# MP4026

## Primary-Side-Control, Offline LED Controller with Active PFC

***PRELIMINARY SPECIFICATIONS SUBJECT TO CHANGE***

***MPS CONFIDENTIAL AND PROPRIETARY INFORMATION– LUXBETTER USE ONLY***

## DESCRIPTION

The MP4026 is a primary-side-control, offline LED controller that achieves high-power factor and accurate LED current for isolated, single-power-stage lighting applications in an FCTSOT package. The proprietary real-current-control method accurately controls LED current from primary-side information with good line and load regulation. The primary-side-control eliminates the secondary-side feedback components and the opto-coupler to significantly simplify LED-lighting-system design.

The MP4026 integrates power-factor correction and works in boundary-conduction mode to reduce MOSFET switching losses.

The MP4026's multiple protection features greatly enhance system reliability and safety. These features include over-voltage protection, short-circuit protection, primary-side over-current protection, brown out protection, cycle-by-cycle current limiting, $V_{CC}$ under-voltage lockout, and auto-restart over-temperature protection.

## FEATURES

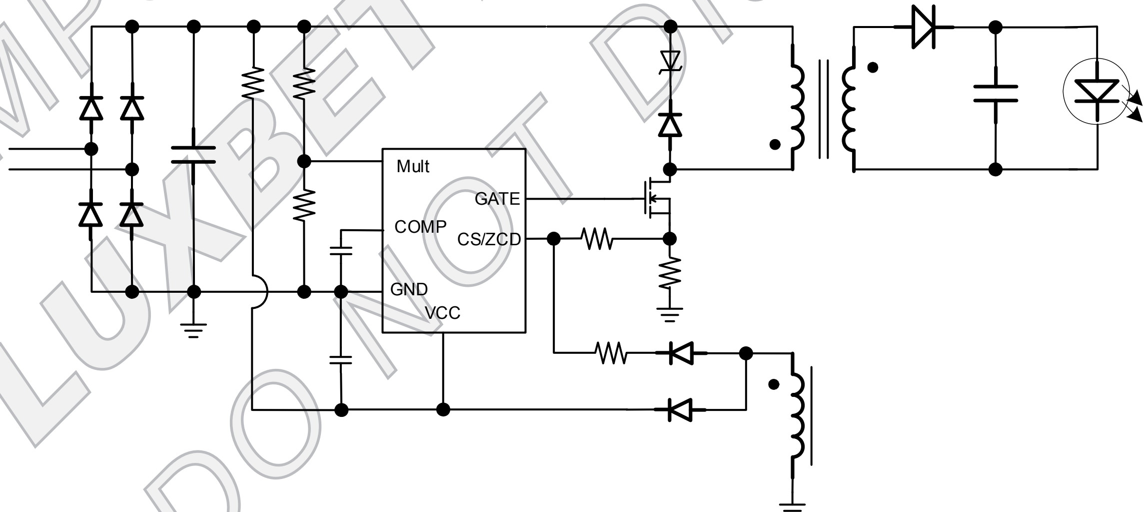
- Real-Current Control without Secondary-Feedback Circuit
- Good Line/Load Regulation
- High Power Factor (≥0.9) over Universal Input Voltage
- Boundary Conduction Mode for Improved Efficiency
- Brown-Out Protection
- Over-Voltage Protection
- Short-Circuit Protection
- Over-Temperature Protection
- Primary-Side Over-Current Protection
- Cycle-by-Cycle Current Limit
- Input UVLO
- Available in FCTSOT-6

## APPLICATIONS

- Industrial and Commercial Lighting
- Residential Lighting



## TYPICAL APPLICATION CIRCUIT

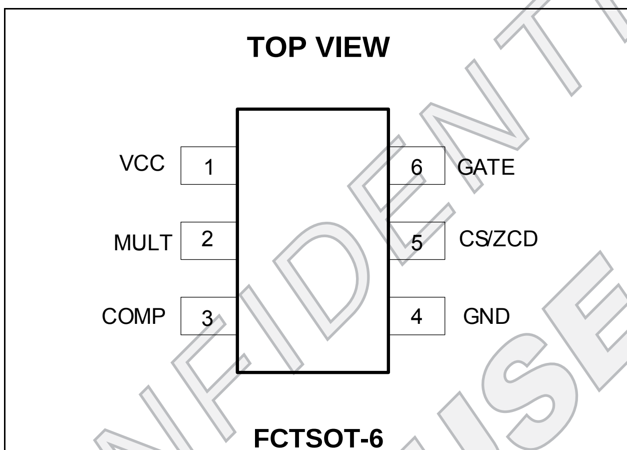


## ORDERING INFORMATION

| Part Number | Package | Top Marking |
|---|---|---|
| MP4026GJ* | FCTSOT-6 | AFS |

* For Tape & Reel, add suffix –Z (e.g. MP4026GJ–Z);

## PACKAGE REFERENCE




## ABSOLUTE MAXIMUM RATINGS [(1)]

Input Voltage $V_{CC}$ ..........................-0.3V to +30V
Gate Drive Voltage .......................-0.3V to +15V
ZCD Pin .........................................-0.3V to 6.5V
Other Analog Inputs and Outputs ..-0.3V to 6.5V
Max. Gate Current .................................. ±0.6A
Continuous Power Dissipation ($T_A$ = +25°C)[(2)]
FCTSOT-6 .............................................. 1.25W
Junction Temperature ...............................150°C
Lead Temperature ....................................260°C
Storage Temperature............... -65°C to +150°C

### *Recommended Operating Conditions* [(3)]

Supply Voltage $V_{CC}$ ..........................9.5V to 27V
Maximum Junction Temp. ($T_J$). ...............+125°C

| *Thermal Resistance* [(4)] | $\theta_{JA}$ | $\theta_{JC}$ | |
|---|---|---|---|
| FCTSOT-6………………….. | 100.... | 55.. | °C/W |

**Notes:**

1) Exceeding these ratings may damage the device.
2) The maximum allowable power dissipation is a function of the maximum junction temperature $T_J$ (MAX), the junction-to-ambient thermal resistance $\theta_{JA}$, and the ambient temperature $T_A$. The maximum allowable continuous power dissipation at any ambient temperature is calculated by $P_D$ (MAX) = ($T_J$ (MAX)-$T_A$)/$\theta_{JA}$. Exceeding the maximum allowable power dissipation will cause excessive die temperature, and the regulator will go into thermal shutdown. Internal thermal shutdown circuitry protects the device from permanent damage.
3) The device is not guaranteed to function outside of its operating conditions.
4) Measured on JESD51-7, 4-layer PCB.

# ELECTRICAL CHARACTERISTICS

**$T_A$ = +25°C, unless otherwise noted.**

| Parameter | Symbol | Condition | Min | Typ | Max | Units |
|---|---|---|---|---|---|---|
| **Supply Voltage** | | | | | | |
| Operating Range | $V_{CC}$ | After turn on | 9.5 | | 27 | V |
| Turn-On Threshold | $V_{CC\_ON}$ | $V_{CC}$ rising edge | 23 | 24 | 25 | V |
| Turn-Off Threshold | $V_{CC\_OFF}$ | $V_{CC}$ falling edge | 8.55 | 9.0 | 9.45 | V |
| Hysteretic Voltage | $V_{CC\_HYS}$ | | 14 | 15 | 16 | V |
| **Supply Current** | | | | | | |
| Start-up Current | $I_{STARTUP}$ | $V_{CC}$= $V_{CC\_ON}$ -1V | | 20 | 30 | μA |
| Quiescent Current | $I_Q$ | No switching | | 0.5 | 0.6 | mA |
| Operating Current Under Fault Condition | | No switching | | 2.3 | | mA |
| Operating Current | $I_{CC}$ | $f_s$ =70kHz, $C_{GATE}$=1Nf | | 2 | 3 | mA |
| **Multiplier** | | | | | | |
| Linear Operation Range | $V_{MULT}$ | | 0 | | 3 | V |
| Gain | K[5] | | | 1.2 | | 1/V |
| Brown-Out Protection Threshold | | | 285 | 300 | 315 | mV |
| Brown-Out Detection Time | | | 25 | 36 | 47 | ms |
| Brown-Out-Protection-Hysteretic Voltage | | | 90 | 100 | 110 | mV |
| **Error Amplifier** | | | | | | |
| Feedback Voltage | $V_{FB}$ | | 0.403 | 0.414 | 0.425 | V |
| Transconductance [6] | $G_{EA}$ | | | 125 | | μA/V |
| Upper Clamp Voltage | $V_{COMP\_H}$ | | 5 | 5.25 | 5.5 | V |
| Lower Clamp Voltage | $V_{COMP\_L}$ | | 1.42 | 1.5 | 1.58 | V |
| Max. Source Current[6] | $I_{COMP}$ | | | 50 | | μA |
| Max. Sink Current[6] | $I_{COMP}$ | | | -400 | | μA |
| **Current Sense Comparator and Zero Current Detector** | | | | | | |
| CS/ZCD Bias Current | $I_{BIAS\_CS/ZCD}$ | | | | 100 | nA |
| Leading-Edge-Blanking Time | $t_{LEB\_CS}$ | | | 400 | | ns |
| Current-Sense-Clamp Voltage | $V_{CS\_CLAMP}$ | | 1.9 | 2.0 | 2.1 | V |
| Over-Current-Protection, Leading-Edge-Blanking Time | $t_{LEB\_CSOCP}$ | | | 280 | | ns |
| Over-Current-Protection Threshold | $V_{CS\_OCP}$ | | 2.4 | 2.5 | 2.6 | V |
| Zero-Current-Detection Threshold | $V_{ZCD\_T}$ | $V_{ZCD}$ falling edge | 0.285 | 0.3 | 0.315 | V |
| Zero-Current-Detect Hysteresis | $V_{ZCD\_HYS}$ | | 617 | 650 | 683 | mV |

## ELECTRICAL CHARACTERISTICS *(continued)*

**$V_{CC}$ =20V, $T_A$ = +25°C, unless otherwise noted.**

| Parameter | Symbol | Condition | Min | Typ | Max | Units |
|---|---|---|---|---|---|---|
| ZCD Blanking Time | $t_{LEB\_ZCD}$ | After turn-off, $V_{MULT\_O}$ >0.3V | | 1.5 | | μs |
| | $t_{LEB\_ZCD}$ | After turn-off, $V_{MULT\_O}$ ≤0.3V | | 0.75 | | μs |
| Over-Voltage Blanking Time | $t_{LEB\_OVP}$ | After turn-off, $V_{MULT\_O}$ >0.3V | | 1.5 | | μs |
| | $t_{LEB\_OVP}$ | After turn-off, $V_{MULT\_O}$ ≤0.3V | | 0.75 | | μs |
| Over-Voltage Threshold | $V_{ZCD\_OVP}$ | 1.5μs delay after turn-off | 4.95 | 5.1 | 5.25 | V |
| Minimum Off Time | $t_{OFF\_MIN}$ | | 4 | 5 | 6 | μs |
| **Starter** | | | | | | |
| Start-Timer Period | $t_{START}$ | | | 190 | | μs |
| **Gate Driver** | | | | | | |
| Output-Clamp Voltage | $V_{GATE\_CLAMP}$ | $V_{CC}$=27V | 12.5 | 13.5 | 14.5 | V |
| Minimum-Output Voltage | $V_{GATE\_MIN}$ | $V_{CC}$=$V_{CC\_OFF}$ + 50mV | 6 | | | V |
| Max. Source Current(6) | $I_{GATE\_SOURCE}$ | | | 0.8 | | A |
| Max. Sink Current(6) | $I_{GATE\_SINK}$ | | | -1 | | A |

**Notes:**

5) The multiplier output is given by: Vcs=k*$V_{MULT}$*($V_{COMP}$-1.5)

6). Guaranteed by design.

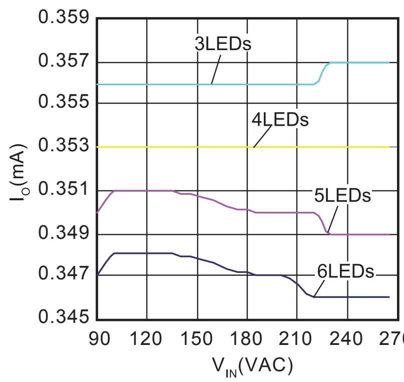


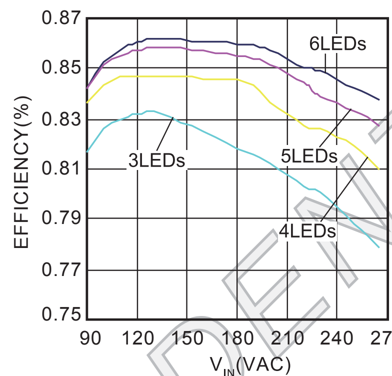
## TYPICAL PERFORMANCE CHARACTERISTICS

**$V_{IN}$ = 90V-265V, $V_{OUT}$ = 10-20V, $I_{LED}$=350mA, $T_A$ = 25°C, unless otherwise noted.**

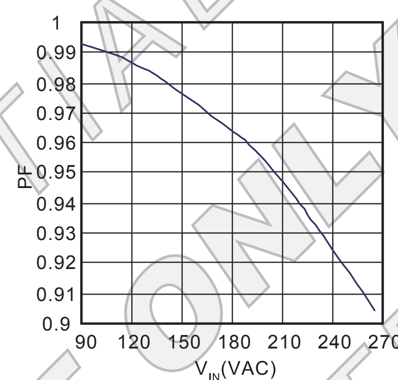
**Line/Load Regulation**



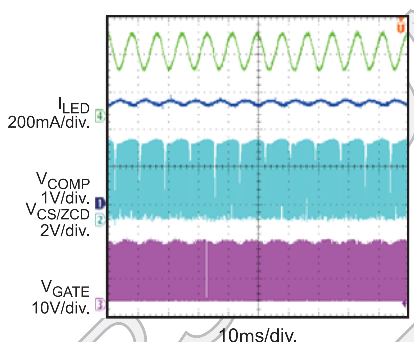

**Efficiency**



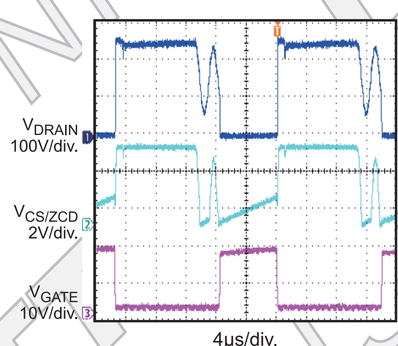

**PF @Full Load**



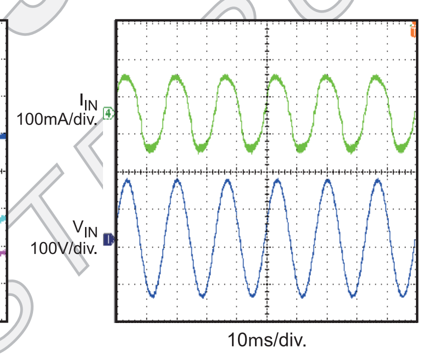

**Steady State**
$V_{IN}$ =110V



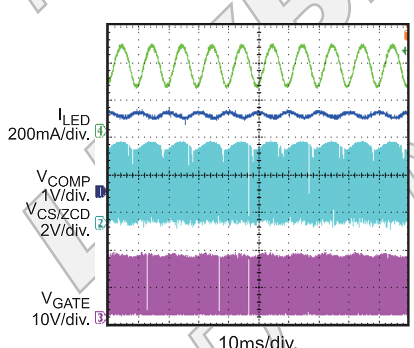

**Steady State**
$V_{IN}$ =110V



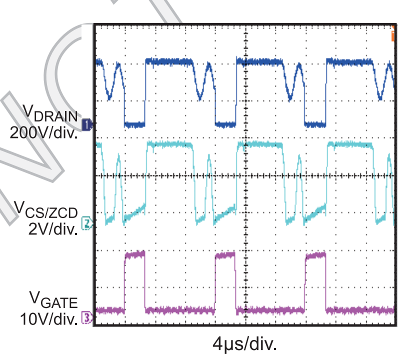

**Steady State**
$V_{IN}$ =110V



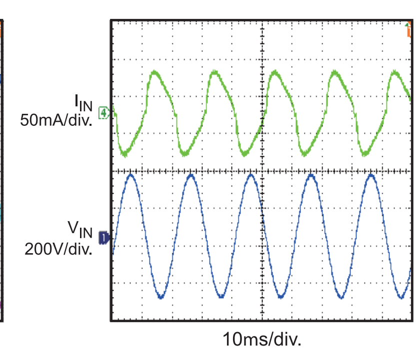

**Steady State**
$V_{IN}$ =230V




**Steady State**
$V_{IN}$ =230V



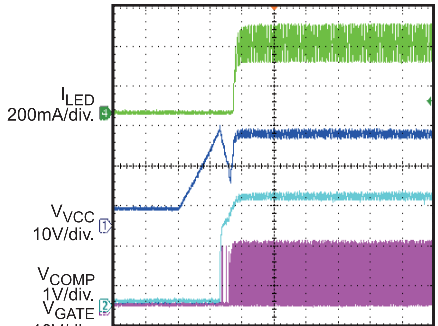

**Steady State**
$V_{IN}$ =230V



## TYPICAL PERFORMANCE CHARACTERISTICS *(continued)*

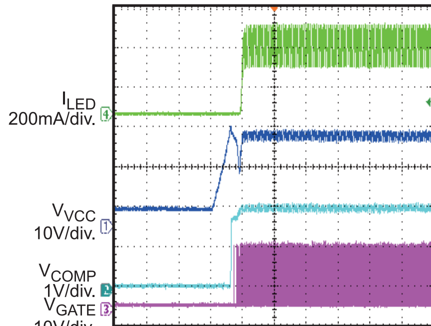
**$V_{IN}$ = 90V-265V, $V_{OUT}$ = 10-20V, $I_{LED}$=350mA, $T_A$ = 25°C, unless otherwise noted.**

**VIN Start up**
$V_{IN}$ = 110V



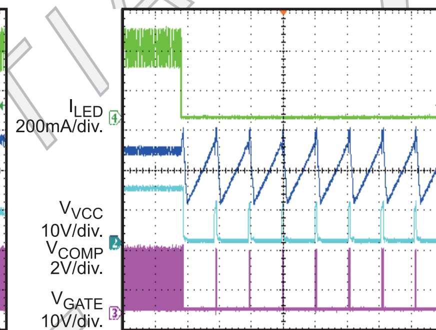
200ms/div.

**VIN Start up**
$V_{IN}$ = 230V



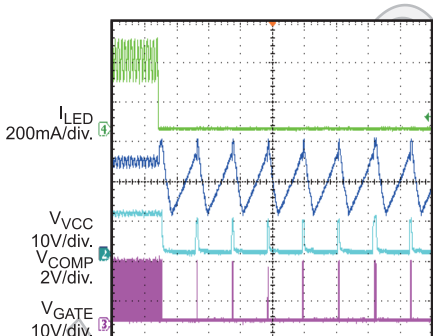
200ms/div.

**Open LED Protection**
$V_{IN}$ = 110V, Open LED @ Working



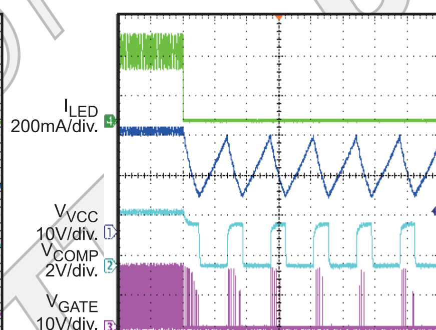
200ms/div.

**Open LED Protection**
$V_{IN}$ =230V, Open LED @ Working



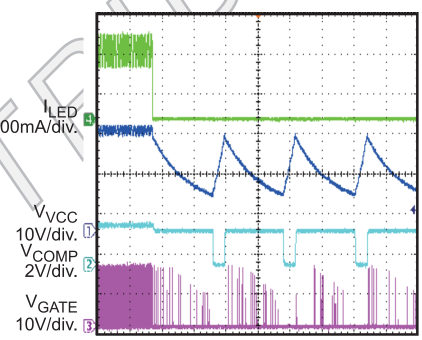
100ms/div.

**Short Circuit Protection**
$V_{IN}$ =110V
Short LED+ to LED- @ Working



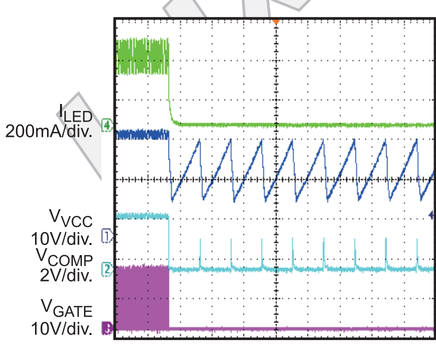
200ms/div.

**Short Circuit Protection**
$V_{IN}$ =230V
Short LED+ to LED- @ Working



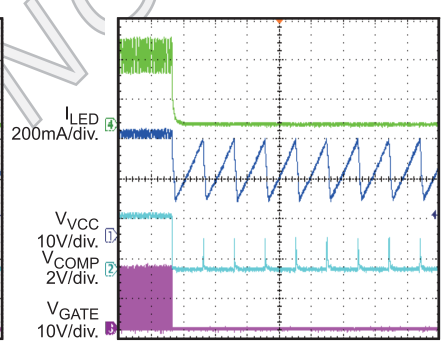
200ms/div.

**Primary-Side OCP Protection**
$V_{IN}$ =110V
Short primary winding @ Working



200ms/div.

**Primary-Side OCP Protection**
$V_{IN}$ =230V
Short primary winding @ Working



200ms/div.

## PIN FUNCTIONS

| Pin | Name | Description |
|---|---|---|
| 1 | VCC | Power Supply. Supplies power for the control signals and the high-current MOSFET. Bypass to ground with an external bulk capacitor (typically 4.7μF). |
| 2 | MULT | Input Voltage Sense. Connect to the tap of resistor divider between the rectified AC line and GND. The half-wave sinusoid provides a reference signal for the internal-current-control loop.<br>The MULT pin is also used for brown-out protection detection. |
| 3 | COMP | Loop Compensation. Connect a compensation network to stabilize the LED driver and maintain an accurate LED current. |
| 4 | GND | Ground. Current return for the control signal and the gate-drive signal. |
| 5 | CS/ZCD | Current Sense or Zero-Current Detection. When the gate driver turns on, a sensing resistor senses the MOSFET current. The comparison between the sensed voltage and the internal sinusoidal-current reference determines when the MOSFET turns off. If the pin voltage exceeds the current limit (2.0V, after turn-on blanking) the gate drive turns off.<br>When the gate driver turns off, the negative falling-edge (after the blanking time) triggers the external MOSFET's turn-on signal. Connect this pin to a resistor divider though a diode between the auxiliary winding and GND.<br>Over-voltage condition is detected through ZCD. For every turn-off interval, if the ZCD voltage exceeds the over-voltage-protection threshold after the 1.5μs ($V_{mult\_o}$ >0.3V) or 0.75μs ($V_{mult\_o}$ ≤0.3V) blanking time, over-voltage protection triggers and the system stops switching until auto-restart.<br>CS/ZCD is also used for primary-side over-current-protection, if the sensing voltage reaches to 2.5V after a blanking time at gate turn-on interval, the primary-side over-current-protection triggers and the system stops switching until auto-restart.<br>A 10pF ceramic cap is recommended to connect from CS/ZCD to GND to bypass the high frequency noise. In order to reduce the RC delay influence to the sample accuracy of the current sensing signal, the CS/ZCD down side resistance ($R_{ZCD2}$ in figure 7) should be smaller than 3kΩ. |
| 6 | GATE | Gate Drive Output. This totem-pole output stage can drive a high-power MOSFET with a peak current of 0.8A source and 1A sink. The high-voltage limit is clamped to 13.5V to avoid excessive gate-drive voltage. The low-voltage is higher than 6V to guarantee a sufficient drive capacity. |

## FUNCTION DIAGRAM

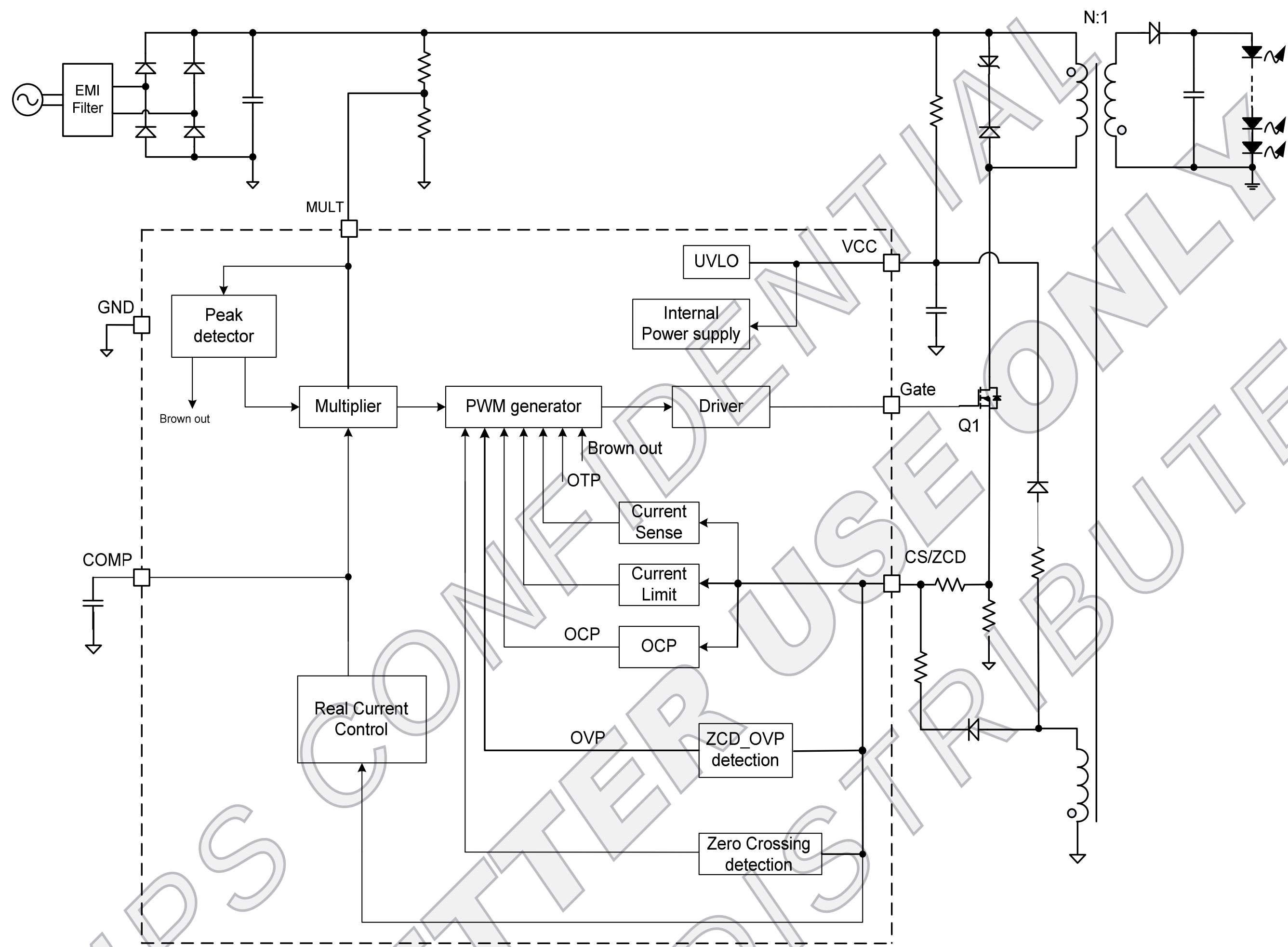



**Figure 1—MP4026 Function Block Diagram**

## OPERATION

The MP4026 is a primary-side-controlled, offline LED controller for high-performance LED lighting. It has primary-side real-current control for accurate LED current regulation. It also has active power factor correction (PFC) to eliminate harmonic noise on the AC line. The rich protections can achieve a high safety and reliability in real application.

### Start Up

Initially, AC line charges up $V_{CC}$ through the start-up resistor. When $V_{CC}$ reaches 24V, the control logic starts. Then the power supply is taken over by the auxiliary winding when the voltage of auxiliary winding builds up.

The MP4026 will shut down when $V_{CC}$ drops below 9V.

The high hysteretic voltage allows for a small VCC capacitor (typically 4.7uF) to shorten the start-up time.

### Boundary-Conduction Mode

During the external MOSFET ON-time ($t_{ON}$), the rectified-input voltage ($V_{BUS}$) charges the primary-side inductor (Lm), and the primary-side current ($I_P$) increases linearly from zero to the peak value ($I_{PK}$). When the external MOSFET turns OFF, the energy stored in the inductor transfers to the secondary-side and turns on the secondary-side diode to power the load. The secondary current ($I_S$) then decreases linearly from its peak value to zero. When the secondary current decreases to zero, the primary-side-leakage inductance, magnetizing inductance, and the parasitic capacitances decrease the MOSFET drain-source voltage—this decrease is also reflected on the auxiliary winding (see Figure 2). The zero-current detector in the CS/ZCD pin generates the external MOSFET's turn-on signal when the ZCD voltage falls below 0.3V (see Figure 3).

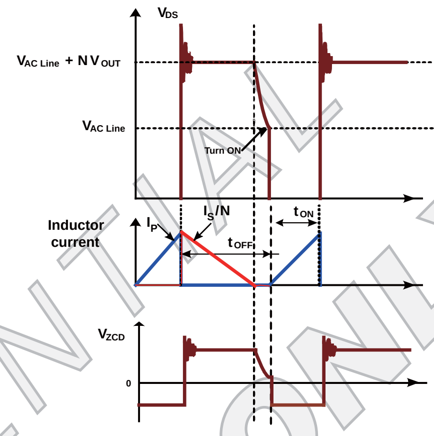



**Figure 2: Boundary-Conduction Mode**

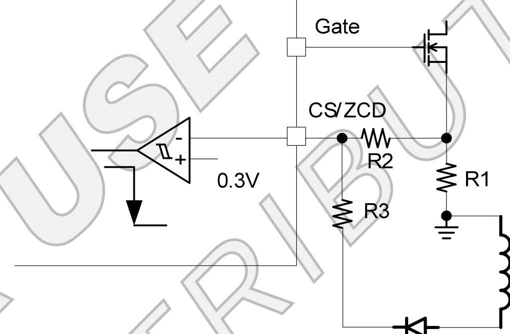



**Figure 3: Zero-Current Detector**

As a result, there are virtually no primary-switch turn-on losses and no secondary-diode reverse-recovery losses, ensuring high efficiency and low EMI noise.

### Real-Current Control

The proprietary real-current-control method allows the MP4026 to control the secondary-side LED current using primary-side information. The mean output LED current is approximately:

$$I_o \approx \frac{N \cdot V_{FB}}{2 \cdot R_s}$$

Where:

- N is the primary-side-to-secondary-side turn ratio,
- $V_{FB}$ is the feedback reference voltage (typically 0.414V), and
- $R_s$ is the sensing resistor connected between the MOSFET source and GND.



### Power-Factor Correction

The MULT pin is connected to a pull up resistor from the rectified-instantaneous-line voltage and fed as one input of the Multiplier. The multiplier output is sinusoidal.. This signal provides the reference for the current comparator and comparing with the primary-side-inductor current, which sets the sinusoidal primary-peak current. This helps to achieve a high-power factor.

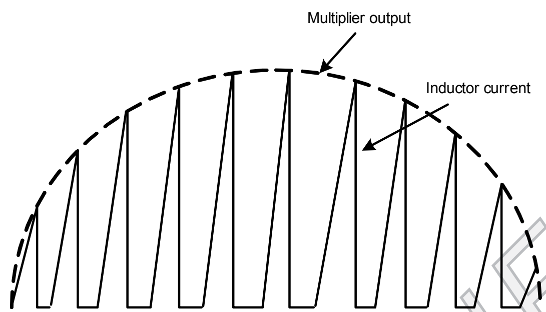



**Figure 4: Power-Factor Correction**

The maximum voltage of the multiplier output to the current comparator is clamped at 2V for a cycle-by-cycle current limit.

### VCC Under-Voltage Lockout

When $V_{CC}$ drops below the UVLO threshold (9V), the MP4026 stops switching and shuts down. The operating current is very low under this condition, the $V_{CC}$ will be charged up again by the external start up resistor from AC line. Figure 5 shows the typical $V_{CC}$ under-voltage lockout waveform.

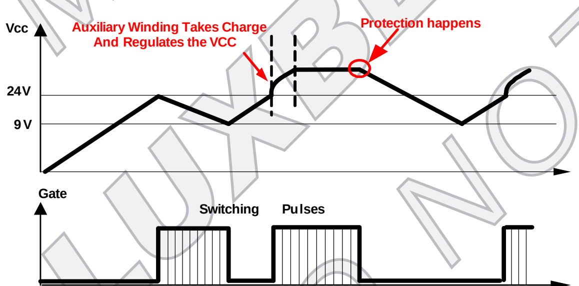



**Figure 5: VCC Start-Up Waveform**

### Auto Starter

The MP4026 has an integrated auto starter. The starter times when the MOSFET is OFF: If ZCD fails to send out another turn-on signal after 190μs, the starter will automatically send out the turn-on signal to avoid unnecessary shutdowns due to missing ZCD detections.

### Minimum Off Time

The MP4026 operates with a variable switching frequency; the frequency changes with the instantaneous-input-line voltage. To limit the maximum frequency and get a good EMI performance, the MP4026 employs an internal, minimum-off-time limiter—5μs.

### Leading-Edge Blanking

To avoid premature switching-pulse termination due to the parasitic capacitances discharging when the MOSFET turns on at normal operation, the MP4026 uses an internal-leading edge blanking (LEB) unit between the CS/ZCD pin and the current-comparator input. During the blanking time, the path from the CS/ZCD pin to the current comparator input is blocked. Figure 6 shows the leading-edge blanking. The LEB time of primary-side OCP detection is relatively short, 280ns.

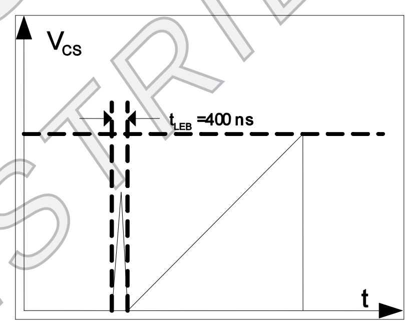



**Figure 6: Leading-Edge Blanking**

### Output Over-Voltage Protection

Output over-voltage protection prevents component damage during an over-voltage condition. The auxiliary-winding voltage's positive plateau is proportional to the output voltage: the OVP uses the auxiliary winding voltage instead of directly monitoring the output voltage. Figure 7 shows the OVP sampling unit. Once the ZCD voltage exceeds 5.1V at gate turn off interval, the OVP signal will be triggered and latched, the gate driver will be turned off and the IC works at quiescent mode, the $V_{CC}$ voltage dropped below the UVLO which will make the IC shut down, and the system restarts again.

The output-OVP-set point is then:

$$V_{OUT\_OVP} \cdot \frac{N_{AUX}}{N_{SEC}} \cdot \frac{R_{ZCD2}}{R_{ZCD1} + R_{ZCD2}} = 5.1V$$

Where:

- $V_{OUT\_OVP}$ is the output-over-voltage-protection point,
- $N_{AUX}$ is the number of auxiliary-winding turns, and
- $N_{SEC}$ is the number of secondary-winding turns.

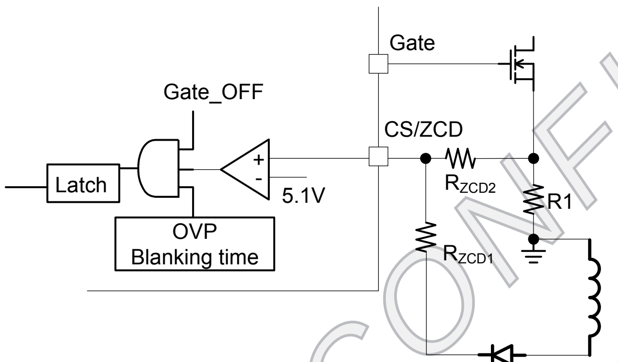



**Figure 7: OVP Sampling Unit**

To prevent a voltage spike from mis-triggering OVP after the switch turns off, OVP sampling has a $t_{LEB\_OVP}$ blanking period (typically 1.5μs when $V_{MULT\_O}$ > 0.3V and 0.75μs when $V_{MULT\_O}$ ≤ 0.3V) as shown in Figure 8.

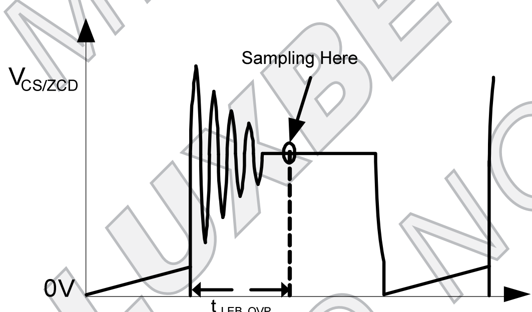



**Figure 8: ZCD Voltage and OVP Sampler**

## Output Short-Circuit Protection

If an output short occurs, the ZCD can not detect the transformer's zero-current-crossing point, so the 190μs auto-restart timer triggers the power MOSFET's turn-on signal. Then the switching frequency of the power circuit drops to about 5kHz, and the output current is limited to its nominal current. The auxiliary-winding voltage drops to follow the secondary-winding voltage, $V_{CC}$ drops to less than the UV threshold, and the system restarts. This sequence limits the output power and IC temperature rise if an output short occurs.

## Primary-Side Over-Current Protection

The primary-side over-current protection prevents device damage caused by extremely excessive current, like primary winding short. If the CS/ZCD pin voltage rising to 2.5V at gate turn on interval, as shown in Figure 9, the primary-side over-current protection signal will be triggered and latched, the gate driver will be turned off and the IC works at quiescent mode, the $V_{CC}$ voltage dropped below the UVLO which will make the IC shut down, and the system restarts again.

To avoid mis-trigger by the parasitic capacitances discharging when the MOSFET turns on, a LEB time is needed, this LEB time is relatively smaller than current regulation sensing LEB time, typical 280ns.

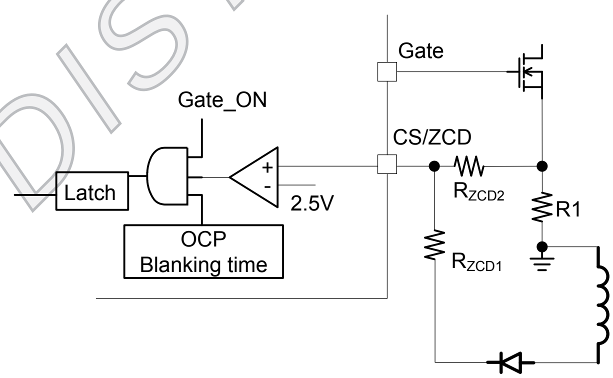



**Figure 9: Primary-side OCP Sampling Unit**

## Brown-Out Protection

The MP4026 has brown-out protection: the internal peak detector detects the peak value of the rectified sinusoid waveform in MULT pin. If the peak value is less than the brown-out-protection threshold 0.3V for 36ms, the IC recognizes this condition as a brown-out, quickly drops the COMP voltage to zero, and disables the power circuit. If the peak value exceeds 0.4V, the IC restarts and the COMP voltage rises softly again. This feature prevents both the transformer and LED currents from saturating during fast ON/OFF switching. Figure 10 shows the brown-out waveforms.

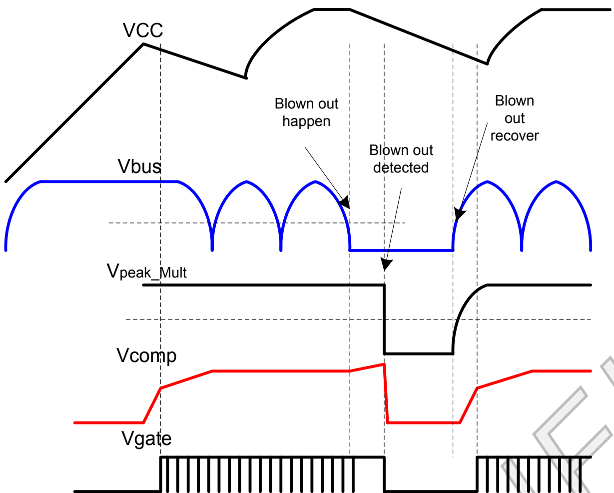



**Figure 10: Brown-Out Protection Waveforms**

### IC Thermal Shut Down

To prevent from any lethal thermal damage, when the inner temperature exceeds the OTP threshold, the MP4026 shuts down switching cycle and latched until VCC drop below UVLO and restart again.

### Design Example

For the design example, please refer to MPS application note AN076 for the detailed design procedure

# TYPICAL APPLICATION CIRCUITS

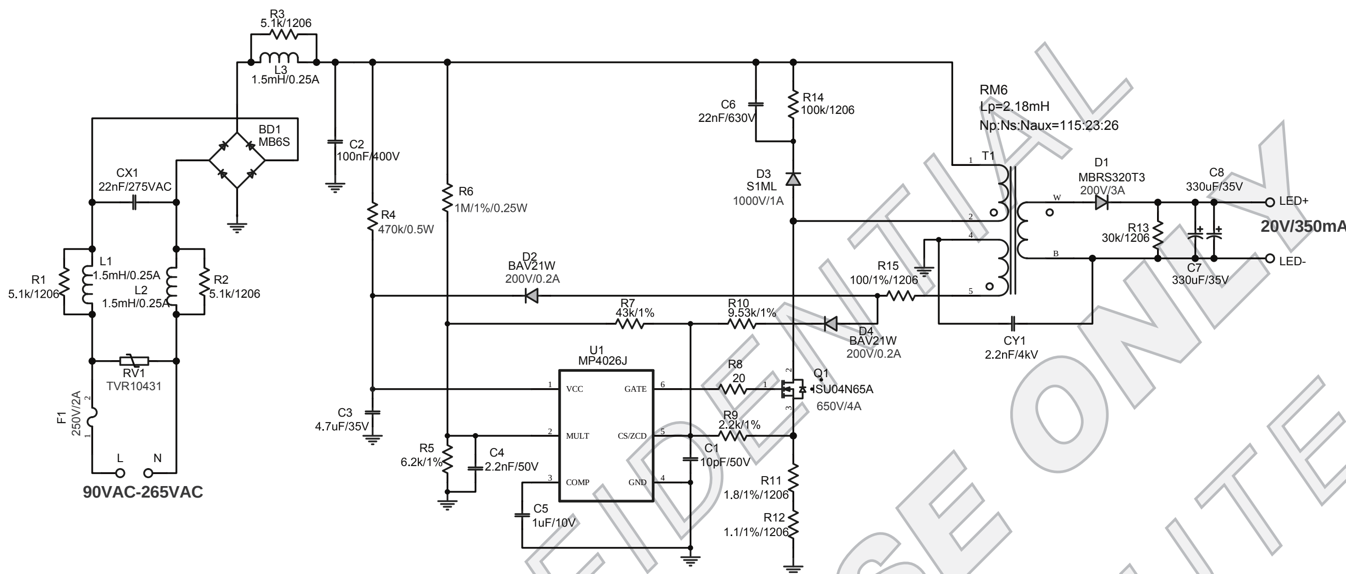



**Figure 11: A19 Bulb Driver, 90-265VAC Input, Isolated Flyback Converter, $V_O$ =20V, $I_O$=350mA**
**EVB Model: EV4026-J-00A**



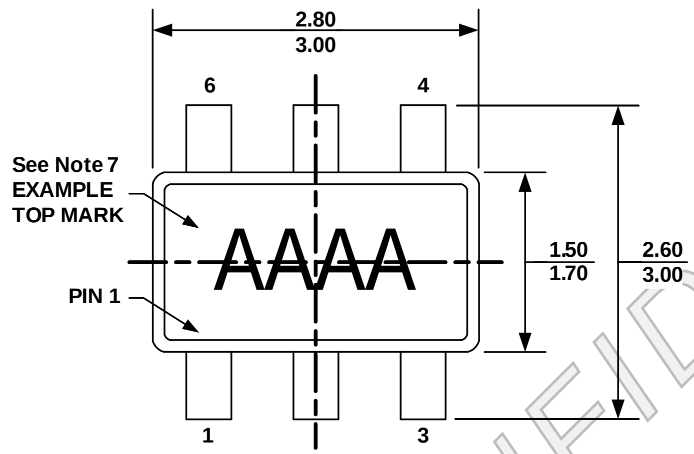
 

*PRELIMINARY SPECIFICATIONS SUBJECT TO CHANGE*

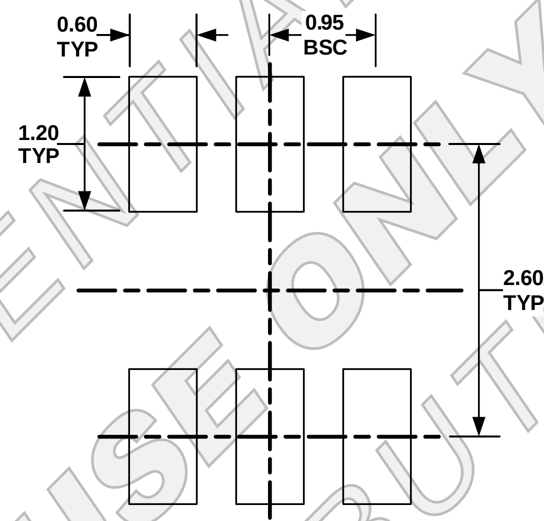
*PRELIMINARY SPECIFICATIONS SUBJECT TO CHANGE – LUXBETTER USE ONLY*

# PACKAGE INFORMATION

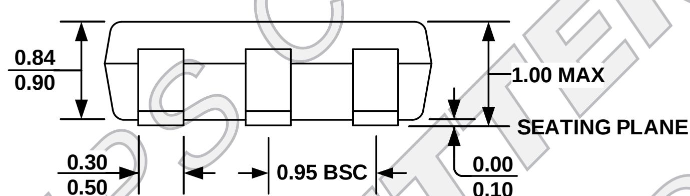
## FCTSOT23-6



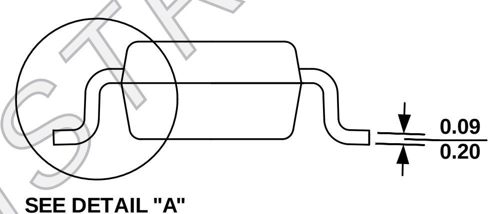

TOP VIEW



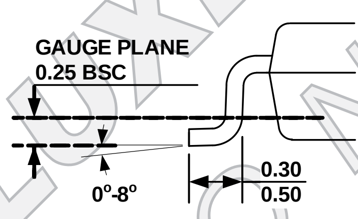

RECOMMENDED LAND PATTERN




FRONT VIEW




SIDE VIEW




DETAIL "A"

**NOTE:**

1) ALL DIMENSIONS ARE IN MILLIMETERS
2) PACKAGE LENGTH DOES NOT INCLUDE MOLD FLASH, PROTRUSION OR GATE BURR
3) PACKAGE WIDTH DOES NOT INCLUDE INTERLEAD FLASH OR PROTRUSION.
4) LEAD COPLANARITY (BOTTOM OF LEADS AFTER FORMING) SHALL BE 0.10 MILLIMETERS MAX.
5) DRAWING CONFORMS TO JEDEC MO-193, VARIATION AB.
6) DRAWING IS NOT TO SCALE
7) PIN 1 IS LOWER LEFT PIN WHEN READING TOP MARK FROM LEFT TO RIGHT, (SEE EXAMPLE TOP MARK)