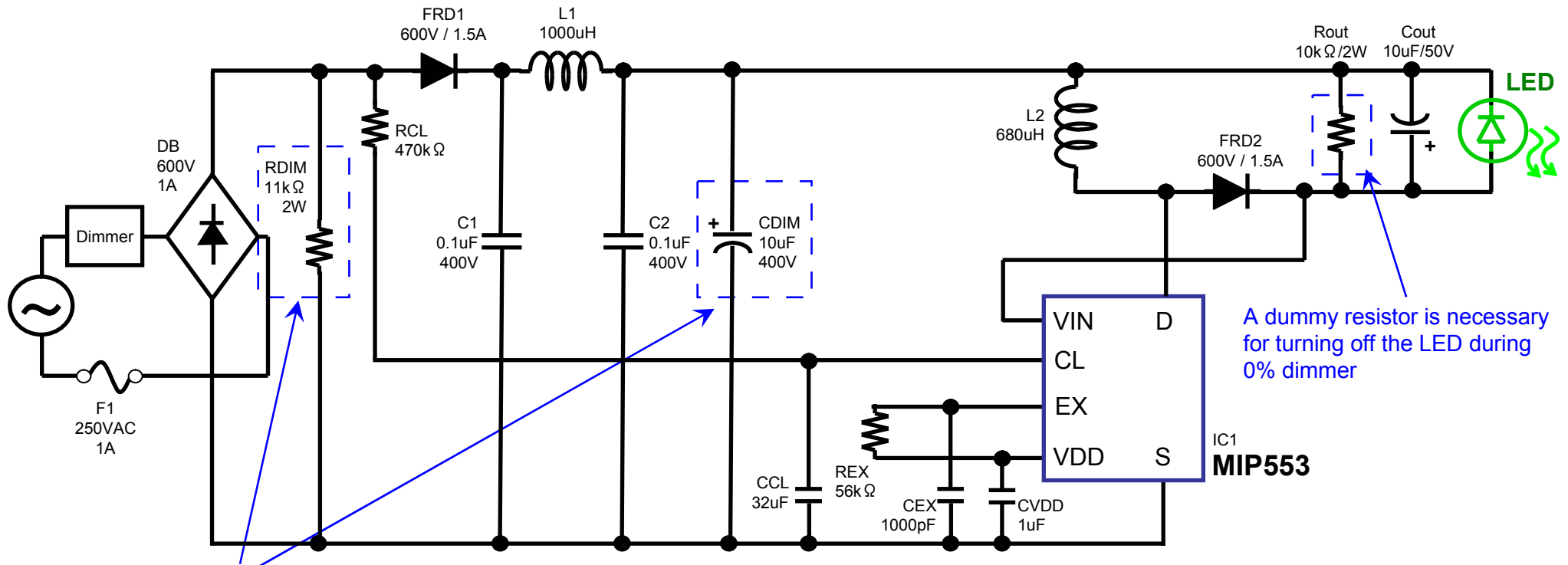
“High PF is achieved
with low component
count”
PF=0.95

Reference data (When LED 10pcs load in series is driven)

VAC = 120V , VLED = 28.4V , ILED = 0.379A , Po = 10.7W , Pin = 13.4W
 $\eta = 80.4\%$, $pF = 0.95$

LED current can be adjusted by the constant L2, RCL and REX.
 However, the efficiency and PF will change, so please confirm.

For TRIAC dimmer (Reference circuit)



These components are necessary for smooth dimming operation when connected to a TRIAC dimmer.

“TRIAC dimmer is achieved with low component count”

Components : 18

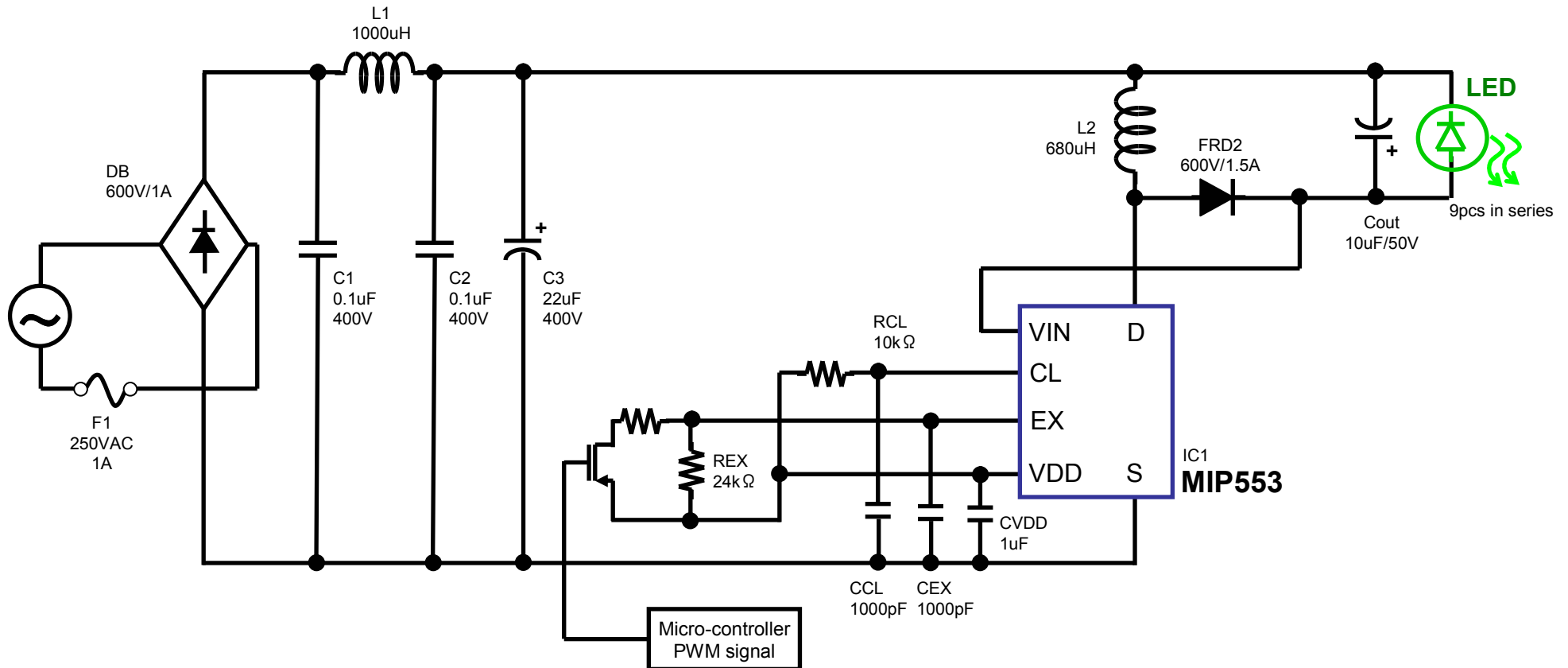
※Buck-Boost type is recommended for flicker-free dimming.
(The buck type will cause oscillation to occur during the stopping period at low input condition)

Please adjust the value of L2, RCL and REX when LED current is increased.

Please adjust RCL, RDIM and CDIM to prevent malfunction of the dimmer.

Moreover, a dummy resistor Rout is necessary to turn of the LED during 0% dimmer.

For PWM dimmer (Reference circuit)



The circuit diagram above is a reference circuit.

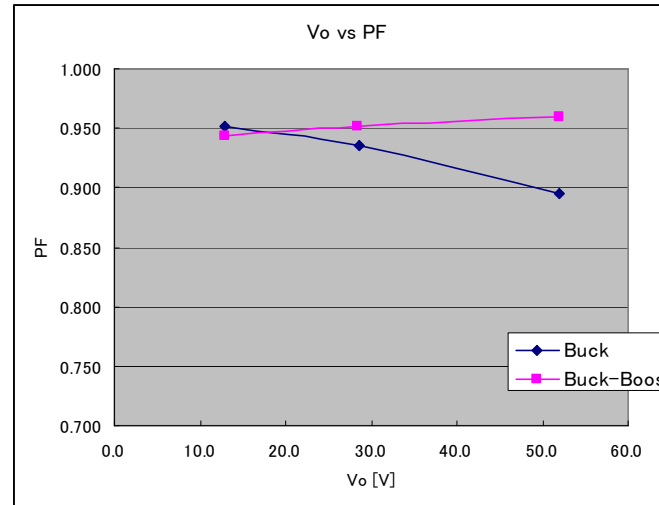
The LED current at 100% dimmer can be adjusted by L2, RCL and REX.

Please modify the circuit configuration according to the micro-controller used.

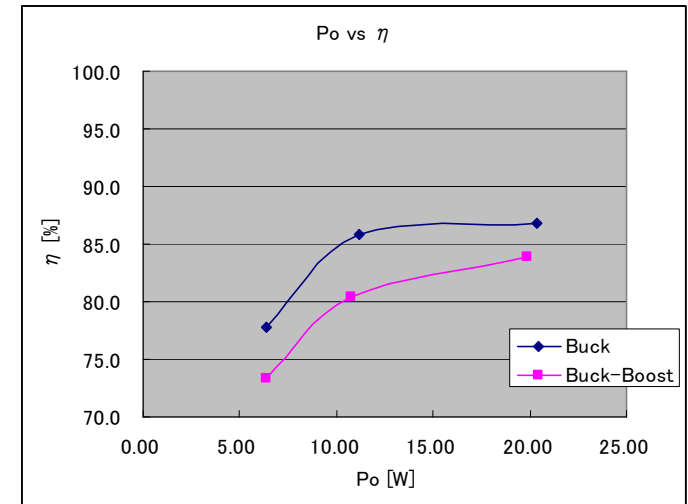
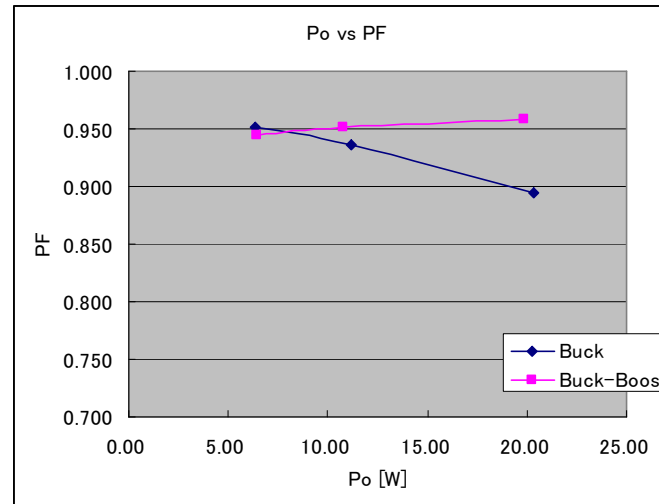
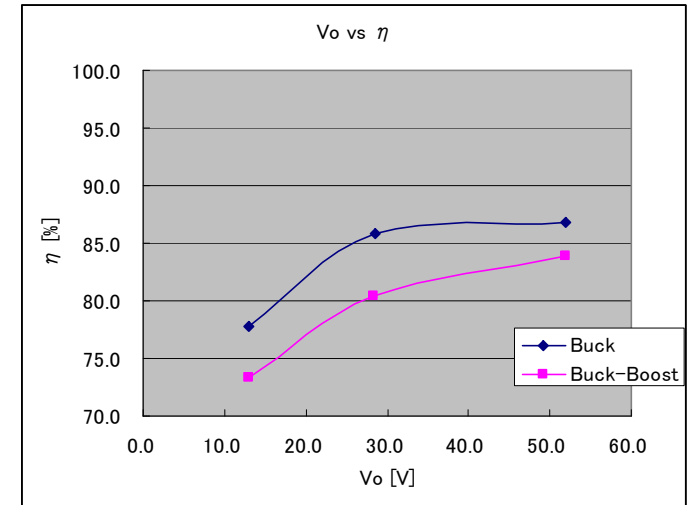
<Measurement condition>

- Input: AC120V
- Load: LED
 - 12V / 500mA
 - 27V / 400mA
 - 54V / 400mA
 (Constants adjusted for each specification)
- Circuit: Buck, Buck-Boost
- Ta: Normal temperature (about 27°C)
- Open frame

Power Factor data



Efficiency data

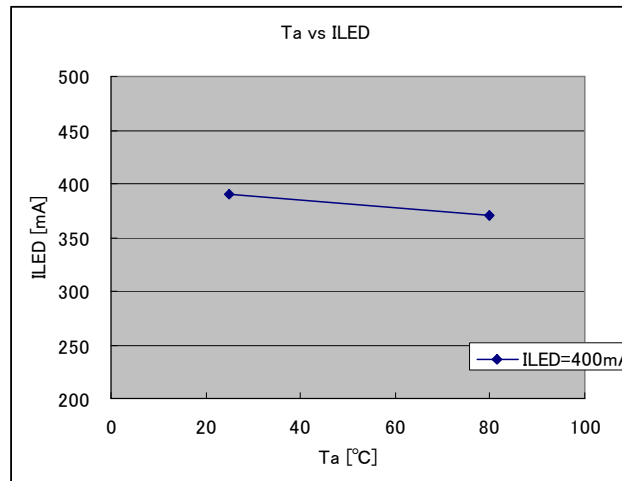


LED Current accuracy

Temperature characteristic (※Confirmation of temperature effect on I_{LIMIT})

<Measurement condition>

- Input: AC120V
- Load: LED 9pcs
27V / 400mA
- Circuit: Buck
Without input filter capacitor
- Ta: Normal Temperature
(about 27°C)
Open frame

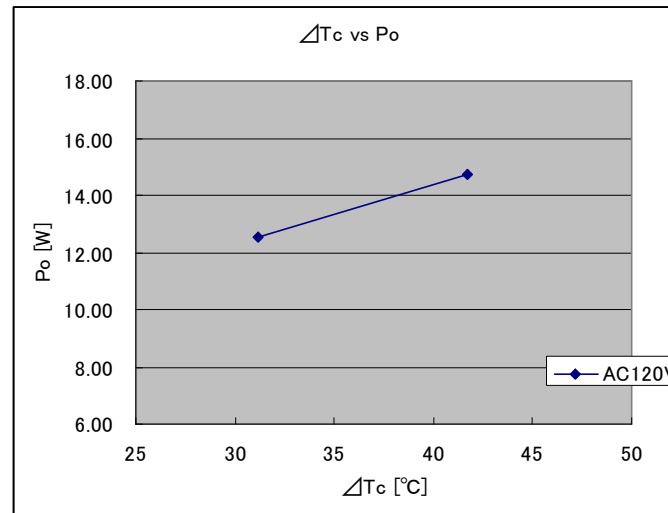


Driving ability (Heat generation evaluation)

<Measurement condition>

- Input: AC120V
- Load: LED 9pcs (about 27V)
(LED current adjusted)
- Circuit: Buck
- Ta: Normal temperature
(about 27°C)
Open frame

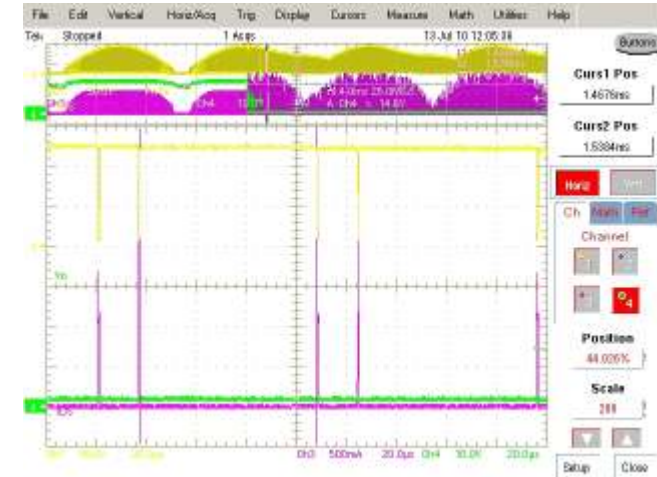
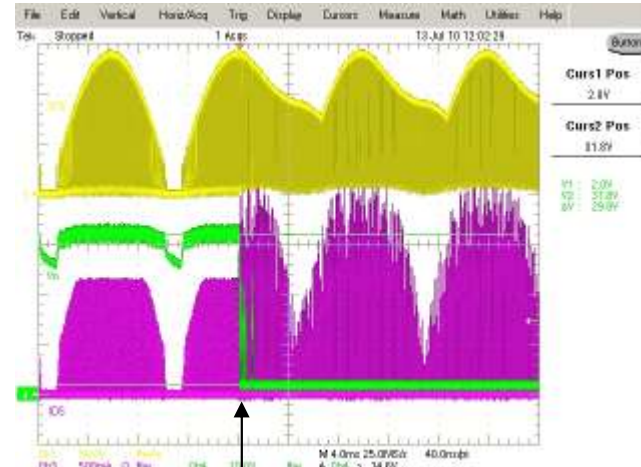
| VIN | FL | lin | Pin | Io | Vo | Po | η | Tc | ΔTc |
|-----|----|-------|-------|-----|------|-------|------|------|------|
| VAC | Hz | mA | W | mA | V | W | % | °C | °C |
| 120 | 50 | 133.4 | 14.60 | 436 | 28.8 | 12.55 | 85.9 | 58.2 | 31.2 |
| 120 | 50 | 152.8 | 17.45 | 508 | 29.0 | 14.75 | 84.5 | 68.7 | 41.7 |



<Measurement condition>

- Input: AC100V
- Load: LED 9pcs (about 27V)
- Circuit: Buck

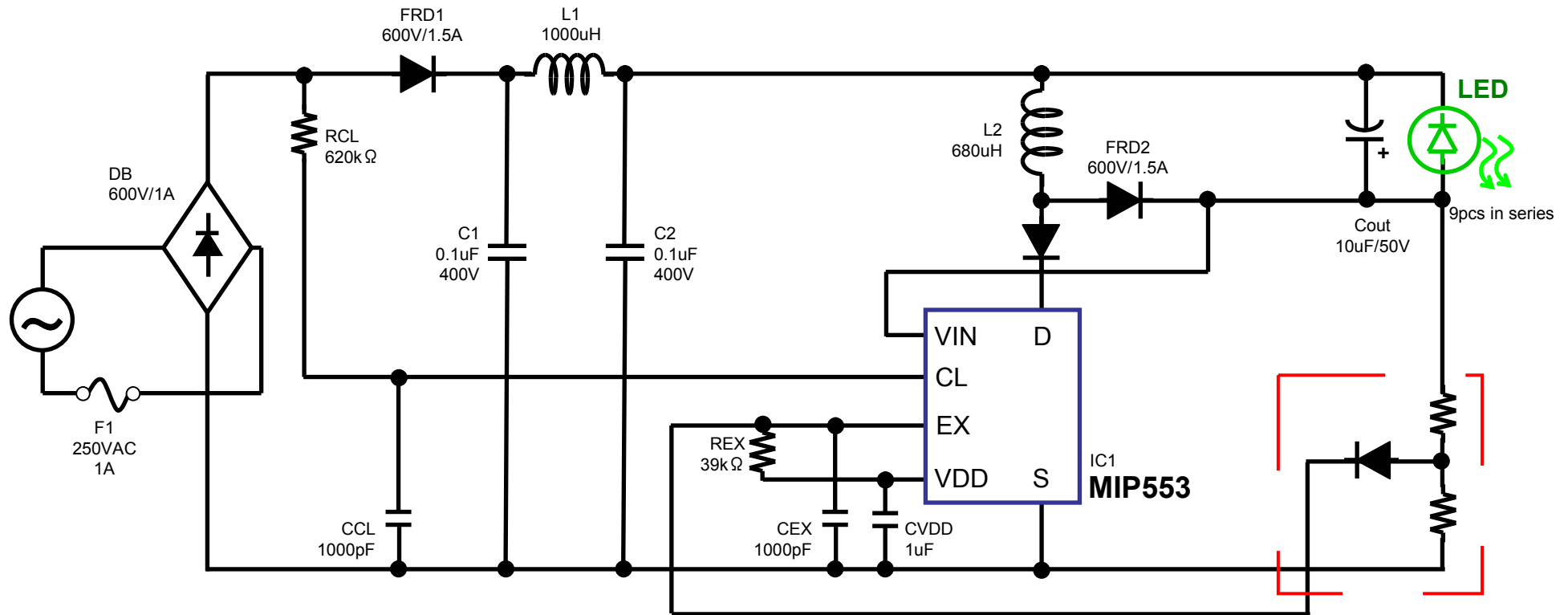
■ It is confirmed that the protection function during LED short is able to operate.



Pin=15W → Reduce to Pin=1.7W

Short occur

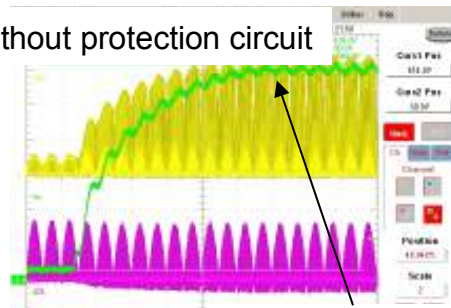
Oscillation stop function with EX pin Buck-Boost)



<Measurement condition>

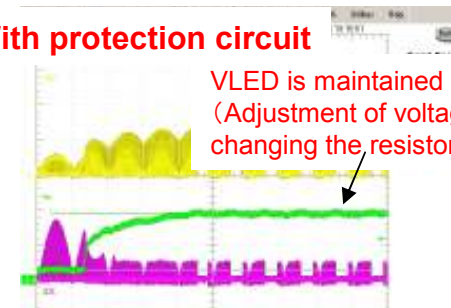
- Input: AC50V
- Load: LED 9pcs (about 27V)
- Circuit: Buck-Boost
LED parallel capacitor 10uF

Without protection circuit



VLED rise up to about 600V

With protection circuit



VLED is maintained at about 200V.
(Adjustment of voltage is possible by changing the resistor value)

For the simplification of the external components design, such as the L value of the coil, CL resistance (RCL), EX resistance (REX), etc., a calculation sheet shown in the figure below has been prepared. If the sheet is required, please contact us.

